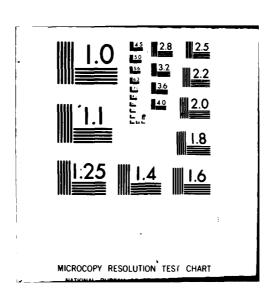
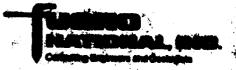
FUGRO NATIONAL INC LONG BEACH CA F/6 8/13 MX SITING INVESTIGATION. GEOTECHNICAL EVALUATION. VOLUME VII. N--ETC(U) AUG 79 F04704-80-C-0006 AD-A113 329 UNCLASSIFIED FN-TR-27-7 NL.



# MX SITING INVESTIGATION GEOTECHNICAL EVALUATION

VOLUME VII NEVADA-UTAH VERIFICATION STUDIES, FY 79 GEOTECHNICAL DATA, REVEILLE-RAILROAD CDP, NEVADA

PREPARED FOR SPACE AND MISSILE SYSTEMS ORGANIZATION (SAMSO)
NORTON AIR FORCE BASE, CALIFORNIA



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VOLUME VII, NEVADA-UTAH
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GEOTECHNICAL DATA
REVEILLE-RAILROAD CDP, NEVADA

# Prepared for:

U. S. Department of the Air Force Space and Missile Systems Organization (SAMSO) Norton Air Force Base, California 92409

Prepared by:

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24 August 1979

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## VOLUME VII GEOTECHNICAL DATA, REVEILLE-RAILROAD CDP

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- 2.0 GROUND-WATER DATA
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- 6.0 BORING LOGS
- 7.0 TRENCH AND TEST PIT LOGS
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- 10.0 FIELD CBR TEST RESULTS

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- 2 CONE PENETROMETER TEST RESULTS

#### **FOREWORD**

This report was prepared for the Department of the Air Force, Space and Missile Systems Organization (SAMSO), in compliance with Contract No. F04704-78-C-0027, CDRL Item 005A2. It presents geological, geophysical, and geotechnical data and evaluates the suitability of portions of Nevada and Utah for siting the MX Land Mobile Advanced ICBM System.

This report is the first of several Verification reports which will be prepared. The objectives are to verify sufficient suitable area for deployment of the MX System and to provide preliminary physical and engineering characteristics of the soils. The Verification Studies are the final phase of a site-selection process which was begun in 1977. Previous studies have been termed Screening, Characterization, and Ranking. In preparing this report, it has been assumed that the reader is familiar with these previous studies.

Results of the FY 79 Verification studies are contained in 11 volumes as follows:

## Geotechnical Results

Volume 1A - Sections 1.0, 2.0, and 3.0 contain Introduction, Results and Conclusions, and Recommendations for Future Studies. Sections 4.0 through 6.0 contain summary geotechnical data for Whirlwind, Snake East, and Hamlin CDP's.

Volume 1B - Sections 7.0 through 10.0 contain summary geotechnical data for White River North, Garden-Coal, Reveille-Railroad and Big Smoky CDP's.

#### Geotechnical Data Volumes

Volume II - Whirlwind CDP

Volume III - Snake East CDP

Volume IV - Hamlin CDP

Volume V - White River North CDP

Volume VI - Garden-Coal CDP

\* Volume VII - Reveille-Railroad CDP

Volume VIII - Big Smoky CDP

Volume IX - Dry Lake CDP

Volume X - Ralston CDP

<sup>\*</sup> This volume is presented herein.

SECTION 1.0 SECTION DATA Column Heading

USCS

# EXPLANATIONS OF GEOLOGIC STATION DATA

Geologic stations were established at selected locations throughout the CDP at which detailed descriptions of surficial basin-fill deposits or rock were recorded. Locations of all geologic stations are shown in Drawing 1, Activity Location Map. All data taken on surficial basin-fill units at these stations are listed in Table 1-1 and an explanation of the column headings in the table is given below. At stations where rock descriptions were made, only geologic unit designations are listed. A general explanation of all geologic unit symbols used in Verification Studies is included at the end of this section.

Table 1-1	<u>Explanation</u>
Station Number	Geologic stations are numbered sequentially. Where more than one geologic field team worked in a CDP, stations made by each team are differentiated with a letter (A, B, or C) following the station number.
Geologic Unit	Generic geologic unit only, i.e. the grain-size designation (f, s, g, c) is omitted from surficial basin-fill units. The letter B in the unit designation indicates a buried deposit not exposed at the surface.
MPS MM	Average maximum particle size in millimeters.
Grain Size (%B, %C, %G, %S, %F)	Estimated particle size distribution using the Unified Soil Classification System. Percentages of boulders (%B) and cobbles (%C) are based on the entire deposit, whereas percentages of gravel (%G), sand (%S) and fines (%F) are taken only on the fraction composed of particles less than 3 inches (76 mm) in diameter.

ification System.

Soil class according to the Unified Soil Class-

Munsell Color Soil color based on Munsell Soil Color Chart.

Source Rock
Types(s)

Rock types of coarse clasts listed in order of abundance.

\* Physical Properties

Data listed in columns 6 through 15 address specific soil properties. These are listed below in parentheses following the column heading number and are also listed at the bottom of Table 1-1. Data are coded with each numerical entry referring to a specific soil condition as listed below.

- 6 (Grain Shape) 1) Angular, 2) Subangular, 3) Subrounded, 4) Rounded, 5) Well rounded
- 7 (Moisture 1) Dry, 2) Moist, 3) Wet Content)
- 8 (Plasticity 1) None, 2) Low, 3) Medium, 4) High
  of Fines)
- 9 (Consistency) Coarse grained: 1) Very Loose, 2) Loose, 3) Medium Dense, 4) Dense, 5) Very Dense,

Fine grained: 1)Soft, 2) Firm, 3) Stiff, 4) Hard

- 10 (Structure)
  1) Stratified Tabular, 2) Stratified Other (lensed, cross bedded, discontinuous beds),
  3) Nonstratified
- 11 (Cementation 1) None, 2) Weak, 3) Moderate, 4) Strong
  Induration)
- 12 (Depth to Depth to layer (in centimeters) exhibiting Cemented cementation induration described in Column 11 Layers) (above)
- 13 (Weathering 1) Fresh, 2) Slight, 3) Moderate, 4) Very of clasts)
- 14 (Soil l) None (A-C profile), 2) Poor (incipient Profile B-horizon), 3) Well (prominant B-horizon) Development)
- 15 (Caliche 1) Stage I, 2) Stage II, 3) Stage III, Development) 4) Stage IV, 5) None

Drainage

DP (M) Average depth of drainages (in meters) WD (M) Average width of drainages (in meters)

Slope (%) Average slope of ground surface (in percent

grade)

Sample Number of samples taken

#### GENERALIZED GEOLOGIC UNITS

#### Explanation

## Surficial Basin-fill Units

- Al Younger Fluvial Deposits Major modern stream channel and flood-plain deposits.
- A2 Older Fluvial Deposits Older incised stream channel and flood-plain deposits in elevated terraces bordering major modern drainages.
- A3 Eolian Deposits Wind-blown deposits of sand occurring as either thin sheets (A3s) or dunes (A3d).
- A4 Playa and Lacustrine Deposits Deposits occurring in modern, active playas (A4) or in either inactive playas or older lake beds and abandoned shorelines associated with extinct lakes (A40).
- As Alluvial Fan Deposits Alluvial deposits consisting of debris flow and water-laid alluvium near mountain fronts, grading into predominantly water-laid alluvium deposited in shifting distributary channels near the basin center. Younger (A5y), intermediate (A5i), and older (A5o) alluvial fans are differentiated by surface soil development, terrain conditions, and present depositional/erosional environment.

Grain sizes of these deposits (except A3 deposits, which are exclusively sandy) are indicated by a single letter (f, s, g, or c) following the geologic unit symbol. These letters indicate the predominant grain size and range of soil types according to the Unified Soil Classification System:

- f fine-grained (ML, CL, MH, CH)
- s sands (SP, SW, SM, SC)
- g gravels (GP, GW, GM, GC)
- c coarse grained with greater than 30 percent boulders and cobbles (generally GP, GW, GM, GC)

#### ROCK UNITS

- I Igneous (undifferentiated). Rocks formed by solidification of a molten or partially molten mass.
  - Il Intrusive Plutonic rocks formed by solidification of molten material beneath the surface (e.g., granite, granodiorite, diorite, gabbro).
  - Extrusive (intermediate and acidic) Volcanic rocks of intermediate and acidic compositon formed by solidification of molten material at or near the surface, (e.g., rhyolite, latite, dacite, andesite).
  - I3 Extrusive (basic) Volcanic rocks of basic composition, generally formed by solidification of molten materials at or near the surface (e.g., basalt).
  - I4 Extrusive (pyroclistic) Rocks formed by accumulation
     of volcanic ejecta (e.g., ash, tuff, welded tuff,
     agglomerate).
- S Sedimentary (undifferentiated) Rocks formed by accumulation of clastic solids, organic solids and/or chemically precipitated minerals.
  - Sl Arenaceous and/or Siliceous Rocks Composed of sand size particles (e.g., sandstone, orthoguartzite) or of cryptocrystalline silica (e.g., opal, chert).
  - S2 Carbonate Rocks Composed predominantly of calcium carbonate detritus or chemical precipitates (e.g., limestone, dolomite, chalk).
  - S3 Argillaceous Rocks Composed of clay and silt-sized particles (e.g., siltstone, shale, claystone).
  - S4 Evaporite Rocks Precipitated from solution as a result of evaporation (e.g., halite, gypsum, anhydrite, sylvite).
  - S5 Coarse Clastic Rocks Composed of gravel sized or larger clasts (e.g., conglomerate, breccia).
- M Metamorphic (undifferentiated) Rocks formed through recrystallization in the solid state of preexisting rocks by heat and pressure (e.g., gneiss, schist, hornfels, metaquartzite).

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STATION Rumper	GEOL MPS CRAIN SIZE UNIT MM RH RC RC RE VF US	MUSTELL STURES IS LOUDE FOCK TYPLISS	+PHYSICAL PROPERTIES 6 7 8 9 10 11 12 17 14 15	CRAINIGE PLINE CREMA NICHA (NA ISANGLE
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\*PHYSICAL PROPERTIES : 6 - GPAIN SHAPE 7 - POISTURE CONTENT 8 - PLASTICITY FIRES

15 - CALIENE GENTLOPTENT

+ - CONSISTEMEN 18 - STAUCTURE 11 - CEMENTATION-INDURATION 12 - (EPTH TO CPMENTED LAVERICM) 13 - MEATHERING OF CLASTS 14 - SOIL PROFILE DEVELOPMENT

> GEOLOGIC STATION DATA VERIFICATION SITE, REVEILLE-RAILROAD, NEVADA

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO TABLE 1-1 1 0F 2

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NPR631C	451 072 00 07 05 065 CA		2 2 3 3 3 2 037 2 3 2	1.0 185 24 2	
MRRESIA	451 217 00 CH 42 333 015			1.0 004 (5 )	
MARGSIC	451 070 00 00 25 085 020	SC 10.0YP4/4 12	3 2 3 3 7 7 027 2 3 1	6.0 025 77 2	
NRº631C	AST 034 09 00 01 064 035			•5 00 <b>•</b> 00 0	
M486324	457 942 94 04 20 060 923			• 1	
484632C	451 145 0T 05 15 065 C20		7 2 2 2 3 2 032 2 7 2	1.5 003 37 3	
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NAGGRA	ASY 102 00 07 15 075 "16		2 2 1 1 3 1 1 1 1	·	
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MEPGAPA	AST 365 OT CL 55 035 CL		2 1 1 2 2 2 025 5 2 2	•# CG7 C7 P	
4886414	ASE 105 00 01 20 065 015		2 2 1 1 1 2 019 7 2 2		
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MARGROA	457 08° 08 08 07 044 621			.0 666 61	
MORESIA	AST 130 00 C3 30 042 7G				
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488G60A	A51 128 CO OT 20 060 C2		2 2 1 3 3 2 022 3 3 2	.4 LO7 C7 C	
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488644	AST 191 00 C1 30 095 01	SP 15.0495/6 12	7 2 1 3 2 1 2 2 5	•£ 003 32 :	
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<b>488647</b>	457 656 80 60 10 978 CZ	: S# 10-6784/4 12 51		.6 056 L1 (	

-PHYSIC'L PROBERTIES:
6 - GPAIN SWAFE
10 - STPUCTUFF 11 - STPUCTUFF 12 - FATHLIFIED LAYLIFIED 15 - CALICHE GEN LUPIENT 7 - POISTURE CONTENT 11 - CEMPITATION-INCURATION 14 - SOIL PROPILE GENELOPMENT

GEOLOGIC STATION DATA
VERIFICATION SITE, REVEILLE-RAILROAD, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

TABLE 1-1 2 OF 2

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C

SECTION 2.0 GROUND-WATER DATA

C

#### EXPLANATIONS OF GROUND-WATER DATA

Existing ground-water data were collected from all available sources. These data were updated where possible from measurements taken during Fugro field operations, and all data are shown on Table 2-1. Locations of water wells and boreholes in which water-level measurements were available are shown in Drawing 1. Well numbers listed in Column 1 (Table 2-1) refer to well locations in Drawing 1. Actual well numbers giving location according to the Bureau of Land Management Land Survey System are shown in Column 2.

Water levels generally refer to the static ground-water table in the unconfined basin-fill aquifer. Perched conditions or levels in artesian aquifers are noted where known.

		ELEVATION	DEPTH OF WELL - FEET (METERS)	WATER LEYEL			
	WELL LOCATION NUMBER*	OF GROUND SURFACE - FEET (METERS) ABOYE M.S.L.		DEPTH BELOW GROUND SURFACE — FEET (METERS)	DATE MEASURED	ELEVATION - FEET (RETERS) ABOVE M.S.L.	REFERENCES**/ REMARKS
W1	4N/51E-13d1	5120	300	3	1959	5117	2
		(1561)	(91)	(1)		(1560)	Ì
W2	4N/54E-18dc	4911	150	137	1967	4774	1
		(1497)	(46)	(42)		(1455)	
W3	4N/55-19da	5000	255	214	1971	4786	1
		(1524)	(78)	(65)		(1456)	
W4	3N/51E-19c1	5450	320	280	1964	5170	2
		(1661)	(98)	(85)	1	(1576)	l
W 5	3N/55E-35bac	4942	204	165	1972	4777	1
		(1506)	(62)	(50)		(1456)	
W6	3N/54E-5bc	5040	325	265	1948	4775	1
		(1536)	(99)	(81)	1	(1455	1
W7	2N/53E-23cbc	4892	180	113	1972	4779	1
		(1491)	(55)	(34)		(1457	
W8	1N/53E-3dac	4851	120	69	1972	4782	1
		(1479)	(37)	(21)	1	(1458	ļ
W9	1N/53E-7adc	4856	136	78	1972	4778	1
		(1480)	(41)	(24)		(1456)	į.
W10	1N/53E-27bba	4969	200	172	1972	4797	1
		(1515)	(61)	(52)		(1462)	
W11	1N/53E-31dcc	5024	272	205	1951	4819	1
		(1531)	(83)	(62)		(1469)	l
W12	1N/53-32db	5004	292	225	1957	4779	1
!		(1525)	(89)	(69)		(1457)	1
W13	1S/51½E-23bc	5930	370	335	1959	5595	1
	''	(1807)	(113)	(102)		(1705)	
W14	1S/53E-28bda	5205	465	415	1972	4790	1
		(1586)	(142)	(126)		(1460)	ł

- \* Mt. Diablo Baseline and Meridian
- \*\* References:
  - 1. Rush and Everett (1966)
  - 2. Van Denburgh and Rush (1974)

GROUND-WATER DATA
VERIFICATION SITE
REVEILLE-RAILROAD CDP, NEVADA

NOTE: All wells tap unconfined alluvial aquifers except where neted. Where published data are lacking or inaccurate, ground surface elevations are taken from topographic maps. MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO

TABLE 2-1

<u>UGRO NATIONAL, INC.</u>

SECTION 3.0 SEISHLE REPRACTION DATA

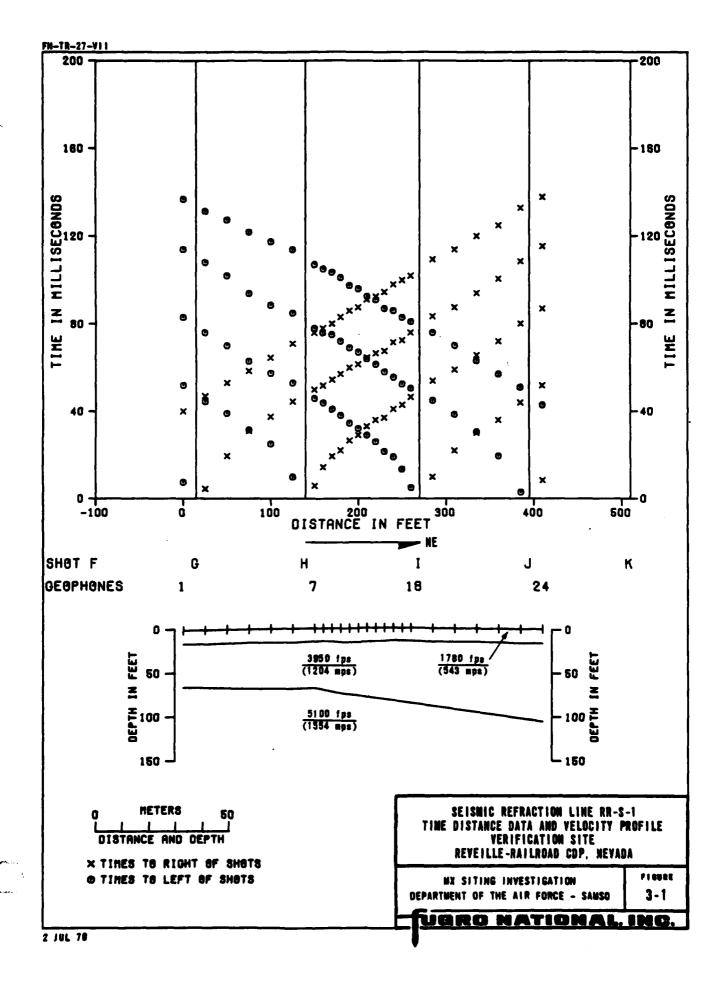
#### EXPLANATIONS OF SEISMIC REFRACTION DATA

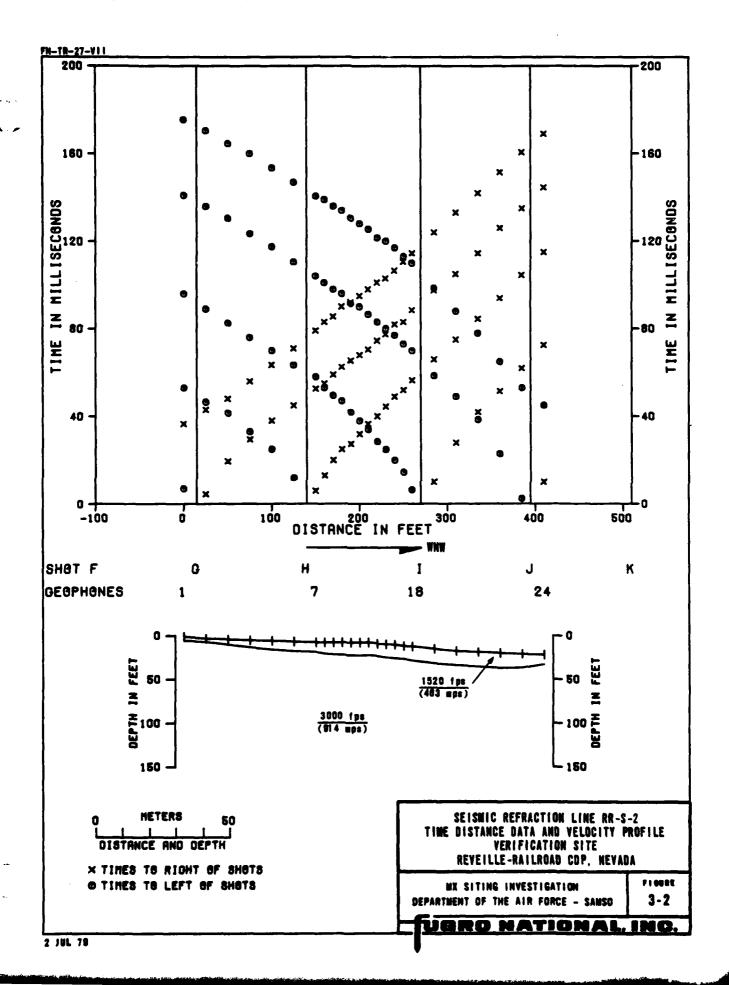
Each figure shows seismic wave travel times plotted versus surface distance between the energy source (shot) and the detector (geophone) for a single seismic line. Distances are measured along the line from geophone number 1 which is designated as zero distance. Distances to the right (on the paper) of geophone 1 are positive. The direction arrow gives the approximate direction of the geophone array from geophone 1 to geophone 24.

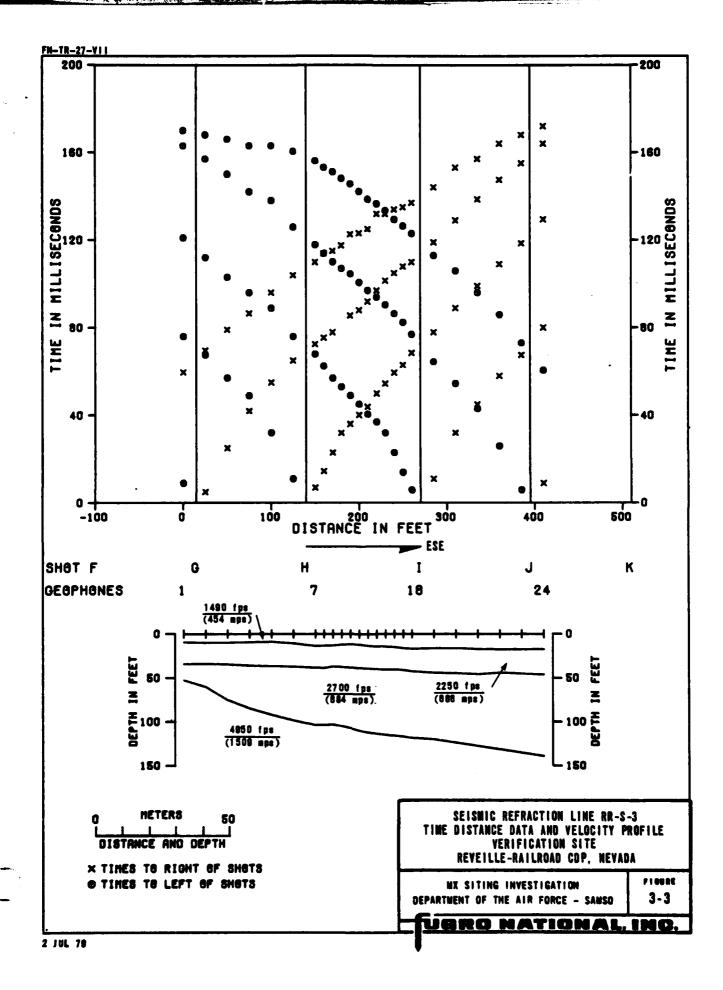
Travel Time Versus Distance Graph (Upper Half of Figure)
This is a travel time versus distance graph. The abscissa
represents distance; the ordinate, time. The six vertical
lines represent the locations of shots (designated as F, G, H,
I, J, and K). The symbol, X, denotes travel times at geophones
that were located to the right of a shot. The symbol, 0,
denotes travel times that were located to the left of shots.

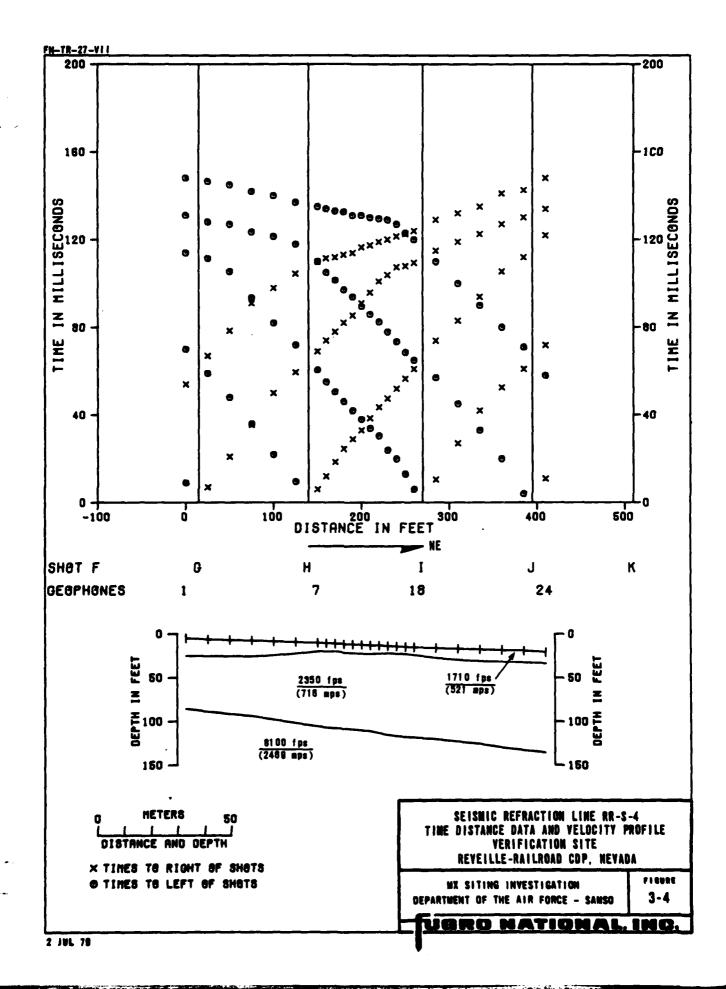
# Velocity Cross Section (Lower Half of Figure)

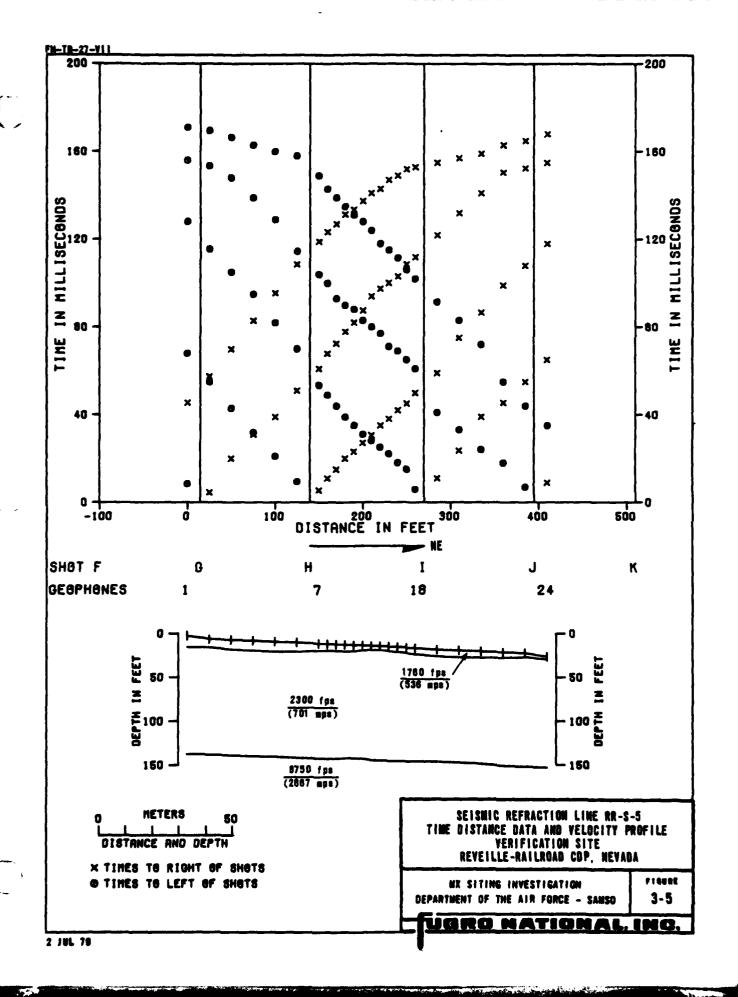
This is an interpreted velocity cross section beneath the seismic line. The top line represents the ground-surface profile. The short vertical lines crossing the top line mark the geophone positions. The depth scale is plotted relative to a point on the line which was arbitrarily chosen as "zero elevation" at the time the line was surveyed. The additional lines across the cross section represent the interpreted boundaries between layers of material with different compressional wave velocities. These boundaries are commonly called "refractors". The velocity interpreted to be representative of each layer is shown.

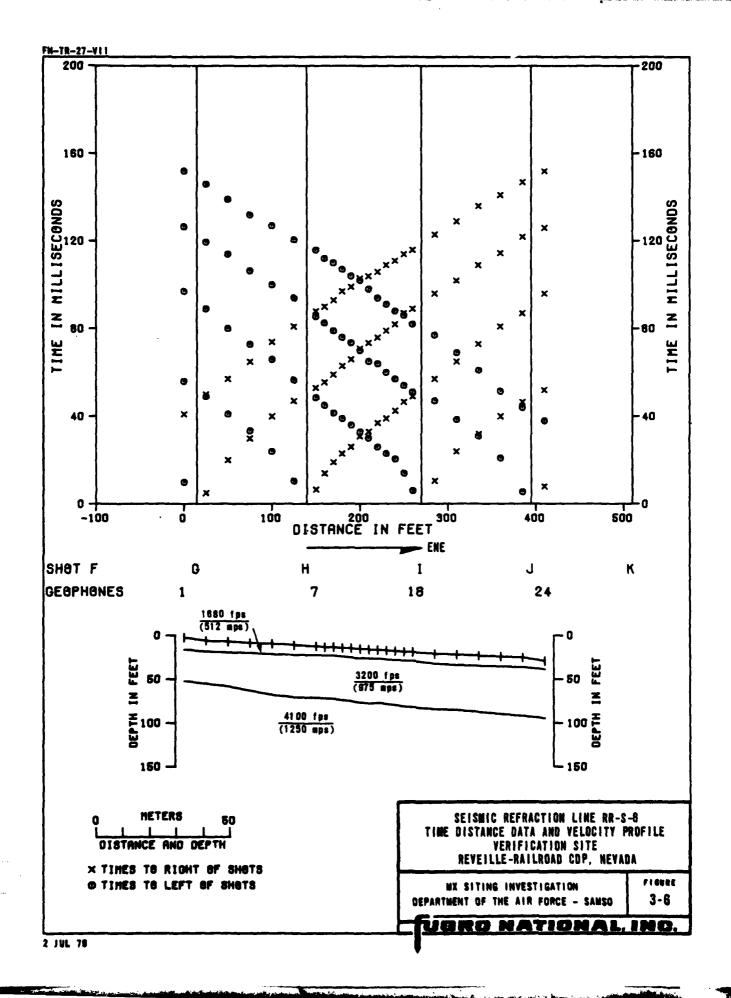


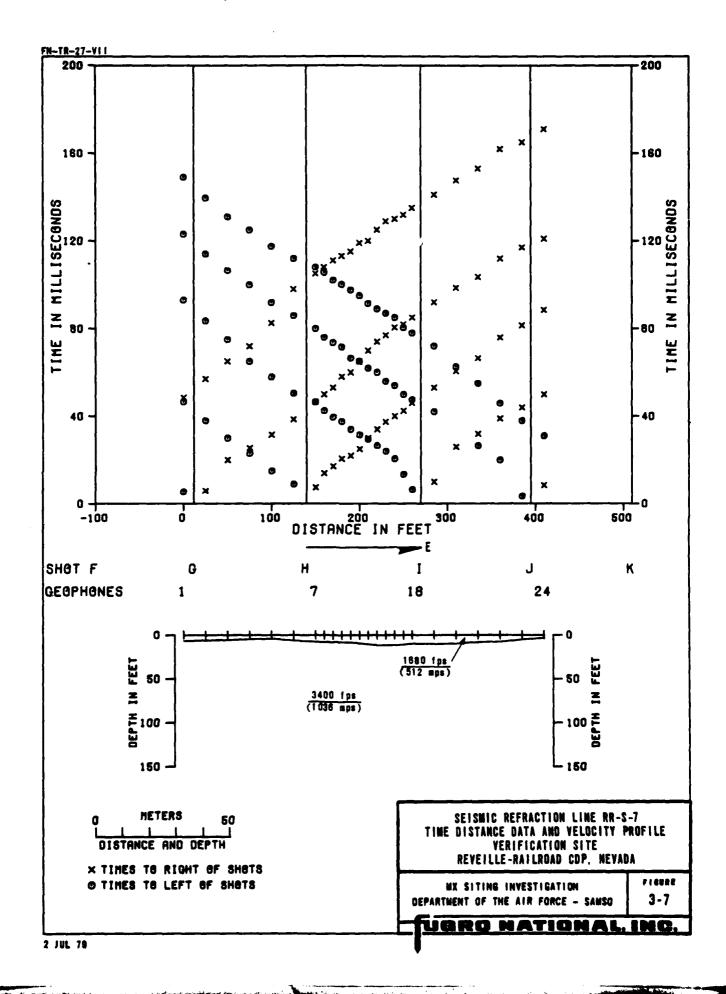


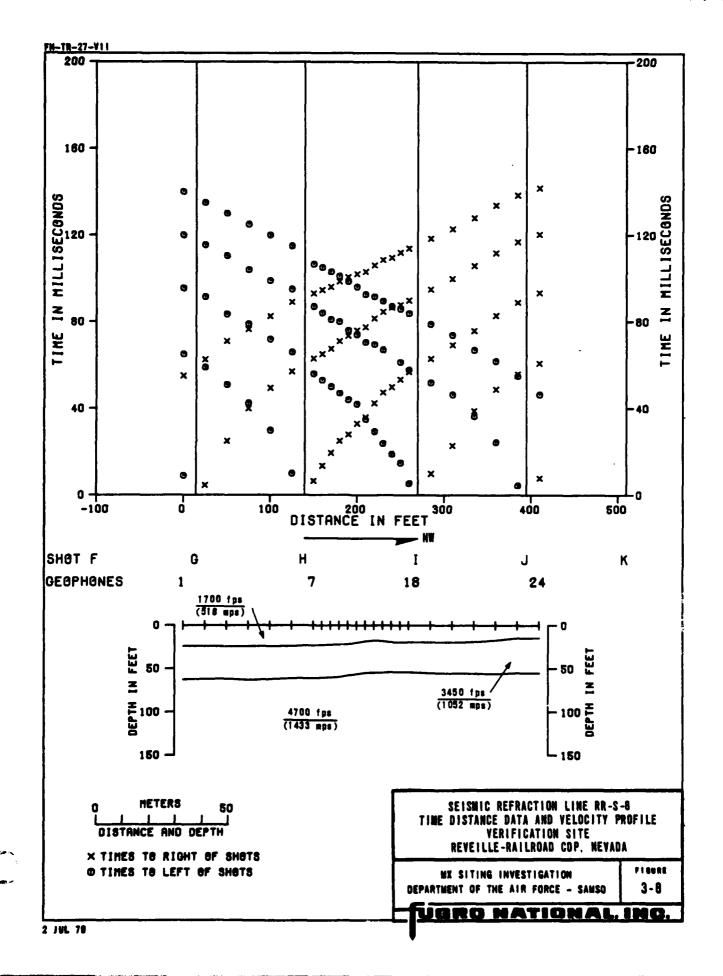


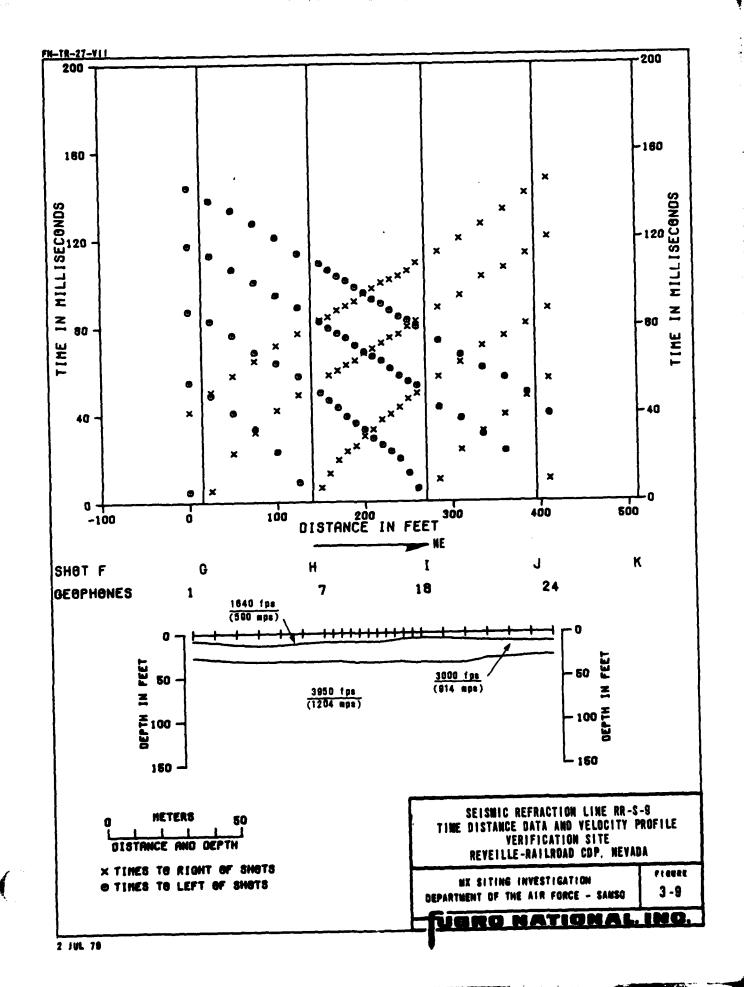


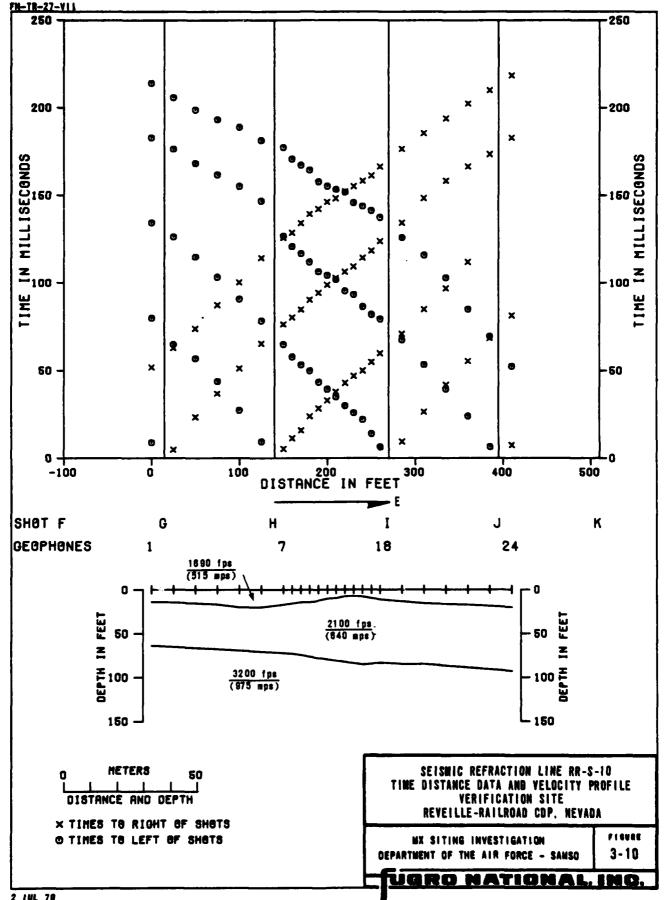


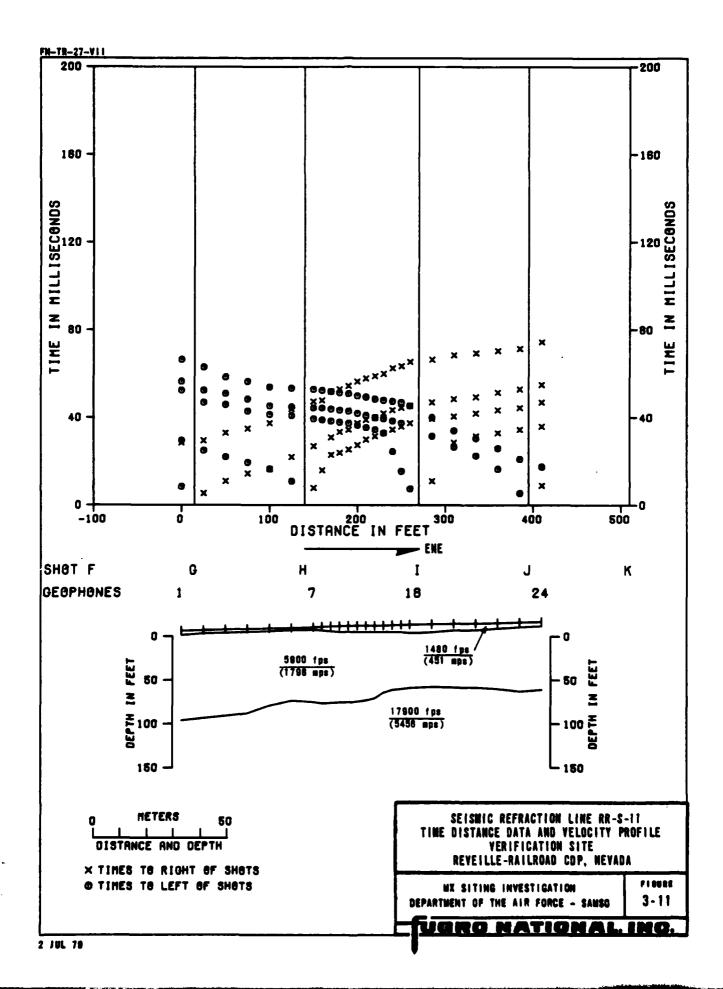


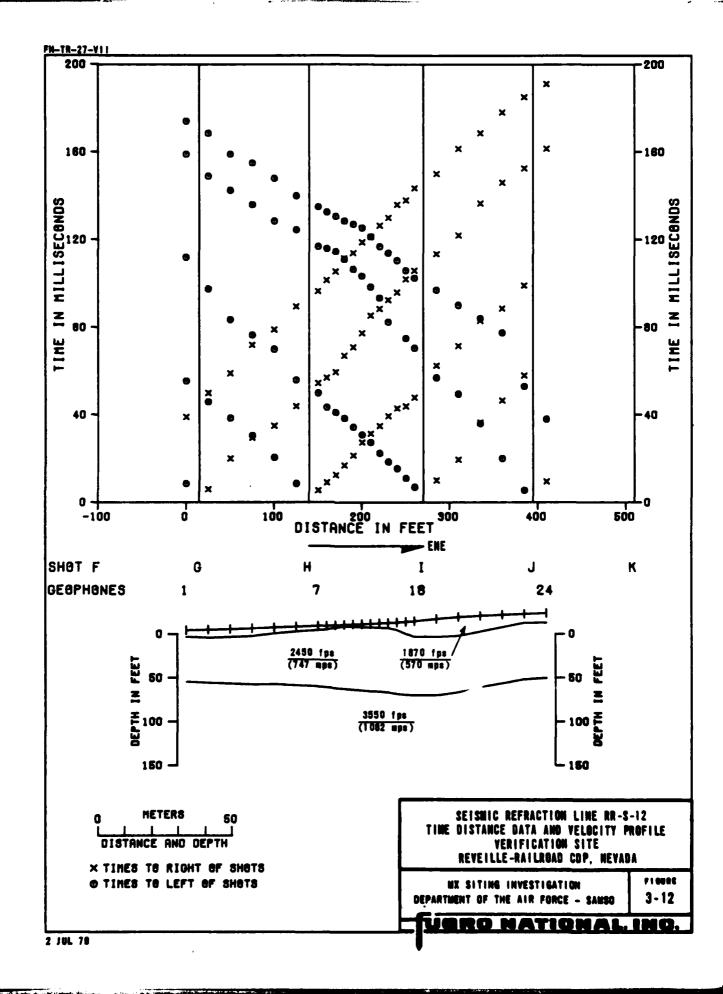


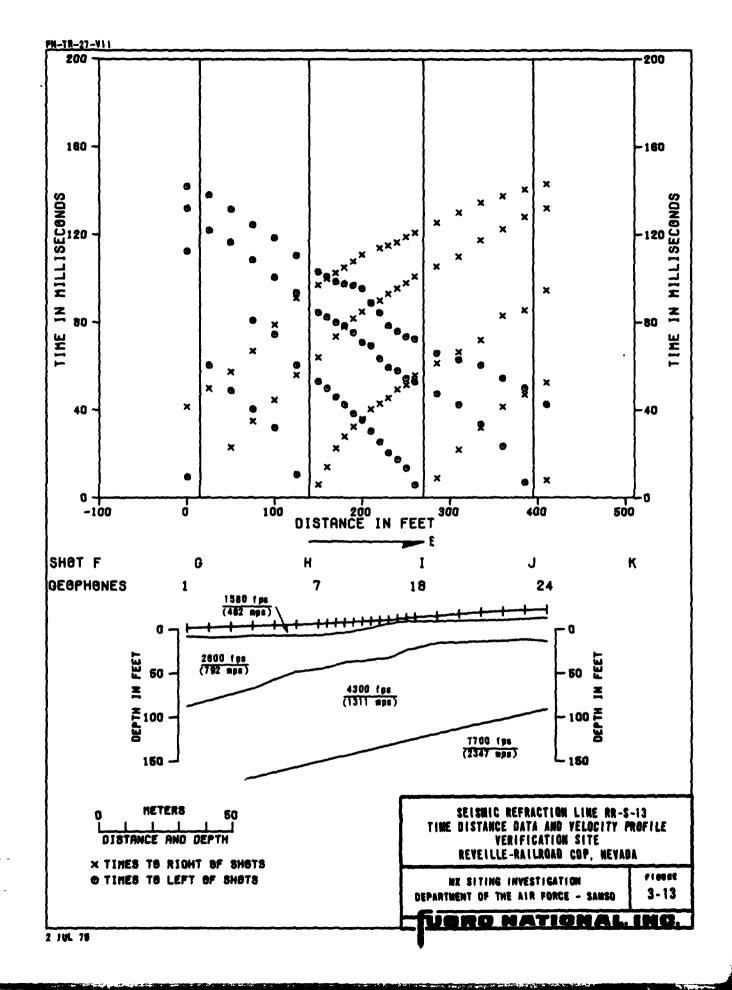


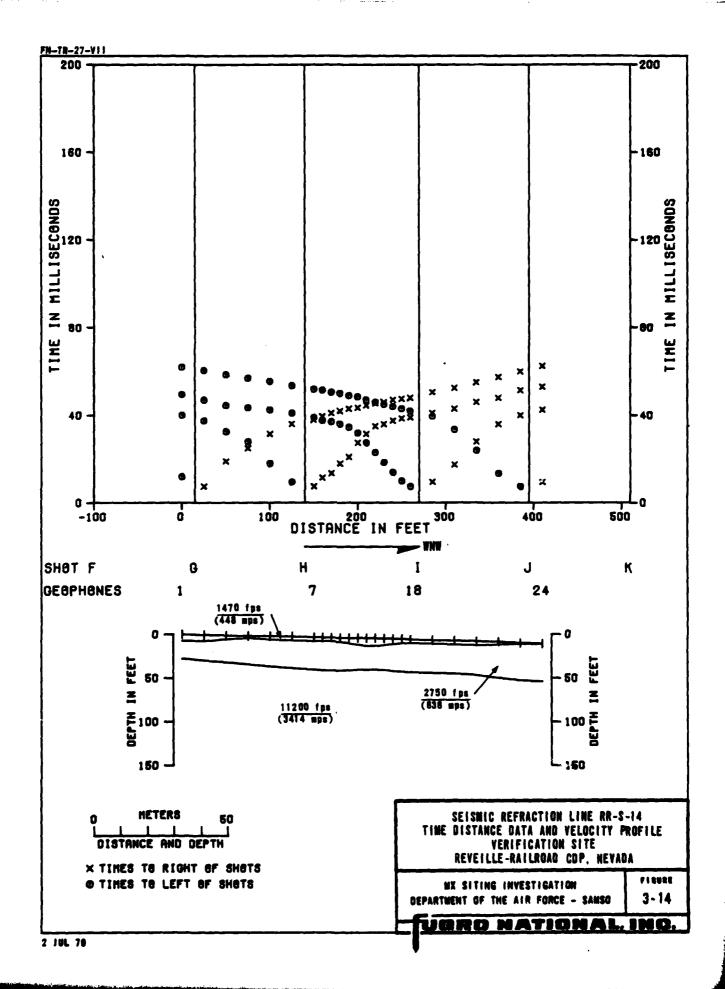


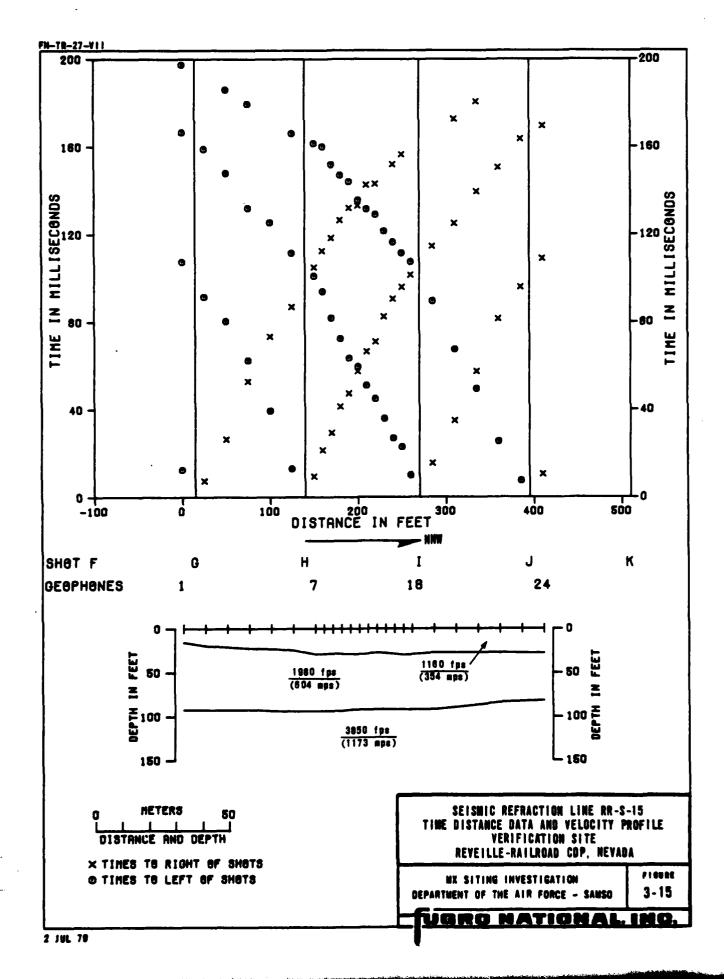


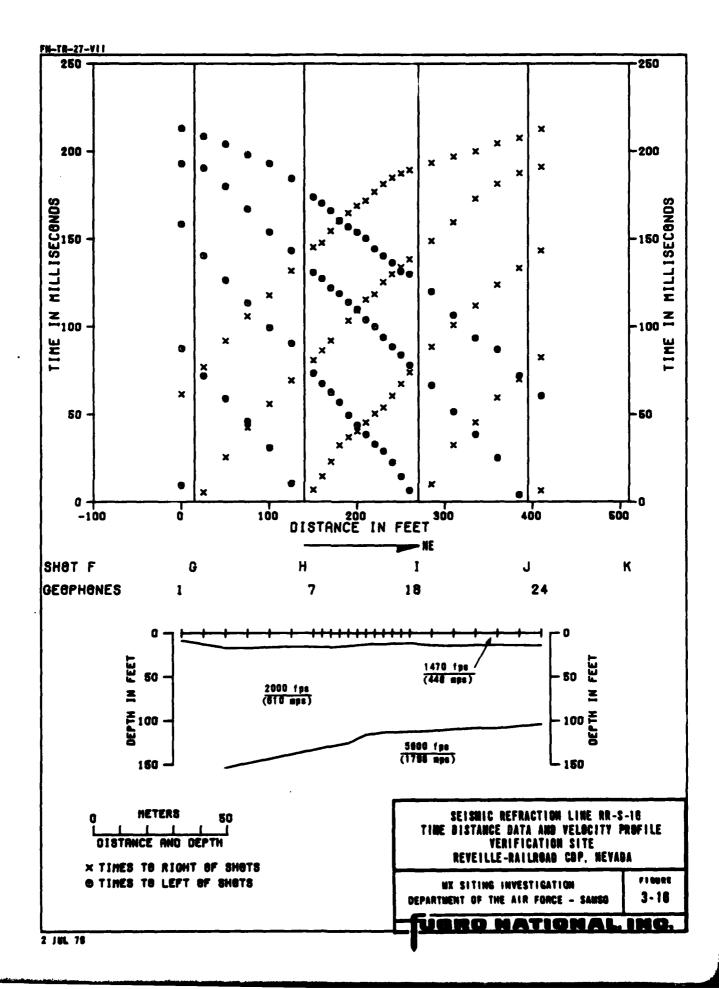












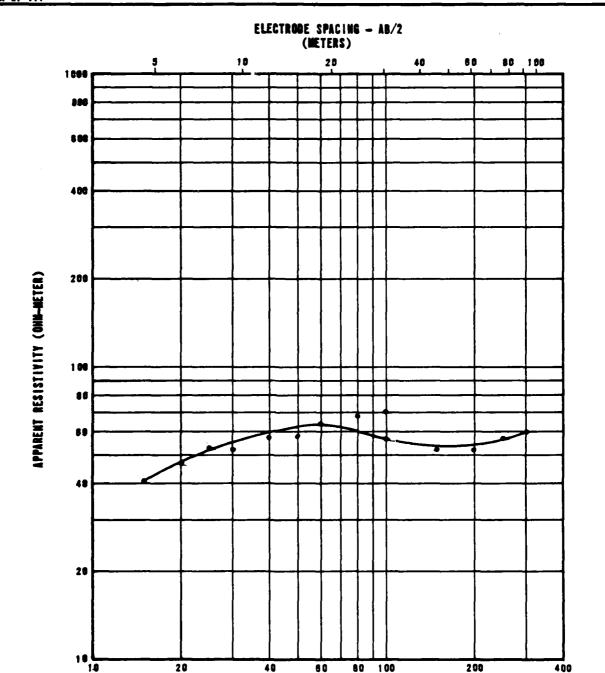
SECTION 4.0
ELECTRICAL RESISTIVITY DATA

## EXPLANATIONS OF ELECTRICAL RESISTIVITY DATA

Each figure in this section presents the data obtained from a resistivity sounding and a tabulated model of resistivity layers that would produce a curve similar to the observed curve.

The upper portion of the figures is a graph in which measured apparent resistivity values in ohm-meters are plotted versus one-half the distance between the current electrodes.

The interpreted model tabulated at the bottom of the page shows a combination of true resistivity layers and thicknesses obtained by matching theoretical curves to the field curve.



ELECTRODE SPACING - AB/2
(FEET)

	INTERPRE	TED MODEL
LAYER DEPTH   RESISTIVITY VALUE		RESISTIVITY VALUES
FEET	METERS	OHM-METER
0	0	30
5	2	70
51	16	30
194	32	100
194	32	100
	1	1

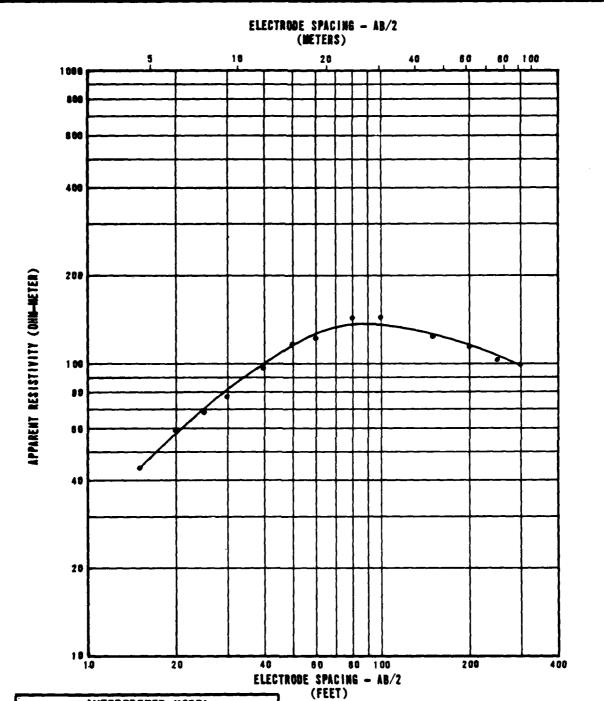
RESISTIVITY SOUNDING RR-R-1
SOUNDING CURVE AND INTERPRETATION
VERIFIE TON SITE
REVEILLE-RAILROAD CDP, NEVADA

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	INTERPRETED MODEL		
LAYE	LAYER DEPTH RESISTIV		
FEET	METERS	OH#-METER	
0	0	25	
6	2	110	
11	3	500	
23	7.	160	
68	21	75	

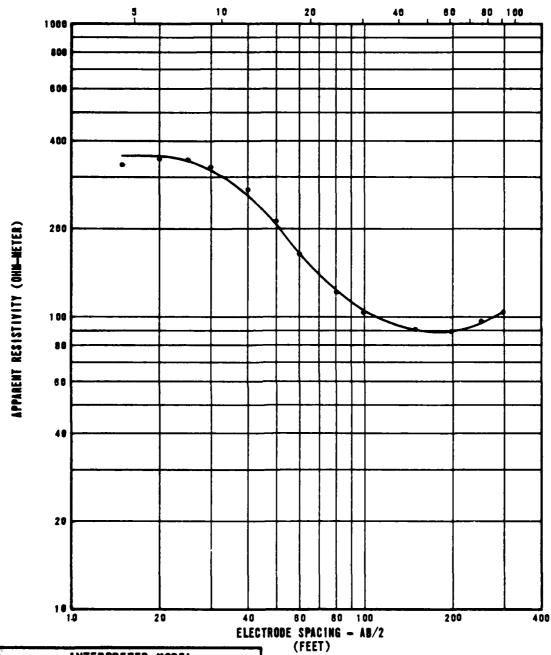
RESISTIVITY SOUNDING RR-R-2 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE REVEILLE-RAILROAD COP, NEVADA

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4-2

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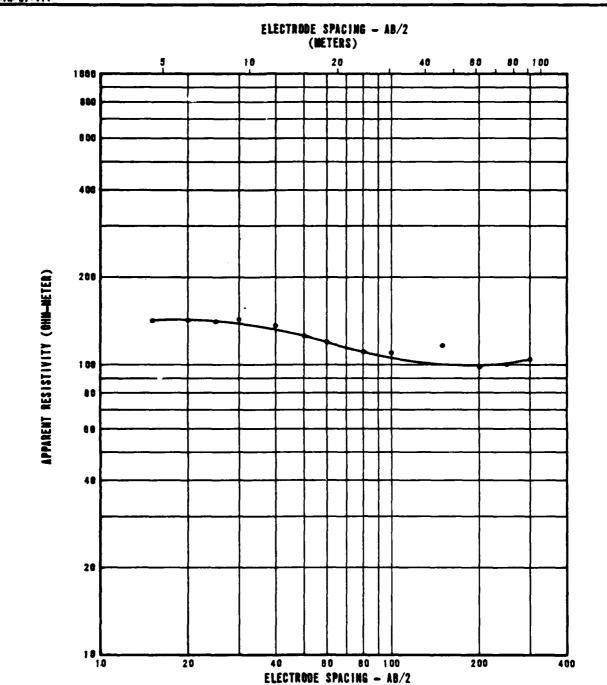
	INTERPRETED MODEL		
LAYE	LAYER DEPTH RESISTIVITY VALUES		
FEET	METERS	OHM-METER	
0	0	420	
19	6	75	

RESISTIVITY SOUNDING RR-R-3
SOUNDING CURVE AND INTERPRETATION
VERIFICATION SITE
REVEILLE-RAILROAD COP, NEVADA

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4-3

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(FEET)

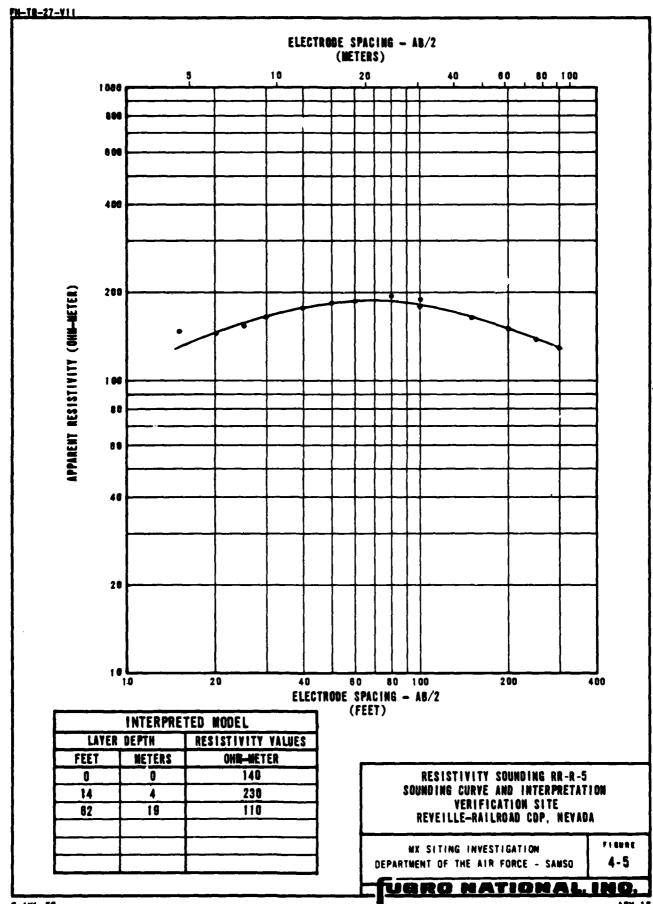
	INTERPRETED MODEL		
LAYE	R DEPTH	RESISTIVITY VALUES	
FEET	METERS	OHR-METER	
0	0	140	
30	8	90	
142	43	130	

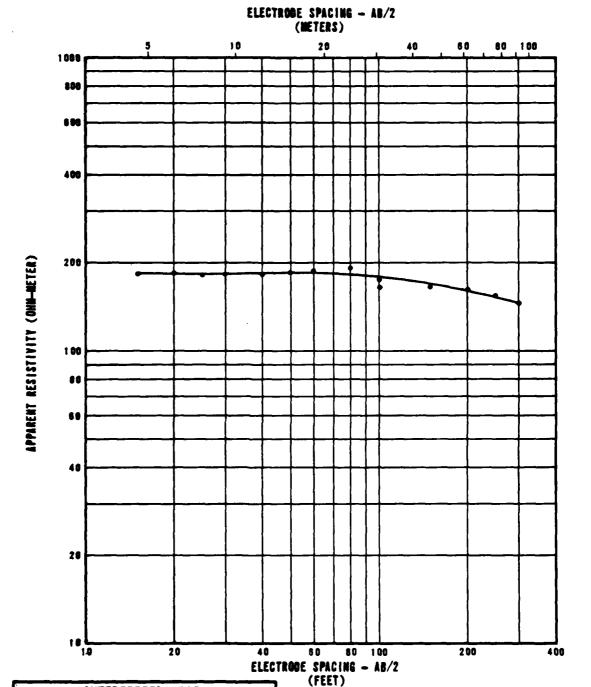
RESISTIVITY SOUNDING RR-R-4
SOUNDING CURVE AND INTERPRETATION
VERIFICATION SITE
REVEILLE-RAILROAD COP, NEVADA

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAWSD

FIGURE 4-4

<u>ugro national inc</u>





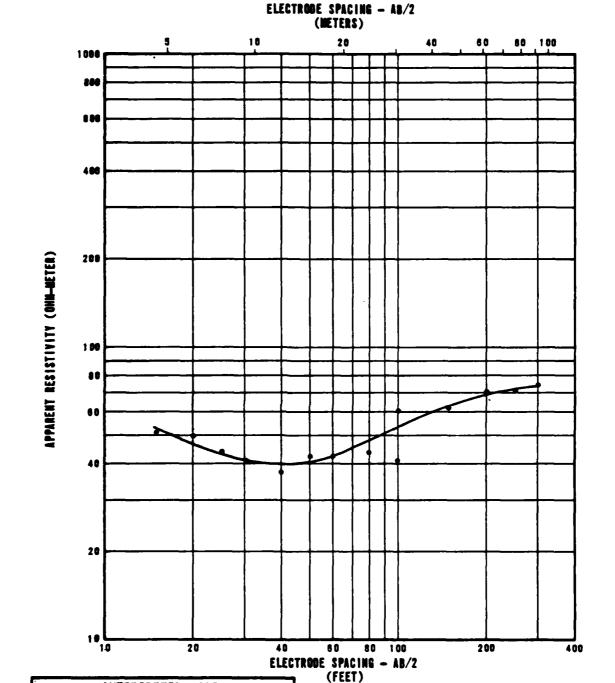
	INTERPRETED MODEL		
LAYEI	LAYER DEPTH RESISTIVITY V		
FEET	METERS	OHM-METER	
0	0	180	
130	40	118	
		]	

RESISTIVITY SOUNDING RR-R-8
SOUNDING CURVE AND INTERPRETATION
VERIFICATION SITE
REVEILLE-RAILROAD CDP, NEVADA

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DEPARTMENT OF THE AIR FORCE - SAMSO

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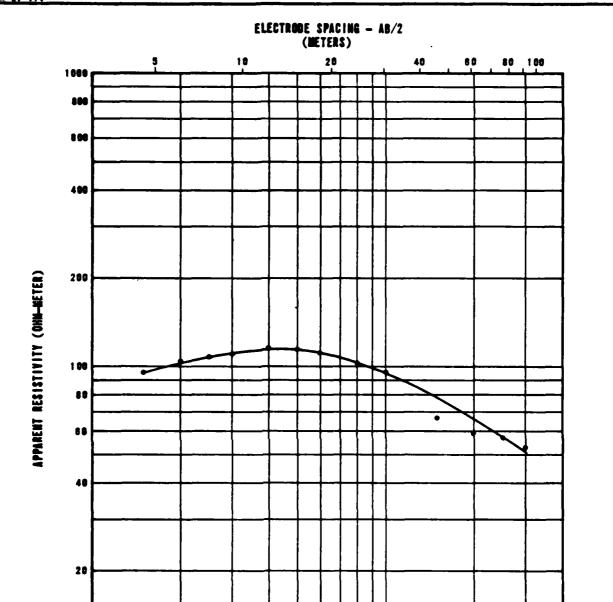
	INTERPRE	TED MODEL
LAYER DEPTH RESISTIVITY VALUE		RESISTIVITY VALUES
FEET	METERS	OHM-METER
0	0	60
8_	2	35
44	13	110
103	31	75
	1	1

RESISTIVITY SOUNDING RR-R-7
SOUNDING CURVE AND INTERPRETATION
VERIFICATION SITE
REVEILLE-RAILROAD COP, NEVADA

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UGRO NATIONAL INC



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ELECTROBE SPACING - AB/2
(FEET)

INTERPRETED MODEL

LAYER DEPTH RESISTIVITY VALUES

FEET METERS OHM-METER

0 0 90
11 3 156
48 15 50

1.0

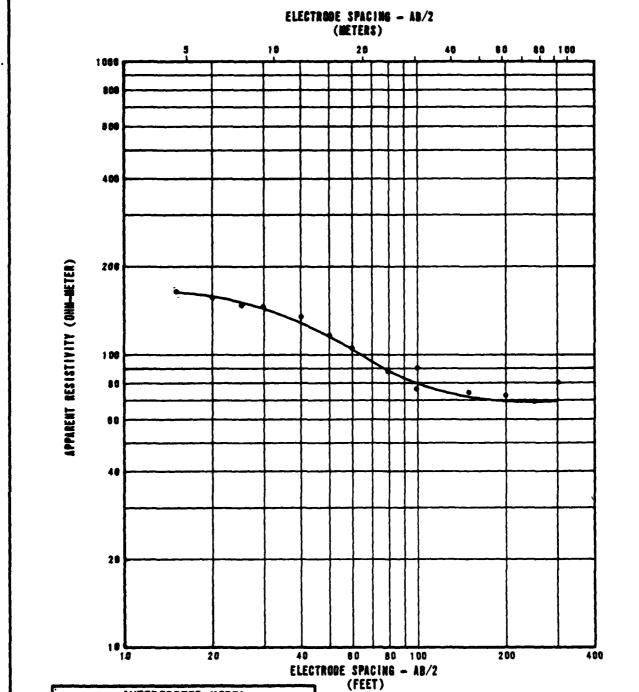
RESISTIVITY SOUNDING RR-R-B
SOUNDING CURVE AND INTERPRETATION
VERIFICATION SITE
REVEILLE-RAILROAD CDP, NEVADA

200

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FIGURE 4-P

UBRO NATIONAL INC.



	INTERPRETED MODEL		
LAYE	R DEPTH	RESISTIVITY VALUES	
FEET	METERS	OHM-METER	
9	0	170	
20	8.	70	

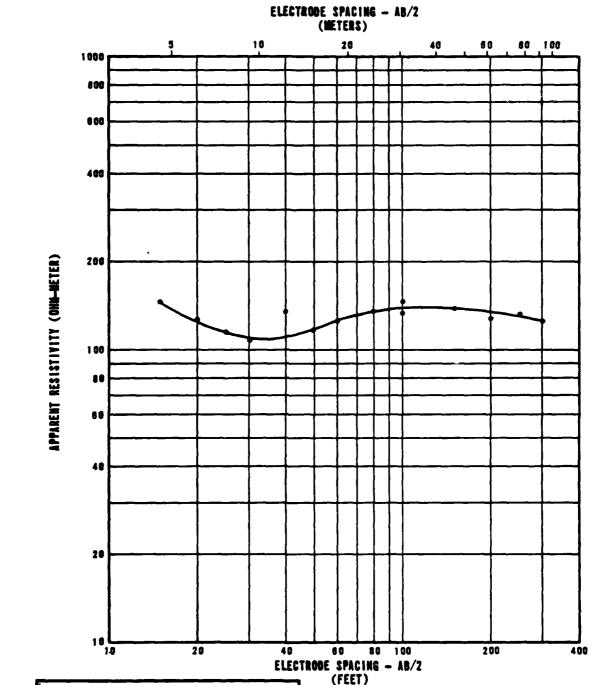
RESISTIVITY SOUNDING RR-R-9
SOUNDING CURVE AND INTERPRETATION
VERIFICATION SITE
REVEILLE-RAILROAD CDP, NEVADA

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FIGURE

4 -9

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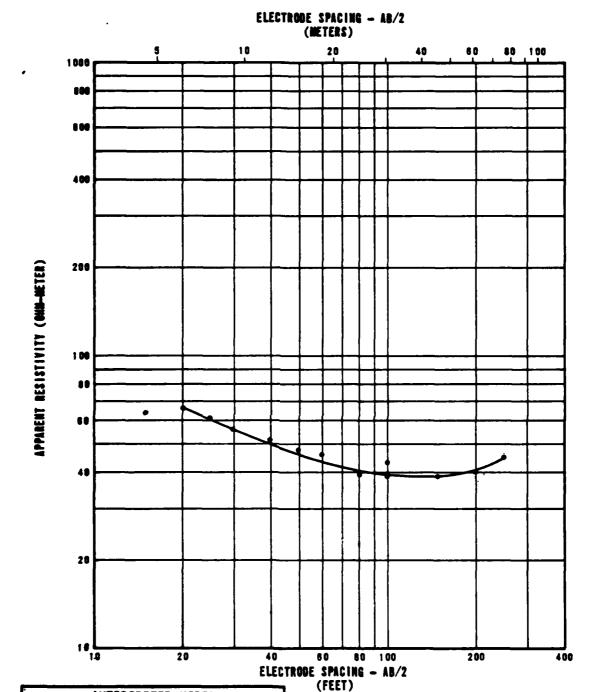
	INTERPRETED MODEL		
LAYE	LAYER DEPTH RESISTIVITY VALUE		
FEET	METERS	OHR-METER	
1	0	170	
8	3	75	
30	9	330	
55	17	100	

RESISTIVITY SOUNDING RR-R-10
SOUNDING CURVE AND INTERPRETATION
VERIFICATION SITE
REVEILLE-RAILROAD CDP, NEVADA

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71 EURE 4-10

**UBRO NATIONAL IN** 



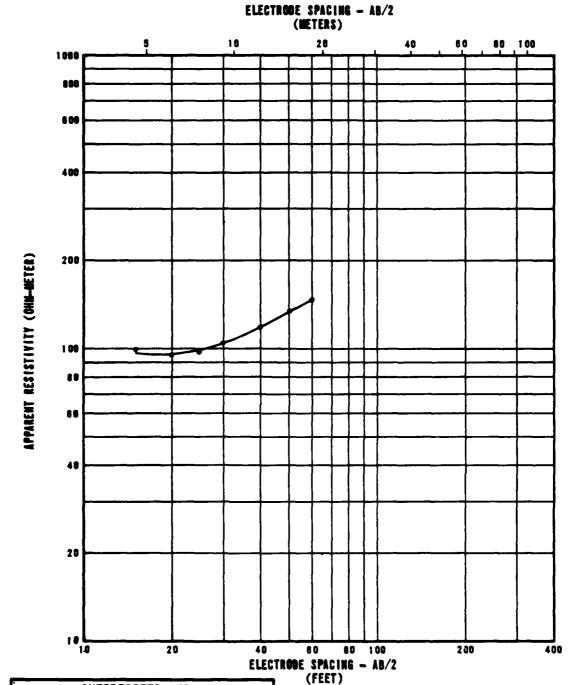
	INTERPRETED MODEL		
LAYE	DEPTH	RESISTIVITY VALUES	
FEET	METERS	OH#-METER	
0	0	75	
18	5	25	
151	48	55	

RESISTIVITY SOUNDING RR-R-11
SOUNDING CURVE AND INTERPRETATION
VERIFICATION SITE
REVEILLE-RAILROAD CDP, NEVADA

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4-11

<u>ubro national inc</u>



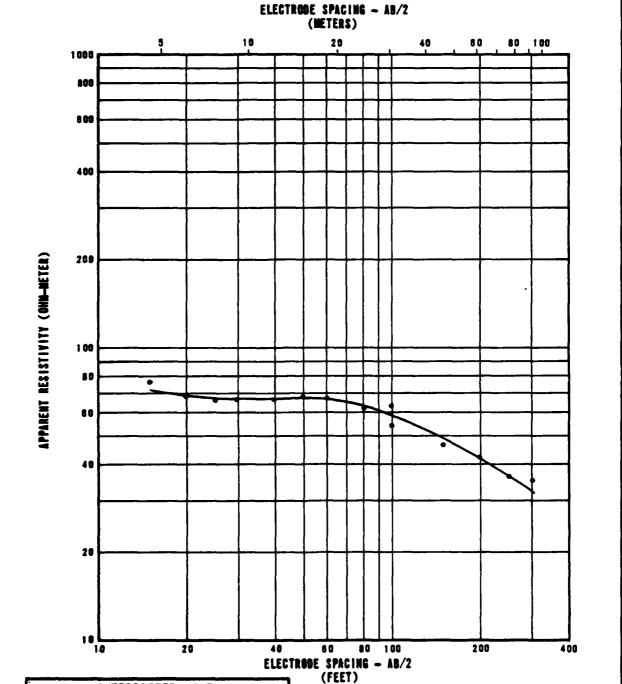
	INTERPRETED MODEL LAYER DEPTH   RESISTIVITY VALUES		
LAYE			
FEET	METERS	OHIR-METER	
g'	0	95	
28	9	290	

RESISTIVITY SOUNDING RR-R-12 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE REVEILLE—RAILROAD COP, NEVADA

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4-12

<u>UBRO NATIONAL INC.</u>



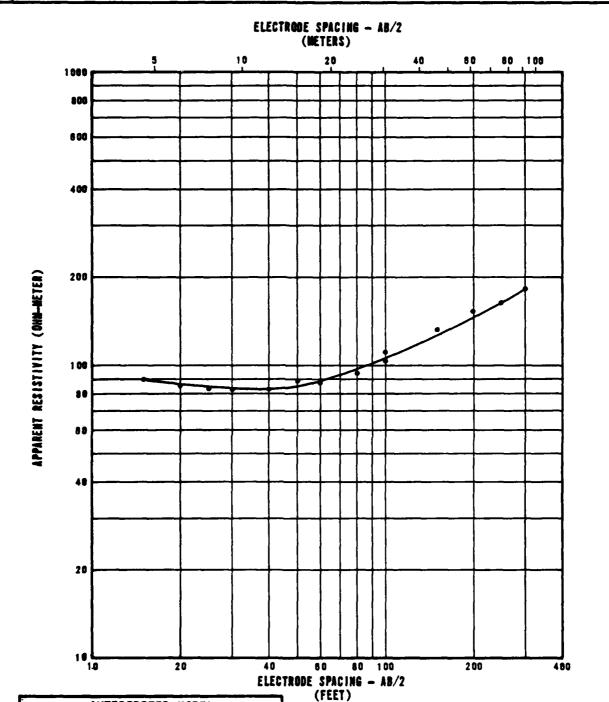
	INTERPRETED MODEL LAYER DEPTH RESISTIVITY VALUES		
LAYE			
FEET	METERS	OHIS-METER	
	0	76	
78	23	25	

RESISTIVITY SOUNDING RR-R-13
SOUNDING CURVE AND INTERPRETATION
VERIFICATION SITE
REVEILLE-RAILROAD CDP, NEVADA

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4-13

**UGRO NATIONAL INC.** 



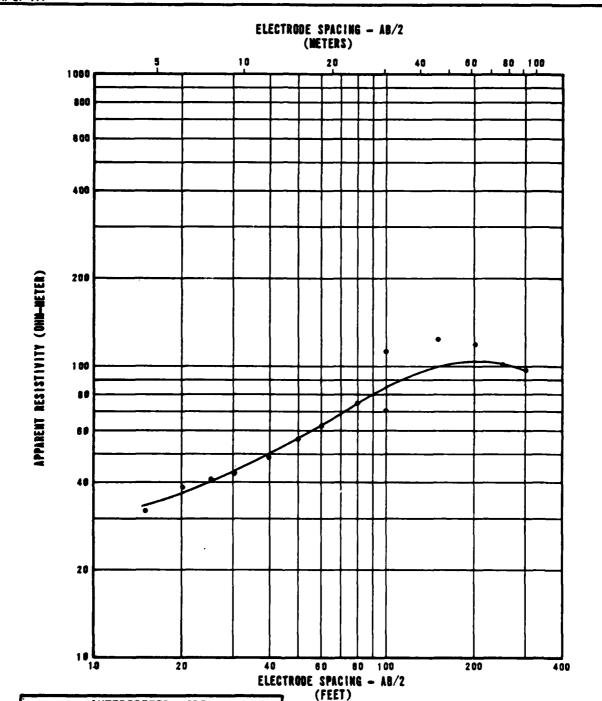
	INTERPRE	TED MODEL
LAYE	R DEPTH	RESISTIVITY VALUES
FEET	METERS	OH#-METER
0	0	90
18	5	70
34	10	90
67	20	280

RESISTIVITY SOUNDING RR-R-14
SOUNDING CURVE AND INTERPRETATION
VERIFICATION SITE
REVEILLE-RAILROAD COP, NEVADA

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4-14

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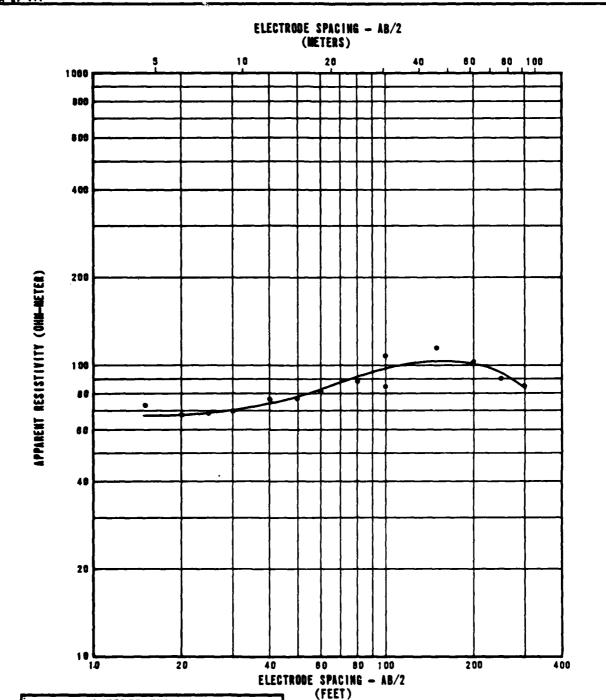
	INTERPRETED MODEL										
LAYE	R DEPTH	RESISTIVITY VALUES									
FEET	METERS	OHM-METER									
0	0	30 13Q									
15	5										
198	60	45									
	T										

RESISTIVITY SOUNDING RR-R-15
SOUNDING CURVE AND INTERPRETATION
VERIFICATION SITE
REVEILLE-RAILROAD COP, NEVADA

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4-15

UBRO NATIONAL INC.



	INTERPRETED MODEL										
LAYE	R DEPTH	RESISTIVITY VALUES									
FEET	METERS	OHM-METER									
0.	0	65									
26	8	120.									
186	57	25									

RESISTIVITY SOUNDING RR-R-18
SOUNDING CURVE AND INTERPRETATION
VERIFICATION SITE
REVEILLE-RAILROAD CDP, NEVADA

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SECTION 5.0 GRAVITY DATA

## EXPLANATIONS OF GRAVITY DATA

Gravity data were not available in time (prior to June 1979) for incorporation into this report. A supplemental report containing gravity data and results will be issued at a later date.

SECTION 6.0

BORING LOGS

## EXPLANATIONS OF BORING, TRENCH, AND TEST PIT LOGS

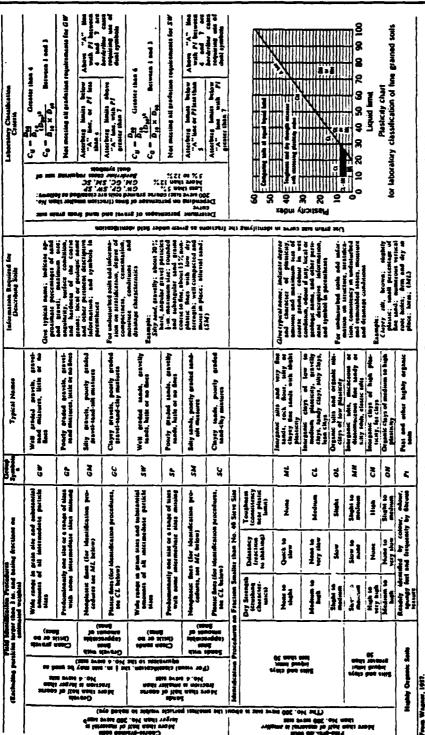
All data from borings, trenches, and test pits are presented on standard Fugro National logs in Sections 6.0 and 7.0. The following explanations are provided as a key to the logs.

A. Designations - Borings, trenches, and test pits are identified as follows:

WW-B-1

WW - abbreviation for the site (e.g., WW-Whirlwind)

- B abbreviation for activity (e.g., B-boring, T-trench, P-test pit)
- 1 number of activity
- B. Sample Type Different sampling techniques were used and the symbols are explained at the bottom of the boring logs. For details of sampling techniques, see Section A5.0 of Appendix in Volume I. Horizontal lines, to scale, indicate the depth where sampling was attempted.
- C. Percent Recovery The numbers shown represent the ratio (in percent) of the soil sample recovered in the sampler to the full penetration of the sampler.
- D. N Value Corresponds to standard penetration resistance, which is number of blows required to drive a standard split-spoon sampler for the second and third of three 6-inch (15 cm) increments with a 140-pound (63.5 kg) hammer falling 30 inches (76 cm) (ASTM D 1586-67).
- E. Depth Corresponds to depth below ground surface in meters and feet.
- F. Lithology Graphic representation of the soil and rock types.



designated by combinations of group symbols. For example GW-GC, well graded From Wigner, 1937.

Sandery, Leadplanders. Such processing characteristics of two groups and
Sandery March also to the Chart to U.S. sendered.

TABLE

6-1

These precidents are to be purioused on the mean big. 40 user use particle, appealments by the first precident processor of the processor of t

Transfers (Conscissors and particles their mercies with the tests.)

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Aler removing particles began their in the form.

Transfers (Conscissors and patricles their their their)

to list about one "ball stick being in such an out-of-patricle to the conscissory of purity. If the offy, units must be saided and it stick, the options purity. If the offy, units must be taked and it stick, the options of their control of the control of their contro

UNIFIED SOIL CLASSIFICATION SYSTEM

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- G. USCS Unified Soil Classification System (see Table 6-1 for complete details) symbols.
- H. Soil Description Except in cases where samples were classified based on laboratory test data, the descriptions are based on visual classification. The procedures outlined in ASTM D 2487-69, Classification of Soils for Engineering Purposes, and D 2488-69, Description of Soils (Visual-Manual Procedure) were followed. Solid lines across the column indicate known change in strata at the depth shown.

Definitions of some of the terms and criteria to describe soils and conditions encountered during the exploration follow.

Gradation: A coarse-grained soil is well graded if it has a wide range in grain size and substantial amounts of most intermediate particle sizes.

Poorly graded indicates that the soil consists predominantly of one size (uniformly graded) or has a wide range of sizes with some intermediate sizes obviously missing (gap-graded).

Moisture: Dry - no feel of moisture
Slightly Moist - much less than normal moisture
Moist - normal moisture for soil
Very Moist - much greater than normal
moisture
Wet - for soils below the water
table (if known)

Consistency: Consistency descriptions of coarse-grained soils (GW, GP, GM, GC, SW, SP, SM, SC) are as follows.

	N Value
Consistency	(ASTM D 1586-67)
Very Loose	0 - 4
Loose	4 - 10
Medium Dense	10 - 30
Dense	30 - 50
Very Dense	>50

Consistency descriptions of fine-grained soils (ML, CL, MH, CH,) are as follows:

Consistence		strength	miala cuia-
Consistency	(ksf)	Kn/m <sup>2</sup> )	Field Guide
Very Soft	0.25	12	Sample with height equal to twice the diameter, sags under own weight
Soft	0.25- 0.50	12 - 24	Can be squeezed between thumb and forefinger
Firm	0.50- 1.00	24- 48	Can be molded easily with fingers
Stiff	1.00-2.00	48- 96	Can be imprinted with slight pressure from fingers
Very Stiff	2.00- 4.00	96- 192	Can be imprinted with considerable pressure from fingers
Hard	over 4.00	over 192	Cannot be im- printed by fingers
_		_	

Grain Shape: Angular - particles have sharp edges and relatively plane sides with unpolished surfaces.

Subangular - particles are similar to angular but have somewhat rounded edges.

Subrounded - particles exhibit nearly plane sides but have well-rounded corners and edges.

Rounded - particles have smoothly curved sides and no edges.

Calcareous: Containing calcium carbonate; presence of calcium carbonate is commonly identified on the basis of reaction with dilute hydrochloric acid.

Caliche : Soils cemented by porous calcium carbonate and/or other soluble minerals by upward-moving solutions.

Degree of

Cementation: (Stages of development of caliche profile)

Stage	Gravelly Soils	Nongravelly Soils
I	Thin, discontinu- ous pebble coatings	Few filaments or faint coatings
II	Continuous pebble coatings, some interpebble fill-ings	Few to abundant nodules, flakes, filaments
III	Many interpebble fillings	Many nodules and internodular fillings
IA	Laminar horizon overlying plugged horizon	Increasing carbon- ate impregnation

Secondary Material

: Example - Sand with trace to some silt

Trace - 5-12% (by dry weight)
Little - 13-20% (by dry weight)
Some - >21% (by dry weight)

Plasticity: Plasticity index is the range of water content, expressed as a percentage of the weight of the oven-dried soil, through which the soil is plastic. It is defined as the liquid limit minus the plastic limit. Descriptive ranges used on the logs include:

Nonplastic (PI, 0 - 4) Slightly Plastic (PI, 4 - 15) Medium Plastic (PI, 15 - 30) Highly Plastic (PI, >31)

Cobbles and Boulders

A cobble is a rock fragment, usually rounded by weathering or abrasion, with an average diameter ranging between 3 and 12 inches (8 and 30 cm).

A boulder is a rock fragment, usually rounded by weathering or abrasion, with an average diameter of 12 inches (30 cm) or more.

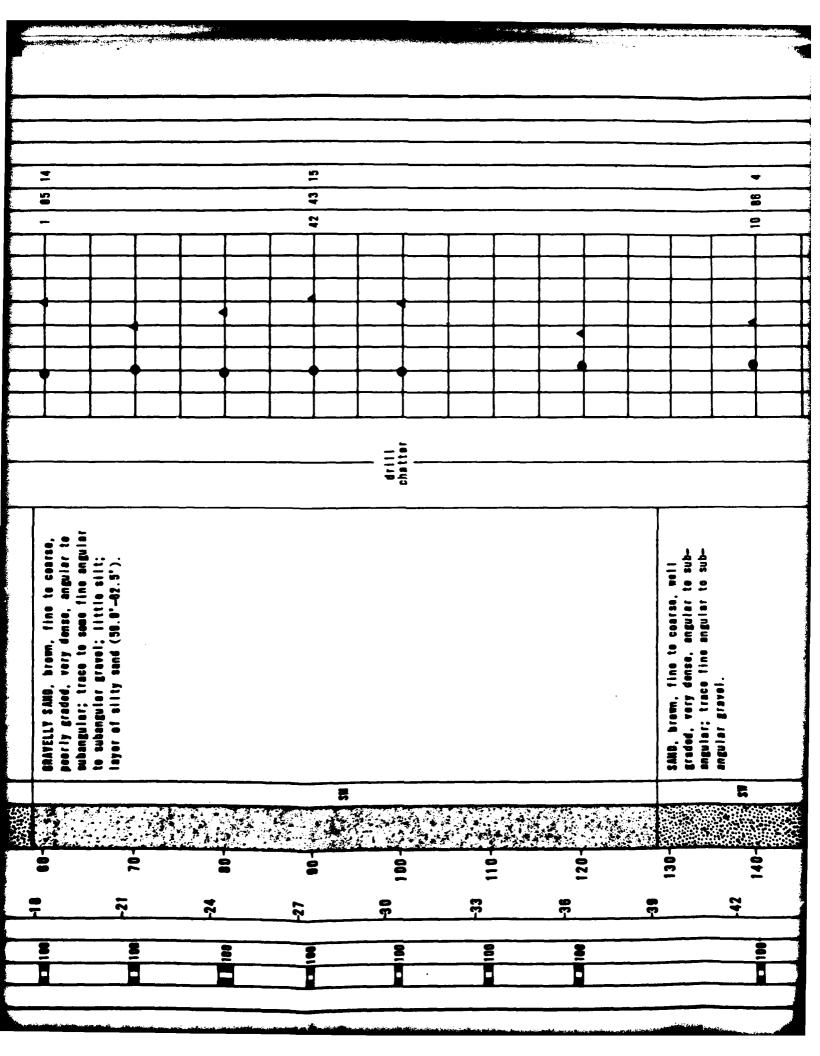
- I. Remarks This column was provided on boring and trench logs for comments regarding drilling difficulty, number and size of cobbles or boulders encountered, trench wall stability, loss of drilling fluid in the boring, and other conditions encountered during drilling and excavations.
- J. Dry Density and Moisture Content The boring logs include a graphical display of laboratory test results for dry density (ASTM D 2937-71) in pounds per cubic foot and kilograms per cubic meter and moisture content (ASTM D 2216-71) in percent from representative samples taken during drilling. The symbols are explained at the bottom of the boring logs.

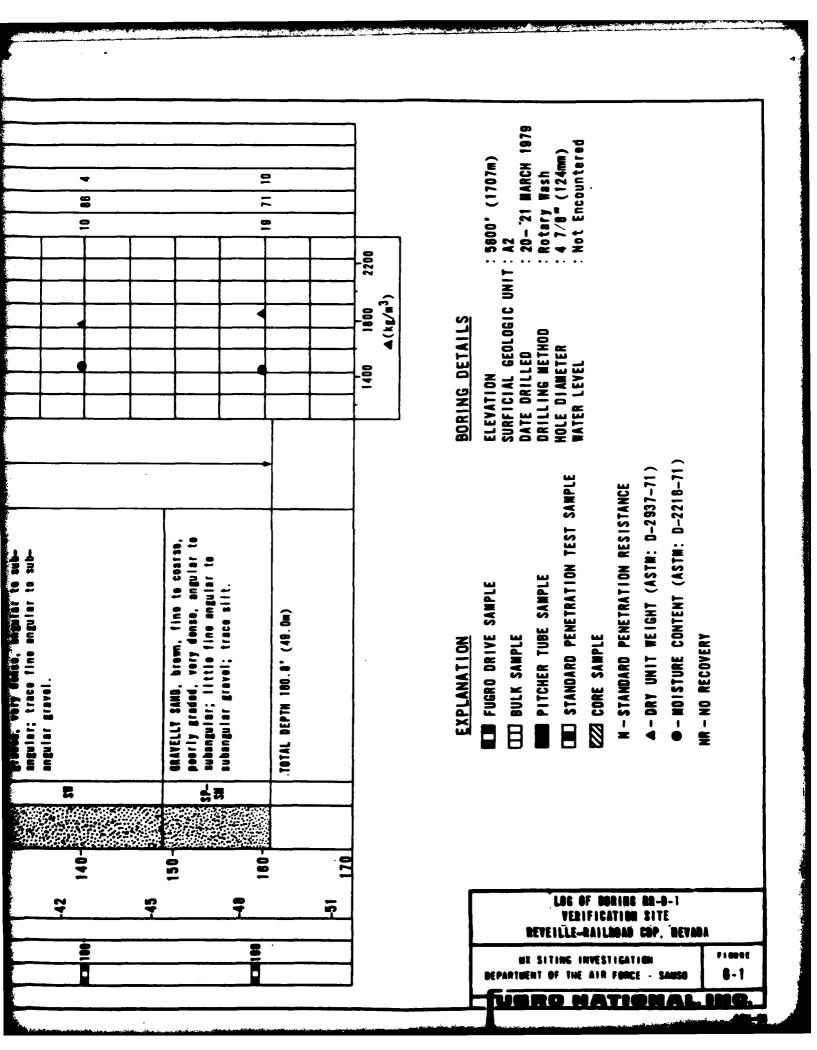
- K. Seive Analysis The numbers represent the percentage by dry weight (ASTM D 422-63) of each of the following soil components:
  - GR Gravel, rock particles that will pass a 3-inch (76 mm) sieve and are retained on No. 4 (4.75 mm) sieve.
  - SA Sand, soil particles passing No. 4 sieve and retained on No. 200 (0.075 mm) sieve.
  - FI Fines, silt or clay, soil particles passing No. 200 sieve.
- L. Atterberg Limits (LL and PI) -
  - LL Liquid Limit, the water content corresponding to the arbitrary limit between the liquid and plastic states of consistency of a soil (ASTM D 423-66).
  - PL Plastic Limit, the water content corresponding to an arbitrary limit between the plastic and the semisolid state of consistency of a soil (ASTM D 424-59).
  - PI Plasticity Index, numerical difference between the liquid limit (LL) and the plastic limit (PL) indicating the range of moisture content within which a soil-water mixture is plastic.
  - NP Nonplastic.
- M. Miscellaneous Information -
  - Elevations indicated elevations on the logs are estimated from topographic maps of the study area, within an accuracy of half the contour interval.
  - Surficial
    Geologic Unit indicates the surficial geologic unit in which the activity is located.
  - Date Drilled indicates the period from beginning to completion of the activity.
  - Drilling
    Method signifies the type of drilling procedure
    used such as rotary wash.
  - Hole Diameter nominal size of boring drilled.
  - Water Level indicates depth from ground surface to water table where encountered.

Coench Length - length at ground surface of final trench excavation.

Trench
Orientation - bearing of longitudinal trench centerline.

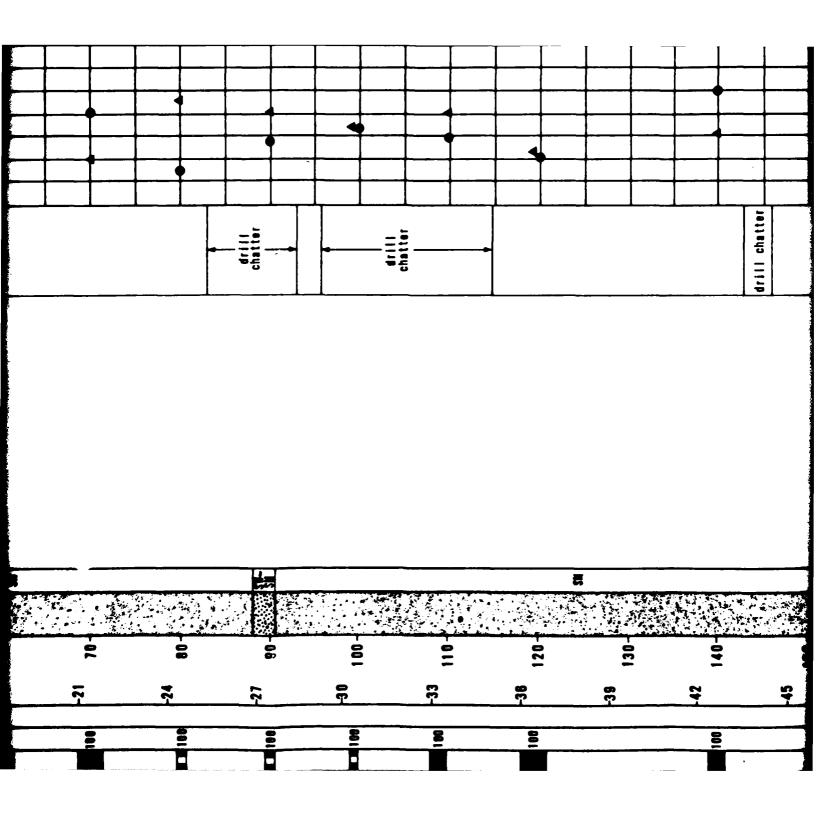
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	SOIL DESCRIPTION		- gat brown, fine to comes.	ingular, calcareous; little te seme	angular gravel; lense of sandy clay (0.5°-1.2°).	T SAND.	BANKS BY TO SUBBRICES. COLORES.	10.5°)			SILTY SAND light brown, fine to coarse poorly graded, very dense, angular to		SAND, light brown, fine to coarse, well graded, very dense, angular to sub-	r; trace		
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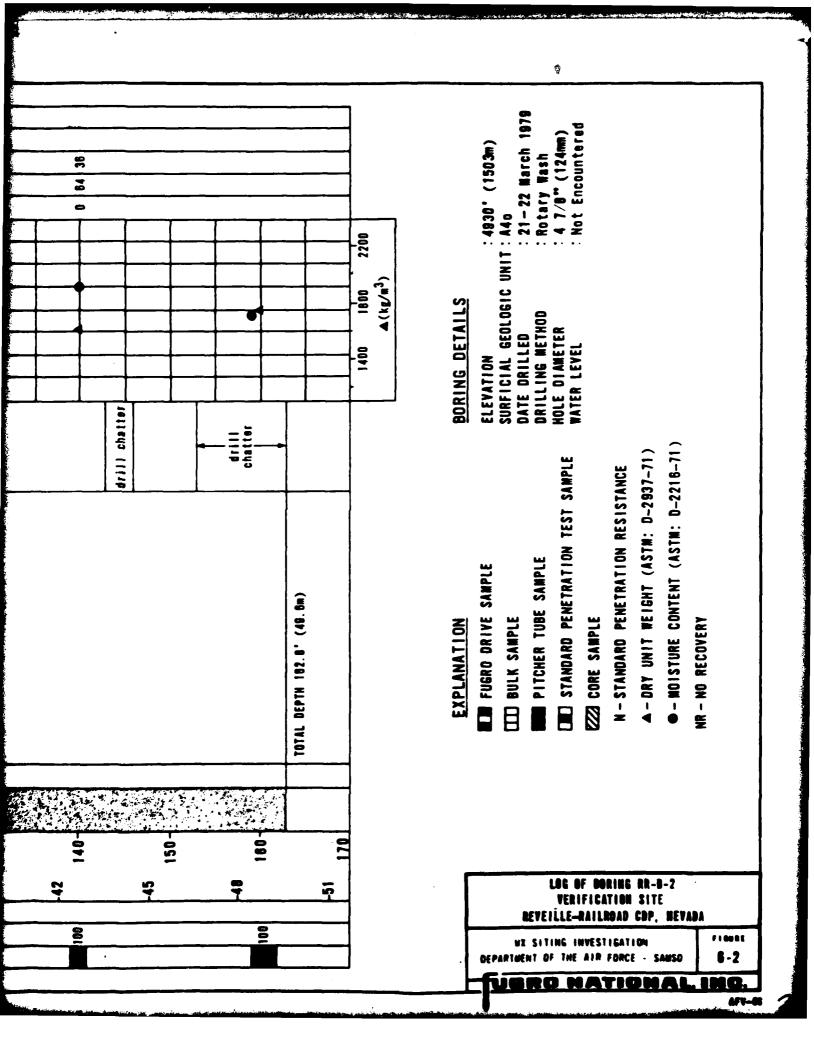




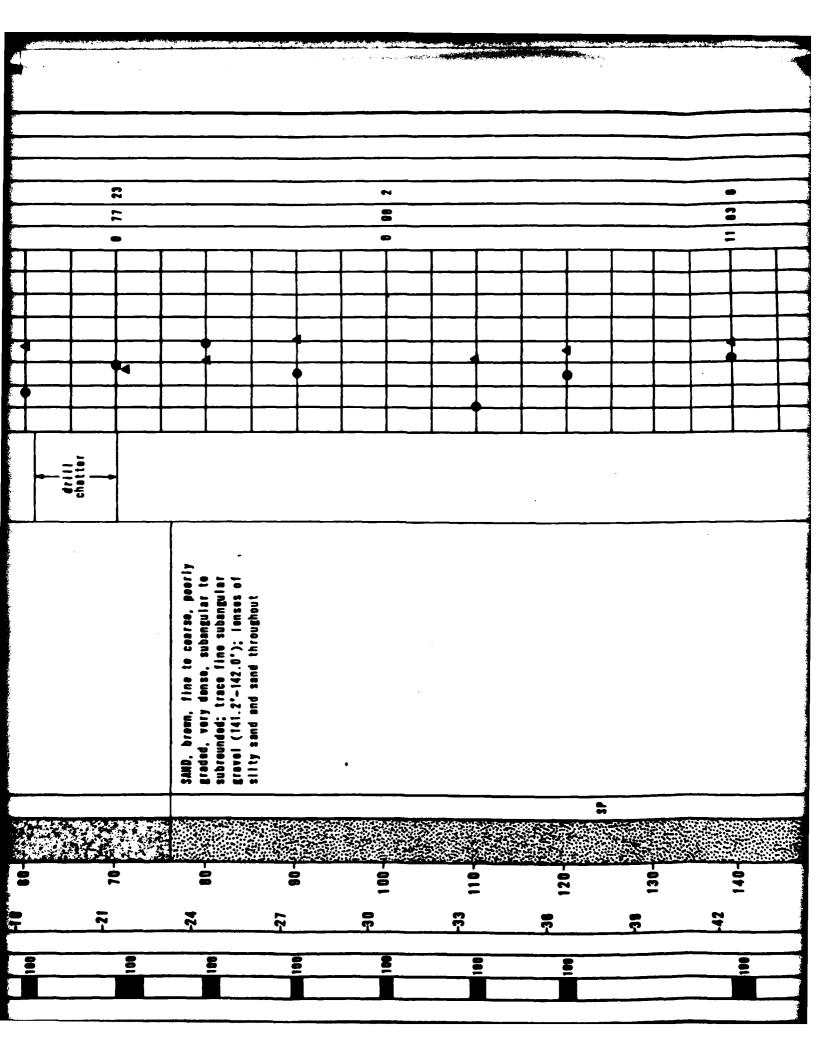
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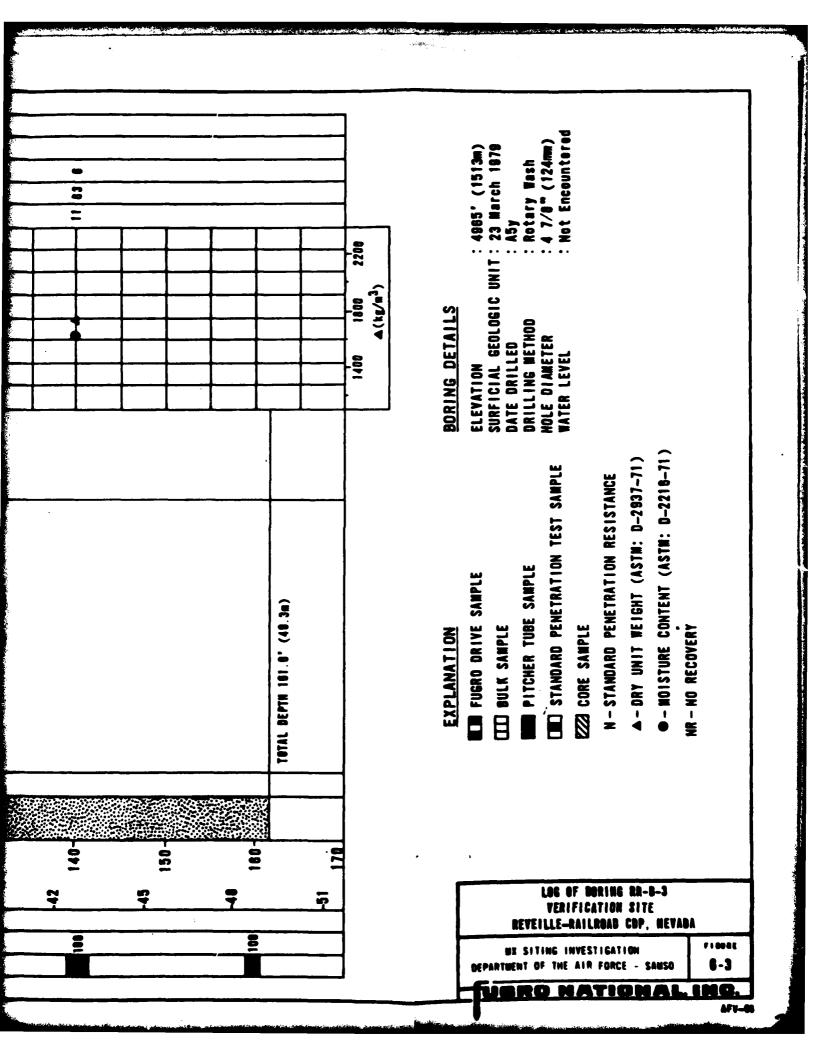
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SOIL DESCRIPTION		SILTY SAND. Doorly grade	SANDY GRAVEL.	rectum conse to conse, angular to sub- recunded; some fine angular to subangular sand; trace silt.	SAND, brown, fine to coarse, poorly graded, dense to very dense, angular	to subsaguist.	SRAVELLY SAND, brown, fine to coarse, well graded, dense to very dense,	gravel.	SANDY SILT, gray brown, very stiff, nonplastic; seme fine to medium sand	SILTY SAMD, brown to gray brown, fine to medium, poorly graded, very dense,	1 2 2	ily sand and silty		
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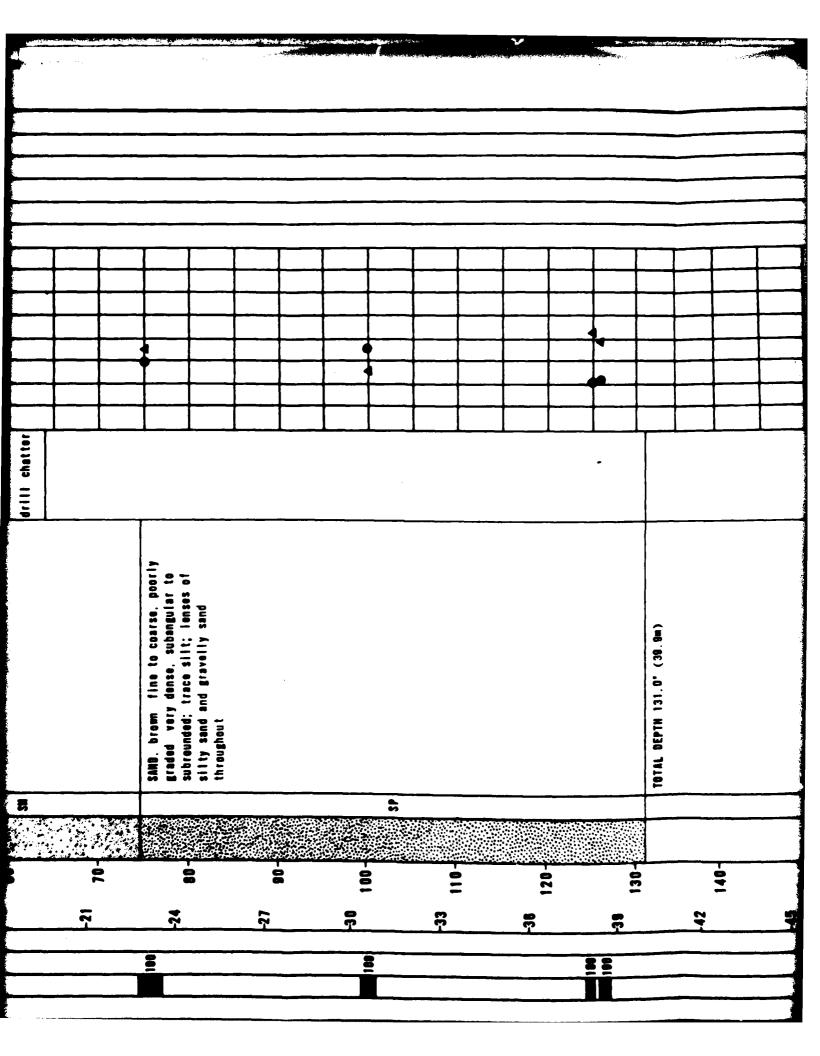
subangula little si te sub-		SILTY SAND, yellow brown, fine to  modium, poorly graded, modium dense to dense, subangular to subrounded, calcarecus; some silt.  BRAVELLY SAND, brown, fine to coorse,		SOLTY SAME, light brown, fine to coarse, poorly graded, very dense, subangular, calcarous; some silt; layer of sand (30.0"-41.3").	
SILTY SAND, brown, fi poorly graded, loose, rounded, calcareous; trace fine subengular rounded gravel.	GRAFELLY SAND, brown, fine to poorly to well graded, medium subangular to subrounded, calc trace to little fine subangula subrounded gravel; trace silt.	SILTY SAND, yellow brown, fine medium , poorly graded, medium to dense, subangular to subreun calcareous; some silt.	subsnguier to subro some fine subsnguie gravel: trace silt.	SILTY SAMO, light brown, flocatso, poorly graded, very subangular, calcarsous; som layer of sand (35.0'-41.3')	

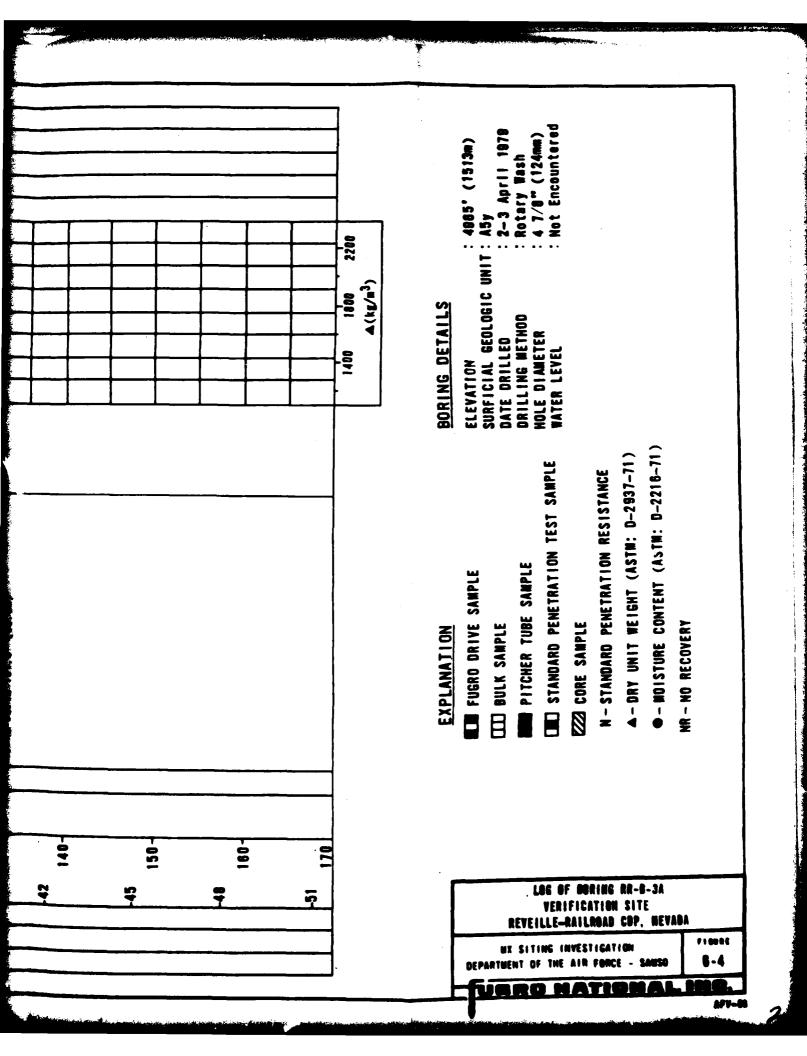




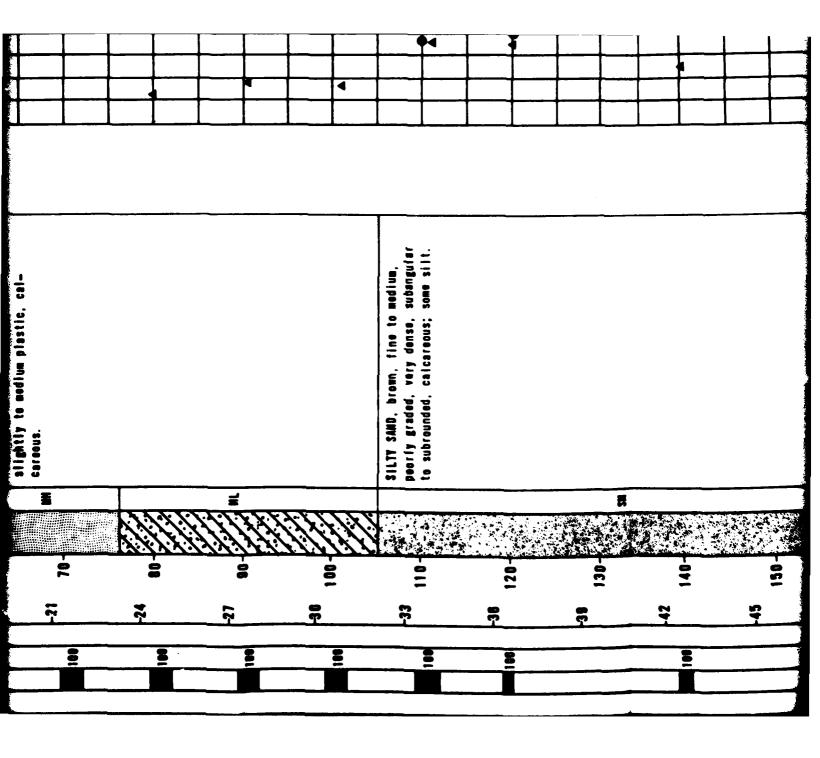
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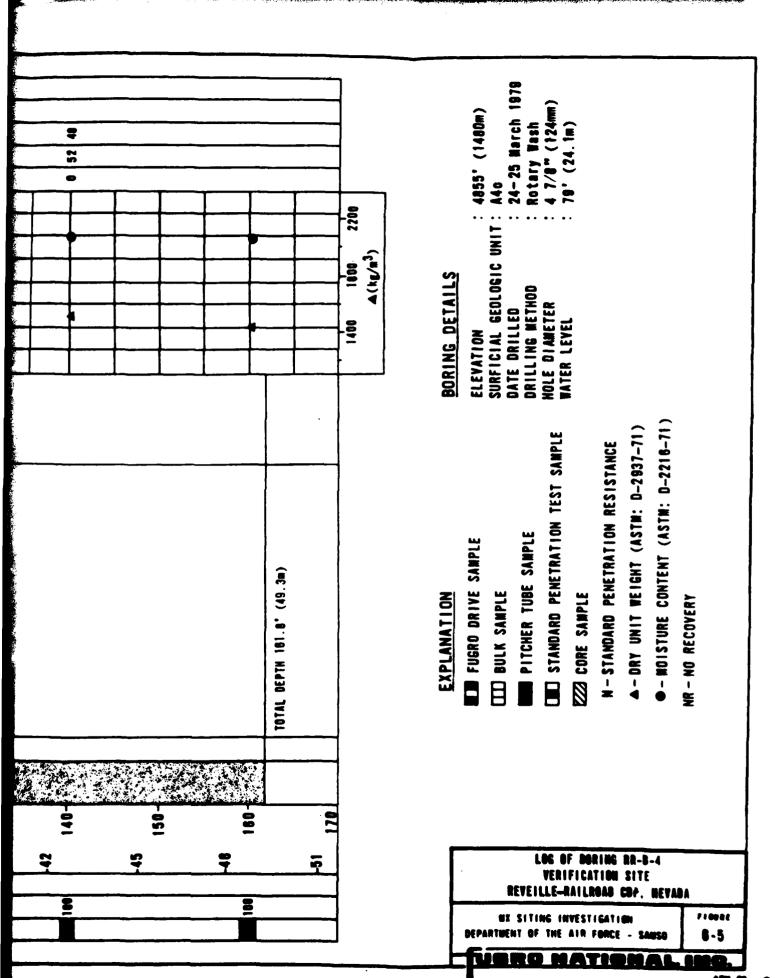
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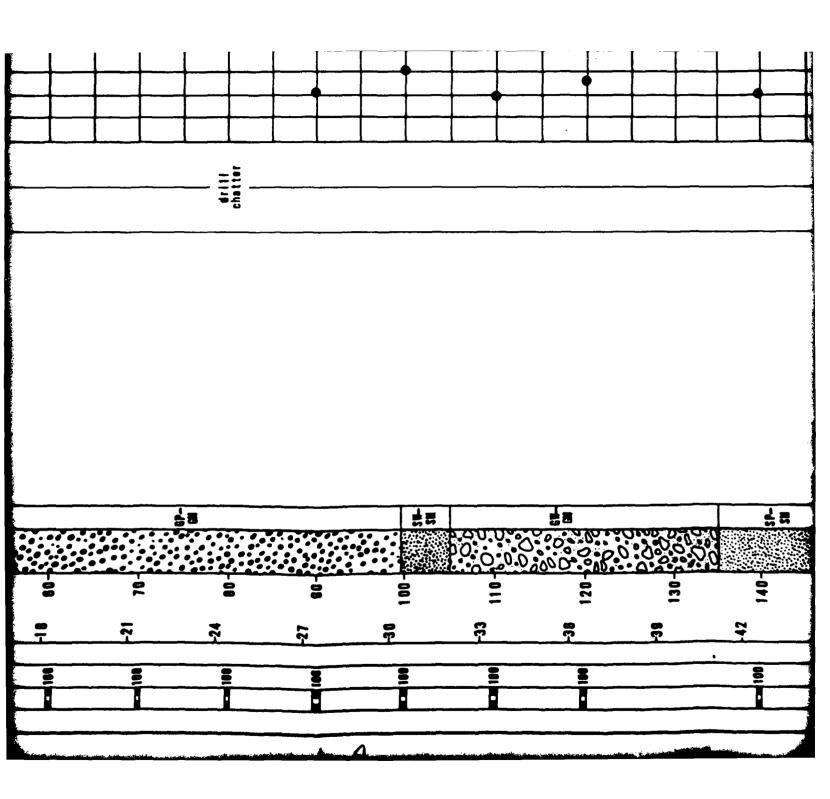


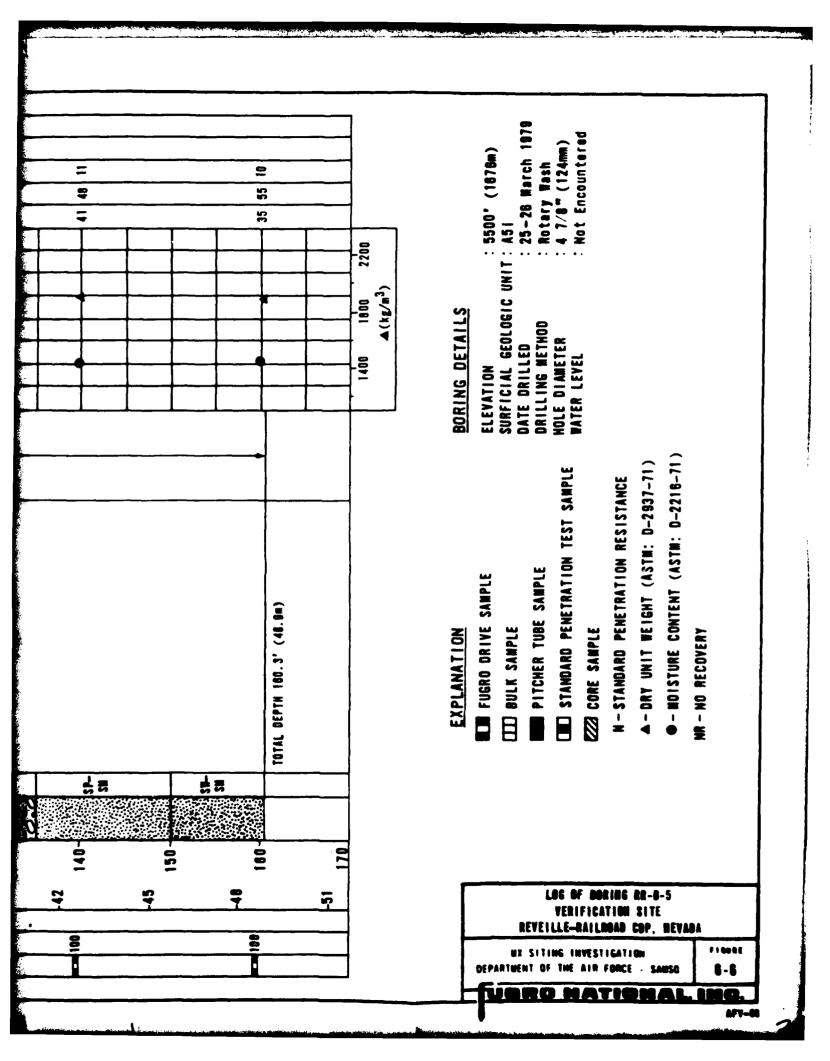
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SOIL DESCRIPTION  SILT, Hight gray, saft to stiff, andium plastic, calcarous; layer of sandy silt (0.0°-2.0°).  Strandy silt (0.0°-2.0°).  Strandy silt (0.0°-2.0°).  Interbedded layers of silt and sake: shift: shift: gray brown to brown, stiff to hard slightly to highly plastic, calcarous; trace to some fine to smedium submnyular to sub- rounded sand.  Same: submnyular to sub- rounded sand.  Same: carous; frace to some silt.  Same: submnyular to sub- rounded sand.  Same: carous; frace to some silt.		<u> </u>	•			<u> </u>				<b></b>					
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T			SILT, light gray, soft to st medium plastic, calcaroous;	CLAVEY SAND, brown, fine to	dense, subangular te subreur calcareeus; little silty cli layer of sand (8.8"-8.5").		SANDY SILT ( SANDY SILT (	slightly to calcareous: to medium su	SAND:	brown, fine graded, dens	subangular t careous; tra		1:		
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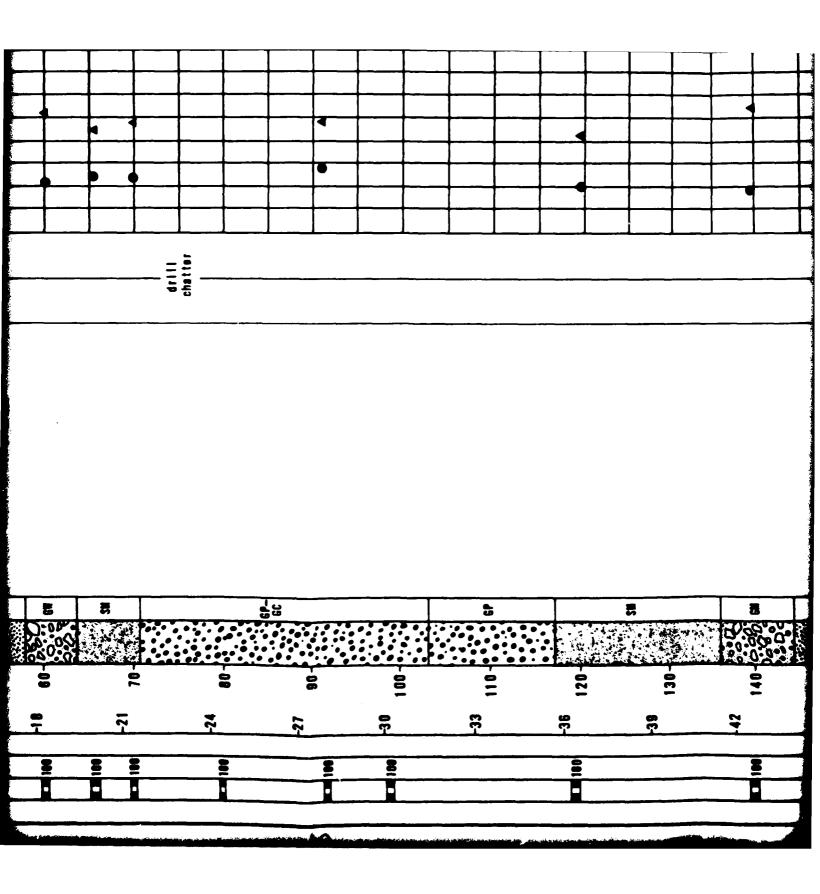
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SOIL DESCRIPTION		Interbedded layers of SAND and GRAVEL:	SRAVELLY brom, f	6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	cobbies to 7" size; layer of silty sand (0.0"-1.5").	3,	graded, dense to coarse, poerly to well graded, dense to very dense, angular to subangular, calcareeus; seme fine	to coars trace si					
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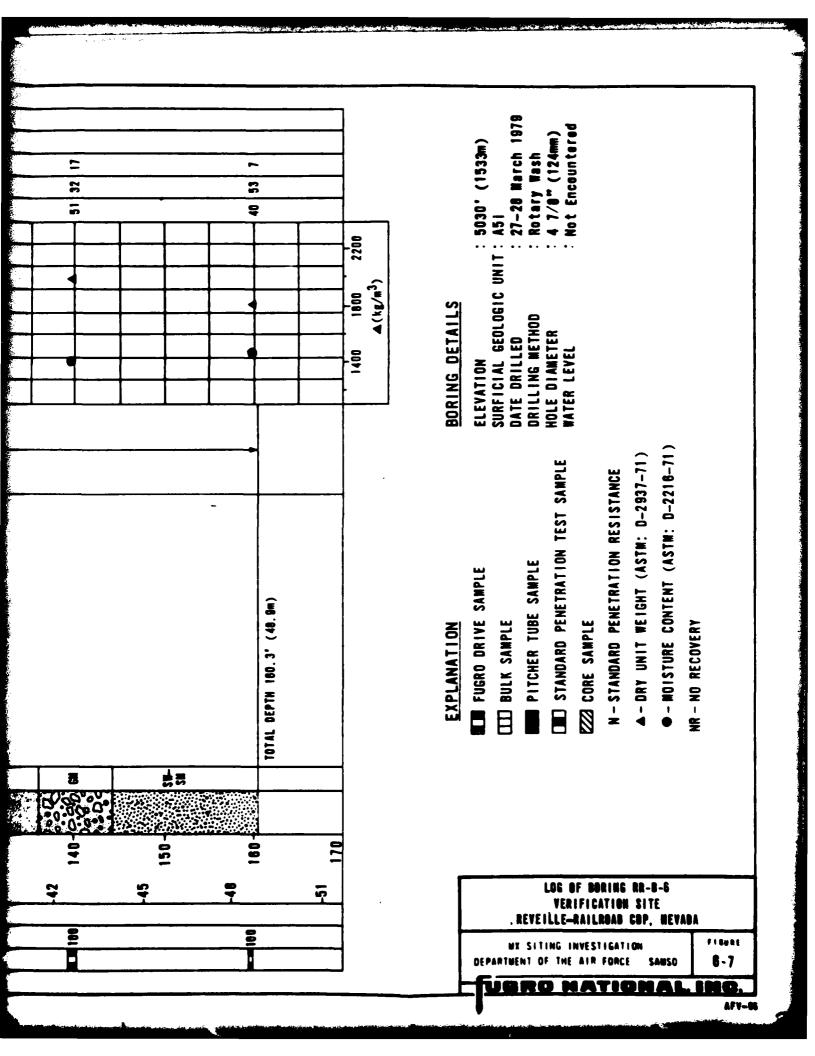




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	SOIL DESCRIPTION		Interbedded layers of SAND and GRAVEL:	-	SILTY SAND (SM): brown, fine to coarse, poorly to well graded,	dense to very dense, angular to subangular, calcareous; little to	some fine to coarse angular to	_	SANDY GRAVEL (GP. GW. GP-GC. GM): brown. fine to coarse, noorly to	9	=	trace to little silt; eccasional cobbies and boulders to 18" size	•					
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SECTION 7.0

TRENCH AND TEST PIT LOGS

# EXPLANATIONS OF TRENCH AND TEST PIT LOGS

See Section 6.0, "Boring Logs", for explanations.

PULE SABPLE	METERS M	PYN	LITHOLOGY	USCS	CONSISTENCY	SOIL BESCRIPTION	REM	RKS		A LY			
	🖫	FEET	5				}		88	24	FI	LL	PI
	0	0		SM	loose	SILTY SAMO, brown, fine to coarse, poorly graded, moist, subangular, calcarcous, some silt; trace fine subrounded gravel.					26		MP
	]  -  -	2-				GRAVELLY SAMD, brown, fine to cearse, poorly graded, alightly meist, sub-angular, calcareous; some fine sub-rounded gravel.	ver wells	tical caving					
		6-		SP	leese								
	-2								l				
		8-				TOTAL DEPTH 7.0' (2.1m)	vertica	esive ng of ol walls cod nation					
								7.9					
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		12-											
		14-											
	-5	16-											
		18-											
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### TRENCH BETAILS

: 5000' (1524m) SURFACE ELEVATION DATE EXCAVATES : 22 MARCH 1978

SURFICIAL GEOLOGIC UNIT: ASY

: 12.0° (4m) TRENCH LENGTH

TRENCH OR IENTATION : E - T

LOG OF TRENCH RR-T-1 VERIFICATION SITE REVEILLE-RAILROAD COP, NEVADA

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO F1 00 RE 7-1

IRO NATIONAL

: 5600' (1707m) SURFACE ELEVATION DATE EXCAVATED : 24 MARCH 1979

SURFICIAL GEOLOGIC UNIT: ASy

TRENCH LENGTH : 18.0' (5m)

TREMEN BRIENTATION : E - #

LOG OF TRENCH RR-T-2 VERIFICATION SITE REVEILLE-RAILROAD COP, MEYADA

MX SITING INVESTIGATION DEPEATMENT OF THE AIR FORCE - SAMSO 71008E 7-2

<u>iro national inc.</u>

DEPTH SVEDICE SEETERS SVEDICE SEETERS SVEDICE	LITHOLOGY	USCS	CONSISTENCY	SOIL DESCRIPTION	REM	NRS	1	IEV	-		
	7		8 3			,	68	SA	FI	LL	71
			soft	\$127, green brown, slightly neist, alightly plastic, calcareous.			0	3	87	44	14
		ML		SAMBY SILT, green, dry, nonplactic, calcareous; some fine sand.		ical					
\ \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\			hard	SILT, green, dry, medium plastic, calcareeus; comented.	98118	stable					
2		SP	leese	SAMS, gray, fine to medium, peerly graded, dry, subangular, calcareeus.	ver	tical caving	1	98	1		
<del>                                    </del>		<b>J</b> .			,	•				1	Н
-3 18-			ned lon dense	SILTY SAMB, gray green, fine, poorly graded, dry, subangular, calcareous; some silt.		tical					
12-		EPL.	hord	SAMBY SILT, brown, dry, slightly plastic, calcareous; little fine send.			0	18	81	29	5
Щ,		100)	hard	SILT, green, dry, highly plastic, colcaroous; trace fine sand.	<u> </u>		0	5	95	50	18
18- -5 18-				TOTAL BEPTH 14.0° (4.3m)							

SURFACE ELEVATION : 4855' (1480m)
BATE EXCAVATED : 26 MARCH 1879

SURFICIAL SECLOGIC UNIT: A40

TRENCH LENGTH : 18.0° (5m)
TRENCH ORIENTATION : N - S

LOG OF TRENCH RR-T-3 VERIFICATION SITE REVEILLE-RAILROAD CDP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

7-3

TURRO NATIONAL INC.

DULK SAMPLE	METERS A	PTH	L: THOLOGY	USCS	CONSISTENCY	SOIL DESCRIPTION	REM	IRKS		IEV			
ī				<u> </u>	83				GR	SA	FI	LL	P
	0	0		CL	atiff	SAMOY CLAY, brown, moist, slightly plastic, calcaroous; some fine sub- angular sand.			6	37	63	30	
		2-		386	nedium dense	SILTY SAMB, light brown, fine, poorly graded, dry, subangular, cal- careous; some silt							
Ш	<del>-</del> 1	4-		SP- SH	ned i un dense	SAME, light brown, fine to coarse, poorly graded, dry, subangular to subrounded, trace silt; trace line subrounded gravel.		tical stable	7	82	11		
Щ	- 2	8-			loose	ERAVELLY SAMD, gray, medium to cearse, poerly graded, dry, subangular, some fine subangular gravel.	,		31	87	2		
	- 3	10-		SP	lesse	SAND, dark brown, fine to coarse, poorly graded, dry, subangular.		ical caving					
	-4	12-			med i um dense	GRAVELLY SAMD, dark brown, medium to corres, poerly graded, dry, subangular; some fine subangular gravel.		ica i stabi e					
						TOTAL DEPTH 14.0° (4.3m)							
	- 5	18-											
		18-											
}	- 6	20~											
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SURFACE ELEVATION : 4830° (1503m)
BATE EXCAVATED : 28 MARCH 1978

SURFICIAL DEBLOCIC UNIT: A40

TRENCH LENGTH : 18.0° (5m)

TRENCH ORIENTATION : N - S

LOG OF TRENCH RR-T-4 VERIFICATION SITE REVEILLE-RAILROAD COP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

7-4

Giano Mariomat

DOLK SABPLE	NETERS S	11 P	I THOLOGY	1350	CONSISTENCY	SOIL DESCRIPTION	REMA	RKS	1	IEV LY:			
3		FEET	[1]		C 8			·	GR	24	FI	3	P
	- 1	2-				SAMOY GRAVEL, brown, fine to coarse, poorly graded, moist, subangular to angular, calcareous (0'-4.0'); some fine to coarse subangular to angular sand; little sift.			59	22	18		
		4 -		ÇM	medium dense								
	- 2	8 -					vert wells	icai stable					
	-3	10-											
	-4	12-		67- 611	nedium densa	SANDY GRAVEL, light brown, fine to 'cearse, poerly graded, slightly meist, subangular, calcareous; some fine to cearse subangular sand; trace silt.			59	32	•		
						TOTAL DEPTH 14.0° (4.3m)							
	- 5	18-											
		18-											
	-\$	20-											

SURFACE ELEVATION : 5200° (1585m) SATE EXCAVATED : 27 March 1979

SURFICIAL GEOLOGIC UNIT: ASy TRENCH LENGTH : 16.0° (5m)

TRENCH ORIENTATION

: E - V

LOG OF TRENCH RR-T-5 VERIFICATION SITE REVEILLE-RAILROAD COP, NEVADA

WX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO F1 00 RE 7-5

BULK SAMPLE	METERS 30	PTH	LITHOLOGY	uscs	CONSISTENCY	SOIL DESCRIPTION	REM	IRKS	AN	IEV	118	
	0	2 -	1	SC- SM	leese	CLAYEY SAND—SILTY SAND, brown, fine to coarse, poorly graded, moist, subangular, calcareous; some silt					F1	
$\prod$	- 2	8-	777777	SP-	ned i un dense	GRAVELLY SAMB, light brown to brown, fine to cearse, poorly graded, slightly moist, subangular, calcareous; little fine subangular gravel; trace slit; stage II caliche (6.0'-8.0').		tical stable				
		8		\$ <b>B</b>	dente	SAND, light brown, fine to cearse, poorly graded, slightly moist, submangular, calcareous; trace fine subangular to subrounded gravel; trace silt; stage III caliche (9.0'-10.0').						
	-3	10-			dense	TOTAL DEPTH 10.0' (3.0m)	soil si					
	4	12-				•	et Cas backh	eity				
		14-										
	- 5	16-										
		18-			į							
	-6	20-										

SURFACE ELEVATION : 5160' (1573m) BATE EXCAVATED : 3 APRIL 1979

SURFICIAL GEOLOGIC UNIT: Als

:18.0° (5m) TRENCH LENGTH : N - \$

TRENCH ORIENTATION

LOG OF TRENCH RR-T-6 VERIFICATION TITE REVEILLE-RAILROAD CDP, NEVADA

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO FIRURE 7-6

UGRO NATIONAL INC.

DULK SAMPLE	ME TE AS	FEET	LI THOLOGY	USCS	CONSISTENC	SOIL DESCRIPTION	REMARKS	AN	A LY:	18	
<b>1</b>	0	0 2-	П	210	ned i um dense	SILTY SAND, light brown, fine to cearse, well graded, slightly meist, subangular, calcareous; some slightly plastic silt; little fine subangular gravel.				F1 25	
	- 1	4			med i um dense	SAND, light brown, fine to coarse, poorly graded, dry, angular, calcareous; trace fine subangular to angular gravel; stage III caliche (5.0'-7.0').					
	- 2	6 -		SP	dense		vertical walls stable				
Щ	-3	10-			dense	GRAYELLY SAND, brown, fine to cogree, poorly graded, dry, subangular, calcareous; little fine subangular gravel.					
					dense	SAND, light brown, fine to coarse, poorly graded, dry, angular, cal— caroous, trace fine subangular to angular gravel.					
	<b>-4</b>	12-				TOTAL DEPTH 12.0' (3.7m)					
	- 5	16-									
		18-									
}	- 6	20-									

SURFACE ELEVATION : 5560' (1885m)
BATE EXCAVATED : 4 APRIL 1979

SURFICIAL GEOLOGIC UNIT: ASI

TRENCH LENGTH : 16.0' (5m)

TRENCH ORIENTATION : E - W

· LOG OF TRENCH RR-T-7 VERIFICATION SITE REYEILLE-RAILROAD CDP, NEVADA

MX SITING INVESTIGATION

DEPARTMENT OF THE AIR FORCE - SAMSO

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UGRO NATIONAL INC.

SURFACE ELEVATION : 3300' (1815m)

DATE EXCAVATED : 5 APRIL 1979

SURFICIAL SECLOSIC UNIT: Als

TRENCH LENGTH : 18.0° (5m)
TRENCH ORIENTATION : NE - SW

LOG OF TRENCH RR-T-8
VERIFICATION SITE
REVEILLE-RAILROAD CDP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

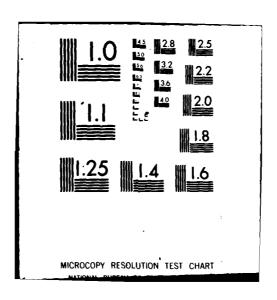
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FUGRO NATIONAL INC LONG BEACH CA F/6 8/13 MX SITING INVESTIGATION. GEOTECHNICAL EVALUATION. VOLUME VII. N--ETC(U) AUG 79 F04704-80-(-0006 AD-A113 329 AUG 79 UNCLASSIFIED FN-TR-27-7 NL .



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DEPARTMENT OF THE AIR FORCE - SAUSO

DALK SAUPLE	BEPTN BENTN BENTN	111101904	20 20	BASISTENCY	SOIL DESCRIPT	1 00	REMARKS	AM	ALY:	_		ī a i
	1 -		sc	nedi un dense	CLAYEY SAMB, brown, fin poorly graded, moist, a calcareous; some slight clay; little fine suban	ubangular. Iv plactic					LL	
	2- 3- 1		GP GM	dense	SAMBY GRAVEL, light bro coarse, poorly graded, moist, subanguiar, caic fine to coarse subangui trace silt; stage II ca 5.0°).	alightly arecus; some ar sand;						
INFACTOR IC	S-CE ELEV CIAL GE O D	ATTIME: 5800 OLDGIC UNIT	(17 : A5 i	ned i un dense	TOTAL DEPTH 5.0' (1.5m) LOG OF TEST PIT RR-P  BRAYELLY SAMB, brown, f poorly graded, soist, a calcareous; some fine to angular gravef; some at clay.	ine to coarse.		29	50	21		
	2- 1 3-		<b>g</b> P	dense	SAMOY GRAVEL, light brocearse, poorly graded, moist, subangular to su calcarsous; some fine to subangular sand; stage (2.0'-3.0').	slightly brounded, o coarse						
WAFAC	S - HE ELEY HAL BE	ATION: S300'	(18 A5y	15m)	TOTAL DEPTH 5.0° (1.5m) LOG OF TEST PIT RR-P	LOGS OF TE	ST PITS RR-P- ERIFICATION : LE-RAILROAD C	SITE			P-1	2
						BEWELL	C Dillaman "		164	4 M A		

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<b>WLE SABPLE</b>	# 16 th 30	FEET #	LITHOLOGY	RGS	MSI STENCY	SOIL DESCRIPTION	REMARKS	AN	LYS	13		
<u>≅</u> ∏	8	6	=			SILTY SAMD, brown, fine to coarse, poorly graded, slightly moist, sub-rounded, calcareous; little silt;		GR	SA	FI	LLP	=
		1		<b>SB</b>	medium dense	trace fine subrounded gravel.						
	-1	3-		<b>SP</b>	nedium dente	GRAVELLY SAND, light brown, fine to cearse, poorly graded, dry, subrounded, colcorous; some fine subsequiar to subrounded gravel.						
	<b> </b>	5-		-		TOTAL DEPTH 5.0° (1.5m)	<del> </del>	1			$\perp$	
VRI	ACE	L GE	ATION: 5000' OLOGIC UNIT	(15: : A5y	24m>	LOG OF TEST PIT RR-P-15	<del></del>					
SUR!	ACE A	ELEV GE	ATION: 5000' OLOGIC UNIT	(15 : Asy	nedium dense	<u></u>		27	57	18		
	PACE	0	ATION: 5000 GLOGIC UNIT	ASy	ned i un	LOG OF TEST PIT RR-P-15  RRAVELLY SAND, brown, fine to coarse, peerly graded, moist, subrounded, calcareous; some fine subrounded gravel; some	alight caving		57.	16		
	0	0 1 - 2 -	OLOGIC UNIT	SM	medium dense medium dense	ERAVELLY SANS, brown, fine to coarse, peorly graded, moist, subrounded, calcareous; some fine subrounded gravel; some silt.  SANDY GRAVEL, light brown, fine, peorly graded, slightly moist, subrounded, calcareous; some fine to coarse subrounded sand.  TOTAL DEPTH 5.0° (1.5e)	slight caving		57	16		
	0	0 1 - 2 -	ATION: 5000 GLOGIC UNIT	SM	medium dense medium dense	COR OF TEST PIT RR-P-15  CRAVELLY SAND, brown, fine to coarse, peorly graded, moist, subrounded, calcarous; some fine subrounded gravel; some silt.  SAMBY GRAVEL, light brown, fine, peorly graded, slightly moist, subrounded, calcarous; some fine to coarse subrounded sand.  TOTAL DEPTH 5.0° (1.5m)  LOG OF TEST PIT RR-P-18  LOGS OF T	EST PITS RR-P-1 VERIFICATION S	5 AN		₹₹ -	P-18	
	0	0 1 - 2 -	OLOGIC UNIT	SM	medium dense medium dense	CORRECT PIT RR-P-15  CRAVELLY SAND, brown, fine to coarse, peerly graded, moist, subrounded, calcareous; some fine subrounded gravel; some silt.  SAMBY GRAVEL, light brown, fine, peerly graded, slightly moist, subrounded, calcareous; some fine to coarse subrounded cand.  TOTAL DEPTH 5.0° (1.5m)  LOG OF TEST PIT RR-P-18  LOGS OF TREVEL	EST PITS RR-P-1	5 ARITE		₹₹ -	)-18	

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DEPARTMENT OF THE AIR FORCE - SAMSO

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MLK SABPL	# 15 to 19	7711	LITHOLOGY	WCS	OHS! BTEMEY	SOIL DESCRIPTION	REMARKS	AN	IEV ALY:	118		
<u> </u>	L	2	] =		8			68	SA	FI	LL	PI
		1 -		SP~	logge	GRAVELLY SAND, dark brown, fine to coarse, poorly graded, moist, sub- angular, calcareous; some fine to coarse subangular gravel; trace silt; eccasional cobbles to 10° size.		27	38	7		
	<b>-</b> 1	3 -										
	r	5 -		┼	<b></b>	TOTAL DEPTH 5.0° (1.5m)	<del> </del>	┨	ł			
TA I	ACE	ELEV	ATIM: 8218	<del>                                     </del>		101AC DEFTH 3.0 (1.30)	<u> </u>	ل_	<u> </u>	نـــا		
			7210	Cia	900)	IAG AE TEGT BIT ON B A1						
türi	'ÎĈ ÎA	L SE	ATION: 5215 OLOGIC UNIT	: A5y	900)	LOG OF TEST PIT RR-P-21						
S UN P	O	0 1 · · · 2 · · · 4 · ·	OLOGIC UNIT	ASY	med i um dense	GRAYELLY SAMD, light brown, fine to coarse, peerly graded, slightly meist, subengular, calcareous; some fine to coarse subangular to angular gravel; stage III caliche (4.5'-5.0'); eccasional cobbles to 8" size.						
		1 -	OLOGIC UNIT		ned i un	GRAYELLY SAMD, light brown, fine to coarse, peerly graded, slightly meist, subengular, calcareous; seme fine to cearse subangular to angular grayel; stage III caliche (4.5'—						
		1 -	OLOGIC UNIT		medium dense	GRAYELLY SAMD, light brown, fine to coarse, peerly graded, slightly meist, subengular, calcareous; seme fine to cearse subangular to angular grayel; stage III caliche (4.5'—						
	0	2-3-	ATION: SADO	SP	med i um den ae	GRAYELLY SAMD, light brown, fine to coarse, peerly graded, alightly moist, subengular, calcareous; some fine to coarse subengular to angular gravel; stage III caliche (4.5'-5.0'); occasional cobbles to 8" size.  TOTAL DEPTH 5.0' (1.5e)  LOG OF TEST PIT RR-P-22	et bire on a	7) 44				
	0	2-3-		SP	med i um den ae	GRAYELLY SAMD, light brown, fine to coarse, peerly graded, alightly moist, subengular, calcareous; some fine to coarse subengular to angular gravel; stage III caliche (4.5'-5.0'); occasional cobbles to 8" size.  TOTAL DEPTH 5.0' (1.5m)  LOG OF TEST PIT RR-P-22  LOGS OF TE	ST PITS RR-P-2 VERIFICATION S LE-RAILROAD C	SITÉ	•			2
	0	2-3-		SP	med i um den ae	GRAYELLY SAMD, light brown, fine to coarse, peerly graded, alightly moist, subengular, calcareous; seme fine to coarse subengular to angular gravel; stage III caliche (4.5'-5.0'); occasional cobbles to 8" size.  TOTAL DEPTH 5.0' (1.5m)  LOG OF TEST PIT RR-P-22  LOGS OF TE	VERIFICATION S LE-RAILROAD C	SITÉ DP,	•			
	0	2-3-		SP	med i um den ae	GRAYELLY SAMD, light brown, fine to coarse, peerly graded, alightly moist, subengular, calcareous; seme fine to coarse subengular to angular gravel; stage III caliche (4.5'-5.0'); occasional cobblec to 8" size.  TOTAL DEPTH 5.0' (1.5m)  LOG OF TEST PIT RR-P-22  LOGS OF TE	VERIFICATION :	SITĒ DP, I	ÑEY		FI	2

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BULK SABPLE	ME TERS	FEET	L. I THOLOGY	USCS	CONSISTENCY	SOIL BESCRIPTION	REMARKS	AN		\$1\$		
3	0	1 -		<b>ea</b>	nedi un dense	SANDY GRAYEL, brown, fine, poorly graded, slightly moist, subangular, calcareous; some fine to coarse subangular sand; little silt.		GR	SA	FI	LL	PI
	ļ -,	3 -		96	dense	SANOY GRAVEL, red brown, fine, poerly graded, slightly moist, subangular, calcareous; some fine to cearse subangular sand; little slightly plastic clay; stage II caliche (3.25'-3.5').					;	
		4-				TOTAL DEPTH 3.5" (1.1m)	comentation exceeded capacity of Case 580C backhee at 3.5°					
SURI	ACE		ATION: 5520° Ologic Unit:	(18	82m)	LOG OF TEST PIT RR-P-31	<u> </u>		<u> </u>		Ш	
	-1	2-		\$- \$3	10020	GRAVELLY SAMB, brown, fine to cearse, peorly graded, slightly meist, sub-angular, calcareous, some fine sub-angular gravel; trace silt.						
		5 -		ep	medium dense	SANDY GRAVEL, gray brown, fine, poorly graded, dry, subangular, calcareous; some fine to coarse subangular send.  TOTAL DEPTH 5.0' (1.5m)						
SURF SURF	ACE ICIA	L GE	ATION: 5600' OLOGIC UNIT:	(17 A5y	07m)	LOG OF TEST PIT, RR-P-32						
							ST PITS RR-P-3 Verification s Le-Railroad Co	ITE			P-32	
						<del></del>		,		T		
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SECUTION 8.0 SUPPLICIAL SAMPLE LOCS

#### EXPLANATIONS OF SURFICIAL SAMPLE LOGS

Finalized logs of the surficial samples are presented in this section. The explanations provided here are to serve as general guidelines to reading the logs.

- A. Designations Surficial samples are identified as follows: SE-CS-1
  - SE abbreviation for the site (e.g., SE Snake East)
  - CS abbreviation for surficial sample
  - 1 number of activity
- B. Ground Surface Elevation Indicated elevations on the logs are estimated from topographic maps of the study area within an accuracy of half the contour interval.
- C. Surficial Geologic Unit Indicates the surficial geologic unit in which the activity is located.
- D. Depth Indicates depth interval for which soil description is given.
- E. USCS Unified Soil Classification Symbol; see Table 6-1 of Section 6.0, "Boring Logs", for details of USCS.
- F. Soil Description Soil is described based on field visual descriptions and/or laboratory test results. See Section 6.0, "Boring Logs", for procedures of soil description.
- G. Sieve Analysis, LL and PI These are from results of laboratory tests. See Section 6.0, "Boring Logs", for explanation.

ACT IVITY	OR OUND SWRFACE ELEVATION,	SURFICIAL GEOLOGIC	be PTN, Feet	ASC2	SOIL DESCRIPTION	1 -	IEV ALY:	_		
*********	FEET (METERS)	UMIT	(METERS)			88	SA	FI	LL	P
RR-cs-5	4970 (1515)	ASy	0.0-1.25 (0.0-8.4)	28	SILTY SAME, brown, fine to medium, peerly graded, subangular, cal— careous; some slit; trace fine gravel.					
			1.25-2.0 (0.4-0.8)	8P	SAMBY SRAYEL, light brown, fine, poorly graded, subrounded, cal-careous; some fine to coarse sand.					
RR-CS-7	4985 (1519)	ASy	0.0-2.0 (0.0-0.8)	SM	SILTY SAND, brown, fine to medium, poorly graded, subangular, calcareus; some silt; trace fine gravel.				<u> </u>	
RA-CS-8	4950 (1509)	ASy	0.0-1.5 (0.0-0.5)	SH	SILTY SAMS, brown, fine to coarse, poorly graded, subrounded, cal- careous; some silt; trace fine to coarse grave!	8	62	30		
			1.5-2.0 (0.5-0.8)	SP	SAMBY GRAVEL, light brown, fine to coarse, poorly graded, subrounded, calcureous; some fine to coarse send.	54	43	3		
RR-CS-10	4930 (1503)	A4e/A5y	0.0-2.0 (0.0-0.8)	CL-	SAMBY CLAY-SANDY SILT, light brown, slightly plastic, calcareous; some fine to medium sand.	1	37	62	24	!
RR-CS-11	4940 (1506)	A5y	0.0-2.0 (0.0-0.8)	SW	GRAVELLY SAND, brown, fine to cearse, poorly graded, subrounded, calcareous; some fine to coarse gravel; some silt.	25	53	22	20	   
RR-CS-13	5050 (153 <b>9</b> )	A5y	0.0-2.0 (0.0-0.5)	M2	SILTY SAND, brown to light brown, fine to medium, poorly graded, subangular, calcareous; some silt.					
RR-CS-15	5030 (1533)	ASI	0.0-2.0 (0.0-8.8)	SM	SILTY SAND, light brown, fine to coarse, poorly graded, subrounded, calcareous; little silt; trace fine gravel.	20	62	18		N
RR-CS-17	5500 (1878)	A5 i	0.0-1.75 (0.0-0.5)	SM	SILTY SAND, brown, fine to cearse, peerly graded, subangular, calcareous; some silt; little fine gravel.					
:			1.75-2.0 (0.5-0.6)	87-SM	SAMPY GRAYEL, white to light brown, fine to cearse, poorly graded, sub-angular, calcareous; some fine to cearse sand; trace sift; stage III caliebe.					
RR-CS-18	5100 (1554)	ASy	0.0-2.0 (0.0-0.8)	<b>51</b>	SILTY SAND, brown, fine to cearse, poerly graded, subangular, calcareous; some sift; trace fine gravel.					
RR-CS-20	5900 (1798)	A5 i	0.0-2.0 (0.0-0.6)	CL	SAMOY CLAY, brown, slightly plastic, calcareous; some fine to coarse sand, little fine gravel; stage III caliche (1.9'-2.0').					

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SANSO

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UERO NATIONAL INC. AFY-17

NUMBER	er ound Surface Elevation	SURFICIAL GEOLOGIC	DE PTH,	uscs	SOIL DESCRIPTION	- [ ]	IEV ALY:	E 8 1 S		
NUMBER	FEET (METERS)	UNIT	FEET (METERS)			ER	SA	FI	᠘	P
RR-CS-25	5005 (1528)	A5y	0.0-2.0 (0.0-0.8)	23	SILTY SAND, brown, fine to coarse, peorly graded, subrounded, cal- careeus; some silt; trace fine gravel.					
RR-68-27	4975 (1516)	A5y	0.0-1.75 (0.0-0.5)	SM	SILTY SAND, brown, fine to coarse, peerly graded, subrounded, cal—careous; some slightly plastic silt; trace fine gravel.					
•			1.75-2.0 (0.5-0.8)	SP	GRAVELLY SAND, light brown, fine to cearse, peerly graded, subrounded, calcareous; some fine gravel.		}   			
RR-CS-28	4865 (1513)	ASy	0.0-2.0 (0.0-0.8)	SH	SILTY SAND, brown, fine to coerse, peorly graded, subrounded, cal—careous; some silt; trace fine gravel.					
RR-CS-29	4950 (1509)	A3/A5y	0.0-2.0 (0.0-0.8)	<b>SM</b>	SAMD, brown, fine to coarse, poorly graded, subrounded, calcareous; little silt.	2	84	14		
RR-CS-30	4963 (1513)	A3/A5y	0.0-0.75 (0.0-0.2)	CL	SANDY CLAY, brown, slightly plastic, calcareous; some fine to medium some.					
			0.75-2.0 (0.2-0.8)	SP-SM	SAND, light brown, fine to coarse, peerly graded, subrounded; trace silt; trace fine gravel.			,		
RR- <b>C\$-</b> 32	51 <i>20</i> (1560)	A5y	0.0-2.0 (0.0-0.8)	39	SILTY SAND, light brown, fine to coarse, poorly graded, subrounded, calcareous; some silt; trace fine gravel.					
RR-CS-34	5380 (1848)	A5y/A5i	0.0-2.0 (0.0-0.5)	SW-SM	SAMD, brown, fine to coarse, well graded, subangular, calcareous; trace silt; little fine gravel.	11	83	6		
RR-CS-37	5010 (1527)	ASI	0.0-1.5 (0.0-0.5)	SM	GRAVELLY SAND, brown, fine to coarse, poorly graded, subangular, cal- careous; little fine gravel; little alt.					
			1.5-2.0 (0.5-0.8)	er er	SAMDY BRAVEL, light brown, fine, poorly graded, subrounded, cal- careous; little fine to coarse sand.					
RR-CS-38	5010 (1527)	ASy	0.0-1.5 (0.0-0.5)	SM	SILTY SAMD, brown, fine to coarse, poorly graded, subengular, cal—careous; some ailt; trace fine gravel.					
			1.5-2.0 (8.5-0.8)	SP-SM	1 -					

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

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UGRO NATIONAL INC.

NUMBER	SURFACE ELEVATION.	SURFICIAL GEOLOGIC	be PTN, Feet	naca	SOIL DESCRIPTION	1	ALY:	E S i S		
	FEET (METERS)	UNIT	(METERS)			GR	SA	FI	LL	P
RRCS38	5808 (1524)	A5y	0.0-2.0 (0.0-0.0)	<b>58</b>	SILTY SAND, light brown, fine to coarse, peerly graded, subangular, calsareous; some silt; trace fine gravel.	7	67	26		
RRC341	4 <b>980</b> (1512)	A5y	0.0-2.0 (0.0-0.8)	<b>39</b>	SILTY SAMB, brown, fine to medium, peerly graded, subangular to sub- rounded, calcareous; little silt; trace fine gravei					
RNCS42	4940 (1508)	A5y	0.0-2.0 (0.0-0.6)	SP-80	SAMD, brewn, fine to medium, peorly graded, subangular; trace silt.					
RR-CS-44	4890 (1480)	A5y	0.0-1.0 (0.0-0.3)	sc	CLAYEY SAMD, brown, fine te coerse, peorly graded, subangular, cal- careous; some slightly plastic elay; trace fine gravel.					
			1.0-2.0 (0.3-0.8)	SP-SM	GRAVELLY SAND, brown, fine to coarse, poerly graded, subangular; some fine gravel; trace silt.					
RR-CS-45	4980 (1484)	A5y	0.0-1.0 (0.0-0.3)	SC-SM	CLAYEY SANG-SILTY SANG, brown, fine to cearse, poerly graded, sub- angular; some slightly plastic silt and slav.	C	50	50	25	
			1.0-2.0 (0.3-0.6)	SM	SILTY SAND, white, fine, peerly graded, subangular, calcareous; some silt; stage [1] celiche.		] 			
RR-CS-47	5060 (1542)	A5y	0.0-1.5 (0.0-0.5)	SM	SILTY SAND, light brown, fine to coarse, poorly graded, subangular, calcareous; little silt; trace gravel.					
			1.5-2.8 (0.5-0.8)	SP	SAMDY GRAVEL, white, fine, poorly graded, subangular, some fine to coarse sand.					
RR-CS-49	5060 (1542)	A1	0.0-0.75 (0.0-0.2)	SM	SILTY SANS, dark brown, fine to coarse, poorly graded, subangular, calcareous; fittle silt; trace fine gravel.					
			0.75 <b>-2.0</b> (0.2 <b>-</b> 0.8)	SC	CLAYEY SAND, light brown, fine to coarse, poorly graded, subangular; little slightly plastic clay; trace fine gravel.					
RRC\$51	5120 (1581)	A5y	0.0-2.0 (0.0-0.6)	SP-SM	SAND, dark brown, fine to cearse, poorly graded, subangular, cal— careous; trace fine gravel; trace silt.		<u>.</u>			
RR-CS-53	5355 (1632)	ASI	0.0-2.0 (0.0-0.5)	sc	CLAYEY SANO, light brown, fine to coarse, peerly graded, subangular, calcareous; some slightly plastic clay; trace fine gravel.	7	58	35		

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO

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UGRO NATIONAL INC.

NUMBER (M	CROUND SURFACE ELEVATION,	SURFICIAL SEOLOGIC	DE PTH, FRET	USCS	SOIL DESCRIPTION	1 "	IEV ALY:	E 5 1 8		
MUMBER	FEET (METERS)	UNIT	(WETERS)			GR	SA	FI	u	PI
RR-CS-57	5580 (1701)	A2	0.0-1.0. (0.0-0.3)	sc	GRAVELLY SAND, brown, fine to course, poerly graded, subangular, calcareous; little fine gravel; little slightly alastic clay.					
	(0.3-0.6) graded, subangular, calcareous seme fine to coarse sand.  -CS-50 5640 A5y 0.0-2.0 SM SILTY SAND, brown, fine to coarse	SANDY GRAVEL, brown, fine, poerly graded, subanguier, caicareous;								
RR-CS-59	5840 (1719)	A5y	0.0-2.0 (0.0-0.8)	<b>SM</b>	SILTY SAMD, brown, fine to coarse. poerly graded, subengular, little silt; trace fine gravel.					
RRCS61	5730 (1747)	ASi	0.0-1.5 (0.0-0.5)	M2	SiLTY SAND, brown, fine to coarse, poorly graded, subangular, cal- careous; little silt; little fine gravel.					
			1.5-2.0 (0.5-0.8)	\$C	CLAYEY SAMD, brown, fine to coarse, poorly graded, subangular, cal- carsous; some slightly plastic clay; trace fine gravel.					
RR-CS-83	592 <b>6</b> (1804)	A51	0.0-2.0 (0.0-0.8)	sc	CLAYEY SAMD, brown, fine to coarse, poorly graded, subangular, cal-careous; some alightly plastic clay; trace fine gravel; stage I caliche (1.0°-2.0°).					
RR-CS-65	5600 (1707)	A2	0.0-2.0 (0.0-0.6)	CL	SAMBY CLAY, light brown, medium slastic, caicareeus; some fine te cearse sand; staga I caliche (0.25'-1.0'); stage II caliche (1.0'-2.0').					
RR-C3-67	5585 (1696)	A5 i	0.0-2.0 (0.0-6.6)	SM	GRAVELLY SAND, brown, fine to coarse, poorly graded, subangular, calcareous; some fine gravel; little sitt.					
RR-C3-69	5510 (1679)	A5i	0.0-2.0 (0.0-0.6)	<b>12-42</b>	GRAYELLY SAMD, brown, fine to coarse, paorly graded, subangular, caicareous; little fine gravel; trace silt.					
RR-CS-71	54 <b>80</b> (1670)	A5y	0.0-2.0 (0.0-0.8)	SP	SAMS, brown, fine to coarse, poorly graded, subangular, calcareous; trace fine gravel.					
RR-CS-73	5520 (1682)	A5y	0.0-2.0 (0.0-0.8)	SC	CLAYEY SAMD, light brown, fine to coarse, peorly graded, subangular, calcareous; some slightly plastic clay; trace fine gravel.					
RA-CS-79	5425 (1854)	A5y	0.0-2.0 (0.0-0.6)	sc	CLAYEY SAND, light brown, fine to cearse, poorly graded, subengular, calcareous; seme slightly plastic clay; trace fine gravel.					
RR-CS-80	5415 (1850)	ASI	0.0-2.0 (0.0-0.8)	SM	SILTY SAND, brown, fine to coarse poorly graded, subangular, cal— careous; little silt; trace fine gravel.					

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

8-1 4 9F 3

VERO NATIONAL INC

ACT IVITY	IIAIAL SOMLWOE	SURFICIAL GEOLOGIC	DE PTH. FEET	USCS	SOIL DESCRIPTION	- 1	BIEV	/E \$ 1\$		
		UNIT	(METERS)	-	ALLEY AND LOCAL SIZE AS ASSAULT	CR	SA	FI	LL	•
# <b>-63-4</b> 2		ASy	0.0-2.0 (0.0-0.6)		SILTY SAMD, brown, fine to coarse, pearly graded, subangular, cal— careeus; little silt; trace fine gravel.					
!										

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FIGURE B-1 S OF S

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SECTION 9.0 LABORATORY TEST RESULTS 

#### EXPLANATIONS OF LABORATORY TEST RESULTS

Laboratory test results are presented in this section. Table 9-1 contains a summary of laboratory test results. This table contains results of sieve analysis; plasticity data; in-situ dry unit weight, moisture content, degree of saturation, and void ratio for drive and Pitcher samples; results of compaction tests; and specific gravity of solids. Other tests such as triaxial compression, unconfined compression, direct shear, consolidation, chemical, and California Bearing Ratio (CBR) are indicated on the table. Tables 9-2 through 9-6 and Figures 9-1 through 9-3 present results of triaxial compression, unconfined compression, direct shear, consolidation, chemical, and CBR tests.

All tests were performed in general accordance with the American Society for Testing and Materials (ASTM) procedures. The following table presents the ASTM designations for the tests performed during the investigation.

Type of Test	ASTM Designations
Particle Size Analysis	D 422-63
Liquid Limit	D 423-66
Plastic Limit	D 424-59
Unit Weight	D 2937-71
Moisture Content	D 2216-71
Compaction	D 1557-70
Specific Gravity of Solids	D 854-58
Triaxial	2850-70
Unconfined Compression	D 2166-66
Direct Shear	D 3080-72
Consolidation	D 2435-70
Test for Alkalinity (pH)	D 1067-70
Water Soluble Sodium	D 1428-64
Water Soluble Chloride	D 512-67
Water Soluble Sulphate	D 516-68
Water Soluble Calcium	D 511-72
Calcium Carbonate	D 1126-67
California Bearing Ratio (CBR)	D 1883-73

Explanation for the tables and figures presented in this section are as follows.

- A. Activity Number Boring, trench, test pit, or surficial sample designation.
- B. Sample Number Prefix indicates the type of sample; explanation is at the bottom of the table.
- C. Sample Interval This is the depth range measured from ground surface over which the sample was obtained.
- D. Percent Finer by Weight Presents the results of laboratory particle size analysis (ASTM D 422-63) performed on representative soil samples at the depth indicated. The numbers represent the percent (by dry weight) of the total sample weight passing through each sieve size indicated.
- E. Atterberg Limits (ASTM D 423-66 and D 424-59)
  - LL Liquid Limit, the water content (as percent of soil dry weight) corresponding to the arbitrary limit between the liquid and plastic states of consistency of a soil (ASTM D 423-66).
  - PL Plastic Limit, the water content corresponding to an arbitrary limit between the plastic and the semisolid state of consistency of a soil (ASTM D 424-59).
  - PI Plasticity Index, numerical difference between the liquid limit (LL) and the plastic limit (PL) indicating the range of moisture content within which a soil-water mixture is plastic.
  - NP Nonplastic.
- F. USCS Unified Soil Classification Symbols are given here; see Table 6.1 in Section 6.0, "Boring Logs", for complete details of USCS system.

- G. In Situ Presents results of tests on drive and Pitcher samples.
  - Dry Unit Weight indicates dry unit weight of soil determined as per ASTM D 2937-71
  - Moisture Content weight of water reported in percent of dry weight of soil sample (ASTM D 2216-71)
  - Saturation the degree of saturation in a soil sample is defined as the ratio (in percent) of the volume of water to the volume of all voids in the soil
  - Void Ratio the numerical ratio of the volume of voids to the volume of solids in a soil specimen
- H. Compacted Indicates results of laboratory maximum dry density and optimum moisture content test as per ASTM D 1557-70.
- I. Specific Gravity of Solids (ASTM D 854-58) Indicates the ratio of (1) the weight in air of a given volume of soil solids at a stated temperature, to (2) the weight in air of an equal volume of distilled water at a stated temperature.
- J. Triaxial The triaxial compression tests were performed in accordance with the procedures of ASTM D 2850-70. The following explanations and definitions apply.

Triaxial Compression Test - a cylindrical specimen of soil is surrounded by a fluid in a pressure chamber and subjected to an isotropic pressure. An additional compressive load is then applied, directed along the axis of the specimen called the axial load.

Consolidated-Drained (CD) Test - a triaxial compression test in which the soil was first consolidated under an all-around confining stress (test chamber pressure), and was then compressed (and hence sheared) by increasing the

vertical stress. Drained indicates that excess pore water pressure generated by strains are permitted to dissipate by the free movement of pore water during consolidation and compression.

Consolidated-Undrained (CU) Test - a triaxial compression test in which essentially complete consolidation under the confining (chamber) pressure is followed by a shear test at constant water content.

Confining Pressure (  $\sigma_3)$  - the isotropic chamber pressure applied to the soil specimen during consolidation and compression.

Maximum Deviator Stress ( $\sigma_1 - \sigma_3$ ) - the difference between the major and minor principal stresses in the specimen at failure. The major principal stress on the specimen is equal to the unit axial load plus the chamber pressure and the minor principal stress on the specimen is equal to the chamber pressure.

Strain Rate - axial strain,  $\epsilon$ , at a given stress level is defined as the ratio of the change in length ( $\Delta L$ ) of the specimen to the original length of the specimen ( $L_0$ ). The rate of strain was controlled during the test so that this ratio increased at equal increments for each minute of testing.

Back Pressure - pressure in excess of atmospheric applied to the pore water of a soil sample. Back pressure is usually applied to (1) increase saturation of the sample, or (2) simulate the actual in-situ pressure regime.

K. Unconfined Compression - Test procedures were as described in ASTM D 2166-66. Unconfined compressive strength is defined as the load per unit area at which an unconfined prismatic or cylindrical specimen of soil will fail in a simple compression test. In these methods, unconfined compressive strength is taken as the maximum load attained per unit area or the load per unit area at 20 percent axial strain, whichever occurred first during the performance of a test. A. C. C.

- L. Direct Shear The procedures of ASTM D 3080-72 were followed for direct shear testing. In this test, soil under an applied normal load is stressed to failure by moving one section of the soil container (shear box) relative to the other section. Normal stress is the value of load per unit area acting perpendicular to the plane of shearing. Maximum shear strength is defined as the maximum resistance (ksf) of a soil to shearing (tangential) stresses.
- M. Consolidation (ASTM D 2435-70) A consolidation test is a test in which a cylindrical soil specimen is laterally confined in a ring and compressed between porous plates. The term "consolidation", as used here, indicates the gradual reduction in volume of the soil mass resulting from an increase in compressive stress (axial load per unit area).
- N. Chemical The chemical tests performed on soil samples included: pH; water soluble sodium, chloride, sulphate, calcium; and calcium carbonate content. pH is an index of the acidity or alkalinity of a soil in terms of the logarithm of the reciprocal of the hydrogen ion concentration.

  ASTM test procedure designations for these chemical tests are included in the table at the beginning of the "Explanation of Laboratory Test Results".
- O. CBR California Bearing Ratio (CBR) is the ratio (in percent) of the resistance to penetration developed by a subgrade soil to that developed by a standard crushed-rock

base material. The procedures for conducting a CBR test were as outlined in ASTM D 1883-73. The materials tested for CBR were also analyzed for particle size distribution (ASTM D 422-63) and compaction characteristics (ASTM D 1557-70). The term "percentage of maximum density" indicates the ratio (as a percentage) of the compacted sample dry unit weight to maximum dry density obtained in the laboratory from ASTM D 1557-70, "Moisture-Density Relations of Soils Using 10-pound (4.5 kg) Hammer and 18-inch (457 mm) Drop".

	_	<u> </u>		r			_		PERCE	NT FIN	FINER BY WEIG				
E _	(a)	SAMPLE 1	NTERVAL		\$	TANDAR	SIEV	E OPEN	186		0.9	81			
ACT I VI TY Number	SAMPLE			BLORS	COBE	ILES	Ι	64	YEL						
2 2	2 =	FEET	METERS	24"	12"	6"	3"	15"	3/4"	3/8"	4	Ħ			
RR-B-1	P-1	0.8-1.6	0.24-0.49												
	D-3	7.2-7.7	2.19-2.35						100	98	87	ब			
	D-4	10.0-10.4	3.05-3.17					100	85	74	63	5			
	D-4	10.4-10.9	3.17-3.32						1						
	D-5	15.4-15.9	4.69-4.85						100	91	74	4			
	D-6	20.0-20.9	6.10-6.37			l									
	D-7	25.2-25.7	7.68-7.83					100	96	77	57	4			
	D-8	30.2-30.7	9.20-9.36												
	D-9	35.1-35.6	10.70-10.85									1			
ļļ	D-10	40.1-40.6	12.22-12.37						100	99	89	76			
ļ	D-11	50.4-50.9	15.36-15.51	l			<b>.</b>		<u> </u>	L					
	D-12	60.2-60.7	18.35-18.50	- 1			<b>.</b>			100	99	8			
	D-13	70.5-70.9	21.49-21.61			<b></b> -	L	ļ,	L						
ļ	D-14	80.9-81.4	24.66-24.81				ļ	L		L					
	D-15	90.1-90.6	27.46-27.61				ļ		100	85	58	40			
<b></b>	D-16	100.1-100.6	30.51-30.66					L	<b>[</b>	<b>[</b> .					
<b></b>	D-17	110.1-110.6	33.56-33.71			ļ		L	<b>.</b>	<b>.</b>					
<b>├</b> ──	D-18	120.1-170.6	36.61-36.76				ļ	<b> </b>		ļ					
	D-19	141.1-141.6	43.01-43.16	<b></b>			ļ	ļ	100	98	90	71			
<u> </u>	D-20	160.2-160.7	48.83-48.98	L					100	94	81	54			
22 2 3	- 1	0010		ł ł					l i						
RR-B-2	P-1	0.9-1.8	0.27-0.55							ļ		10			
	P-2	3.0-3.9	0.91-1.19				<b> </b>								
<b></b>	D-3	7.0-8.2	2.13-2.50	<b> </b>		L			100	65	40	31			
<b>├──</b>	D-4	10.8-11.3	3.29-3.44				<b></b> -								
} <del>-</del>	D-5 D-6	15.4-15.9	4.69-4.85							100	98	2			
<u> </u>	D-7	20.4-20.9	6.22-6.37												
<del>                                     </del>	D-8	25.4-25.9 30.4-30.9	7.74-7.89	├			<b> </b>		100	82	62	37			
<b>}</b>	D-8 D-9	35.3-35.9	9.27-9.42	<b>├</b> {		ļ	<b> </b>			<b> </b>		<b> </b>			
<del>}</del>	P-10	38.8-39.6	10.76-10.94			<del></del>	├			100	90				
<del> </del>	P-11	40.4-41.1	11.83-12.07				├		ļ	100	99 100	9			
	D-12	50.2-50.7	15.30-15.45			<del> </del>					100	24			
	P-13	59.0-61.8	17.98-18.84				<b></b>								
	P-14	69.0-71.8	21.03-21.88	<del></del>			$\vdash$		<del>                                     </del>		100	91			
· · · · · · · · · · · · · · · · · · ·	D-15		24.44-24.66					<b></b>	<del>                                     </del>	<del>                                     </del>	-50				
<del> </del>	D-16		27.49-27.71	<b></b>			$\vdash$	<del></del>	100	99	89	6			
<u> </u>		100.1-100.6	30.51-30.66						100	<del>-??</del> -	- 03	-			
<del>                                     </del>	P-18		33.22-33.77	<del> 1</del>							-				
<b></b>		119.0-120.2	36.27-36.64				<b></b>	<del></del>							
<del> </del>		120.0-121.1	36.58-36.91	<del>                                     </del>			<b></b>	—	-	<del></del>	100				
<del> </del>		140.0-140.9		<b></b>			-	<b></b>			100	3			
·	P-21			<del></del> -{	——		$\vdash$	<del></del>				14			

(a) Sample types

- (c) USCS Unified Soil Classification System
- SS Standard split spoon
- P Pitcher
- (d) \* Indicates that test has been performed and results are included in this report
- D Fugro Orive
- B,b Buik
- (b) NP Not Plastic

		SM	120.4	1929	6.5	43.6
		SM				
		SP	112,5	1802	8,1	44.0
		SW	116.6	1788	9.6	50.8
		SW	121.5	1946	9.8	68.3
		SW	111.6	1788	12.2	64.8
		SM				
		SW-SM	111.3	1783	11.7	61.7
	1	SW-SM	114.1	1828	10.5	59.3
		SM	118.3	1895	8.5	54.4
		SM	109.6	1756	10.8	59.2
		SM	116.0	1858	9.7	57,0
		SM	121.7	1949	10.7	75.0
		SM	118.4	1897	9.7	61.8
		SM				1
		SM	107.1	1716	12.0	56.8
		SW	111.3	1783	13.3	69.8
		SP-SM	114.5	1834	10.7	61.
	1					
		SM	98.8	1583	14.6	56.0
		SM	100.3	1607	6.6	26.
	<b></b>	GW-GM	102.7	1645	15.5	65.4
$\overline{}$		GW-GM	109.4	1752	2.9	14.5
	· †	SP	102.2	1637	3.5	14,
		SP	104.9	1680	4.3	19.0
	$\vdash$	SW	110.1	1764	15.5	78.9
	<b></b>	SW	98.7	1581	6.2	23.
		ML	105.6	1692	6.9	31.

SM 111.6 1788 12.2 64.8 0.51  SM SM 111.3 1783 11.7 61.7 0.51  SM-SM 111.1 1828 10.5 59.3 0.48  SM 116.0 1858 9.5 54.4 0.42  SM 109,6 1756 10.8 59.2 0.54  SM 116.0 1858 9.7 57.0 0.45  SM 116.0 1858 9.7 57.0 0.45  SM 116.1 1949 10.7 75.0 0.39  SM 118.4 1897 9.7 61.8 0.42  SM 107.1 1716 12.0 56.8 0.57  SM 111.3 1783 13.3 69.8 0.51  SM 114.5 1834 10.7 61.5 0.47  SM 98.8 1583 14.6 56.0 0.71  SM 98.8 1583 14.6 56.0 0.71  SM 100.3 1607 6.6 26.2 0.68  GM-CM 102.7 1645 15.5 65.4 0.64  GM-CM 109.4 1752 2.9 14.5 0.54  SP 102.2 1637 3.5 14.7 0.65  SP 102.2 1637 3.5 14.7 0.65  SP 102.9 1639 4.3 19.0 0.61  SM 98.4 1576 5.1 19.4 0.71  SM 98.4 1576 5.1 19.4 0.71  SM 13.6 1820 16.9 1.9 1.9 0.51  SM 13.1 1.6 120 16.3 9.1.0 0.71  SM 98.4 1576 5.1 19.4 0.71  SM 98.5 1585 14.6 15.5 78.9 0.53  SM 98.7 1581 6.2 23.7 0.71  ML 105.6 1692 6.9 31.2 0.60  SM 98.4 1576 5.1 19.4 0.71  SM 111.4 1784 11.2 59.3 0.51  SM 98.7 1581 6.2 23.7 0.71  SM 111.6 1820 16.3 91.3 0.54  SM 111.6 1820 16.3 91.3 0.54  SM 98.8 1583 14.6 21.7 10.65  SM 98.9 1585 15.5 57.0 0.60  SM 98.1 11.8 1791 13.6 72.4 0.51  SM 110.1 1766 15.5 74.2 0.60  SM 111.8 1791 13.6 72.4 0.51  SM 110.1 1668 10.4 45.5 0.53  SM 104.1 1668 10.4 45.5 0.53  SM 104.1 1668 10.4 45.5 0.66  SM 101.3 1623 24.4 99.3 0.66							 						
SN-SN 111.3 1783 11.7 61.7 0.51 SN-SN 114.1 1828 10.5 59.3 0.48 SN 116.3 1895 8.5 54.4 0.42 SN 109.6 1756 10.8 59.2 0.54 SN 116.0 1858 9.7 57.0 0.45 SN 116.0 1858 9.7 57.0 0.45 SN 118.4 1897 9.7 61.8 0.42 SN 118.4 1897 9.7 61.8 0.42 SN 107.1 1716 12.0 56.8 0.57 SN 111.3 1783 13.3 69.8 0.51 SP-SN 114.5 1834 10.7 61.5 0.47 SN 98.8 1583 14.6 56.0 0.71 SN 98.8 1583 14.6 56.0 0.71 SN 100.3 1607 6.6 26.2 0.68 CN-CN 102.7 1645 15.5 65.4 0.64 SP 102.2 1637 3.5 14.7 0.65 SP 104.9 1680 4.3 19.0 0.61 SN 10.1 1764 15.5 78.9 0.53 SN 10.1 1764 15.5 78.9 0.53 SN 98.7 1581 6.2 23.7 0.71 ML 105.6 1692 6.9 31.2 0.60 SN 98.8 13.3 14.6 59.3 0.51 SN 98.9 14.5 176 51.1 9.4 0.71 SN 11.4 1784 11.2 59.3 0.51 SN 11.5 1846 12.9 68.4 0.87 SN 98.7 1581 6.2 0.9 31.2 0.60 SN 11.6 1820 16.3 91.3 0.48 SN 11.6 1820 16.3 91.3 0.48 SN 11.6 1820 16.3 91.3 0.48 SN 11.6 1820 16.3 91.3 0.48 SN 11.6 1820 16.3 91.3 0.48 SN 11.6 1820 16.3 91.3 0.48 SN 11.6 1820 16.3 91.3 0.48 SN 11.6 1850 7.4 44.2 0.45 SN SN 11.8 1791 13.6 72.4 0.51 SN SN 11.8 1791 13.6 72.4 0.51 SN SN 11.8 1791 13.6 72.4 0.51 SN SN 11.8 1791 13.6 72.4 0.51 SN SN 11.0 1765 14.4 73.5 0.53 SN SN 110.2 1765 14.4 73.5 0.53 SN SN 110.2 1765 14.4 73.5 0.53 SN SN 110.1 1668 10.4 45.5 0.62	SW	111.6	1788	12.2	64.8	0.51					L	•	L
SW-SM       114.1       1828       10.5       59.3       0.48         SM       116.3       1895       8.5       54.4       0.42         SM       109.6       1756       10.8       59.2       0.54         SM       116.0       1858       9.7       57.0       0.45         SM       121.7       1949       10.7       75.0       0.39         SM       118.4       1897       9.7       61.8       0.42         SM       107.1       1716       12.0       56.8       0.57         SM       107.1       1716       12.0       56.8       0.57         SW       111.3       1783       13.3       69.8       0.51         SP-SM       114.5       1834       10.7       61.5       0.47         SM       100.3       1607       6.6       26.2       0.68         GW-CM       102.7       1645       15.5       65.4       0.64         GW-GM       109.4       1752       2.9       14.5       0.54         SP       104.9       1680       4.3       19.0       0.61         SW       91.0       1764       15.5 <th< th=""><th>SM</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></th<>	SM												
SW-SM 114.1 1828 10.5 59.3 0.48 SM 116.3 1895 8.5 54.4 0.42 SM 109.6 1756 10.8 59.2 0.54 SM 121.7 1949 10.7 75.0 0.39 SM 121.7 1949 10.7 75.0 0.39 SM 107.1 1716 12.0 56.8 0.57 SM 107.1 1716 12.0 56.8 0.57 SW 111.3 1783 13.3 69.8 0.51 SP-SM 114.5 1834 10.7 61.5 0.47  SM 98.8 1583 14.6 56.0 0.71 SM 100.3 1607 6.6 26.2 0.68 GN-GM 102.7 1645 15.5 55.4 0.64 GW-GM 109.4 1752 2.9 14.5 0.54 SP 102.2 1637 3.5 14.7 0.65 SP 104.9 1680 4.3 19.0 0.61 SW 110.1 1764 15.5 78.9 0.53 SW 98.7 1581 6.2 23.7 0.71 ML 105.6 1692 6.9 31.2 0.60 SM 98.4 1576 5.1 19.4 0.71 SM 113.6 1820 16.3 91.3 0.48 SM 113.6 1820 16.3 91.3 0.48 SM 99.3 1446 15.5 15.0 0.77 SM 113.6 1820 16.3 91.3 0.48 SM 99.3 1446 15.5 15.0 0.77 SM 98.4 1576 5.1 19.4 0.77 SM 98.5 1581 6.2 23.7 0.71 SM 113.6 1820 16.3 91.3 0.48 SM 99.3 1446 21.9 68.4 0.87 SM 90.3 1446 22.9 60.0 SM 91.0 13.6 1820 16.3 91.3 0.48 SM 90.3 1446 22.9 60.4 0.87 SM 90.3 1687 16.5 74.2 0.60 SM 91.0 1888 7.4 44.2 0.45 SM 91.0 1 1668 10.4 47.5 0.53 SM 90.3 1687 16.5 74.2 0.60 SM 91.0 1 1668 10.4 45.5 0.62	SW-SM	111.3	1783	11.7	61.7	0.51							
SM 116.3 1895 8.5 54.4 0.42  SM 109.6 1756 10.8 59.2 0.54  SM 116.0 1858 9.7 57.0 0.45  SM 121.7 1949 10.7 75.0 0.39  SM 118.4 1897 9.7 61.8 0.42  SM 107.1 1716 12.0 56.8 0.57  SM 111.3 1783 13.3 69.8 0.51  SP-SM 114.5 1834 10.7 61.5 0.47  SM 98.8 1583 14.6 56.0 0.71  SM 100.3 1607 6.6 26.2 0.68  CM-CM 102.7 1645 15.5 65.4 0.64  CM-CM 102.7 1645 15.5 65.4 0.64  CM-CM 109.4 1752 2.9 14.5 0.54  SP 102.2 1637 3.5 14.7 0.65  SP 104.9 1680 4.3 19.0 0.61  SW 110.1 1764 15.5 78.9 0.53  SW 98.7 1581 6.2 23.7 0.71  ML 105.6 1692 6.9 31.2 0.60  SM 98.4 1576 5.1 19.4 0.71  SM 113.6 1820 16.3 91.3 0.48  SM 90.3 1446 21.9 68.4 0.87  SM 90.3 1446 21.9 68.4 0.87  SM 90.3 1446 21.9 68.4 0.87  SM 110.1 1765 14.4 73.5 0.53  SM 90.3 1446 21.9 68.4 0.87  SM 110.2 1765 14.4 73.5 0.53  SM 110.2 1765 14.4 73.5 0.53  SM 100.3 1687 16.5 74.2 0.60  SM 9M 110.1 1668 10.4 45.5 0.62	SW-SM	114.1	1828	10.5									
SM 116.0 1858 9.7 57.0 0.45 SM 121.7 1949 10.7 75.0 0.39 SM 118.4 1897 9.7 61.8 0.42 SM SM 107.1 1716 12.0 56.8 0.57 SW 111.3 1783 13.3 69.8 0.51 SP-SM 114.5 1834 10.7 61.5 0.47  SM 98.8 1583 14.6 56.0 0.71 SM 100.3 1607 6.6 26.2 0.68 GM-GM 109.4 1752 2.9 14.5 0.54 SP 102.2 1637 3.5 14.7 0.65 SP 104.9 1680 4.3 19.0 0.61 SW 110.1 1764 15.5 78.9 0.53 SW 98.7 1581 6.2 23.7 0.71 ML 105.6 1692 6.9 31.2 0.60 SM 98.4 1576 5.1 19.4 0.71 SM 98.4 1576 5.1 19.4 0.71 SM 113.6 1820 16.3 91.3 0.48 SM 99.3 1446 21.9 68.4 0.87 SM 99.3 1446 21.9 68.4 0.87 SM 99.3 1446 21.9 68.4 0.87 SM 99.3 1446 21.9 68.4 0.87 SM 90.3 1687 16.5 7.4 44.2 0.45 SM-SM 111.8 1791 13.6 72.4 0.51 SM 91.0 1 1668 10.4 45.5 0.62	SM	116.3	1895	8.5									
SM 121.7 1949 10.7 75.0 0.39 SM 118.4 1897 9.7 61.8 0.42 SM 107.1 1716 12.0 56.8 0.57 SM 111.3 1783 13.3 69.8 0.51 SP-SM 114.5 1834 10.7 61.5 0.47  SM 98.6 1583 14.6 56.0 0.71 SM 100.3 1607 6.6 26.2 0.68 CM-GM 102.7 1645 15.5 65.4 0.64 GW-GM 109.4 1752 2.9 14.5 0.54 SP 102.2 1637 3.5 14.7 0.65 SP 104.9 1680 4.3 19.0 0.61 SW 110.1 1764 15.5 78.9 0.53 SW 98.7 1581 6.2 23.7 0.71 ML 105.6 1692 6.9 31.2 0.60 SM 98.4 1576 5.1 19.4 0.71 SM 98.4 1576 5.1 19.4 0.71 SM 98.5 132 1525 15.1 53.0 0.77 SM 133.6 1820 16.3 91.3 0.48 SM 99.3 1446 21.9 68.4 0.87 SM 99.3 1446 21.9 68.4 0.87 SM 99.3 1446 12.9 68.4 0.87 SM 111.8 1791 13.6 72.4 0.51 SM-SM 111.8 1791 13.6 72.4 0.53 SM 98.1 110.2 1765 14.4 73.5 0.53 SM 110.2 1765 14.4 73.5 0.53 SM 110.2 1765 14.4 73.5 0.53 SM 110.2 1765 14.4 73.5 0.53	SM	109.6	1756	10.8	59.2	0.54							
SM 107.1 1716 12.0 56.8 0.57 SM 111,3 1783 13.3 69.8 0.51 SP-SM 114.5 1834 10.7 61.5 0.47  SM 98.8 1583 14.6 56.0 0.71 SM 100.3 1607 6.6 26.2 0.68 GM-GM 102.7 1645 15.5 65.4 0.64 GW-GM 102.7 1645 15.5 65.4 0.64 SF 102.2 1637 3.5 14.7 0.65 SF 102.2 1637 3.5 14.7 0.65 SF 104.9 1680 4.3 19.0 0.61 SW 110.1 1764 15.5 78.9 0.53 SW 98.7 1581 6.2 23.7 0.71 ML 105.6 1692 6.9 31.2 0.60 SM 98.4 1576 5.1 19.4 0.71 SM 98.4 1784 11.2 59.3 0.51 SM 99.3 1446 21.9 68.4 0.87 SM 90.3 1446 21.9 68.4 0.87 SM 90.3 1446 21.9 68.4 0.87 SM 111.8 1791 13.6 72.4 0.51 SM 110.2 1765 14.4 73.5 0.53 SM 105.3 1687 16.5 74.2 0.60 SM 110.2 1765 14.4 73.5 0.53 SM 100.3 1687 16.5 74.2 0.60 SM 110.4 1784 11.8 1791 13.6 72.4 0.51 SM 105.3 1687 16.5 74.2 0.60 SM 105.3 1687 16.5 74.2 0.60 SM 105.3 1687 16.5 74.2 0.60 SM 100.1 1668 10.4 45.5 0.62	SM	116.0	1858	9.7	57.0	0,45							
SM 107.1 1716 12.0 56.8 0.57 SW 111.3 1783 13.3 69.8 0.51 SP-SM 114.5 1834 10.7 61.5 0.47  SM 98.8 1583 14.6 56.0 0.71 SM 100.3 1607 6.6 26.2 0.68 GW-GM 102.7 1645 15.5 65.4 0.64 GW-GM 109.4 1752 2.9 14.5 0.54 SP 102.2 1637 3.5 14.7 0.65 SP 104.9 1680 4.3 19.0 0.61 SW 110.1 1764 15.5 78.9 0.53 SW 98.7 1581 6.2 23.7 0.71 ML 105.6 1692 6.9 31.2 0.60 SM 98.4 1576 5.1 19.4 0.71 SM 98.4 1576 5.1 19.4 0.71 SM 111.6 1820 16.3 91.3 0.48 SM 95.2 1525 15.1 53.0 0.77 SM 99.3 1446 21.9 68.4 0.87 SM 116.0 1858 7.4 44.2 0.45 SM-SM 111.8 1791 13.6 72.4 0.51 SM 110.2 1765 14.4 73.5 0.53 SM SM 105.3 1687 16.5 74.2 0.60 SM 110.2 1765 14.4 73.5 0.53 SM SM 110.2 1765 14.4 73.5 0.53 SM SM 110.2 1765 14.4 73.5 0.53	SM	121.7	1949	10.7	75.0	0.39							
SM 107.1 1716 12.0 56.8 0.57 SW 111.3 1783 13.3 69.8 0.51 SP-SM 114.5 1834 10.7 61.5 0.47  SM 98.8 1583 14.6 56.0 0.71 SM 100.3 1607 6.6 26.2 0.68 GW-GM 102.7 1645 15.5 65.4 0.64 GW-GM 109.4 1752 2.9 14.5 0.65 SP 104.9 1680 4.3 19.0 0.61 SW 110.1 1764 15.5 78.9 0.53 SW 10.1 1764 15.5 78.9 0.53 SW 98.7 1581 6.2 23.7 0.71 ML 105.6 1692 6.9 31.2 0.60 SM 98.4 1576 5.1 19.4 0.71 SM 111.4 1784 11.2 59.3 0.51 SM 113.6 1820 16.3 91.3 0.48 SM 95.2 1525 15.1 53.0 0.77 SM 99.3 1446 21.9 68.4 0.87 SM 90.3 1685 7.4 44.2 0.45 SM-SM 111.8 1791 13.6 72.4 0.51 SM 111.8 1791 13.6 72.4 0.51 SM 110.2 1765 14.4 73.5 0.53 SM 110.2 1765 14.4 73.5 0.53 SM SM 100.1 1765 14.4 73.5 0.53 SM SM 100.1 1765 14.4 73.5 0.53	SM	118.4	1897	9.7	61.8	0.42							
SW 111.3 1783 13.3 69.8 0.51  SP-SM 114.5 1834 10.7 61.5 0.47  SM 98.8 1583 14.6 56.0 0.71  SM 100.3 1607 6.6 26.2 0.68  GW-GM 102.7 1645 15.5 65.4 0.64  GW-GM 109.4 1752 2.9 14.5 0.54  SP 102.2 1637 3.5 14.7 0.65  SP 104.9 1680 4.3 19.0 0.61  SW 110.1 1764 15.5 78.9 0.53  SW 98.7 1581 6.2 23.7 0.71  ML 105.6 1692 6.9 31.2 0.60  SM 98.4 1576 5.1 19.4 0.71  SM 111.4 1784 11.2 59.3 0.51  SM 113.6 1820 16.3 91.3 0.48  SM 95.2 1525 15.1 53.0 0.77  SM 90.3 1446 21.9 68.4 0.87  SM 116.0 1858 7.4 44.2 0.45  SM SM 111.8 1791 13.6 72.4 0.51  SM 110.2 1765 14.4 73.5 0.53  SM 110.2 1765 14.4 73.5 0.53  SM SM 110.2 1765 14.4 73.5 0.53	SM												
SP-SM 114.5 1834 10.7 61.5 0.47  SN 98.8 1583 14.6 56.0 0.71  SM 100.3 1607 6.6 26.2 0.68  GW-GM 102.7 1645 15.5 65.4 0.64  GW-GM 109.4 1752 2.9 14.5 0.54  SP 102.2 1637 3.5 14.7 0.65  SP 104.9 1680 4.3 19.0 0.61  SW 110.1 1764 15.5 78.9 0.53  SW 98.7 1581 6.2 23.7 0.71  ML 105.6 1692 6.9 31.2 0.60  SM 98.4 1576 5.1 19.4 0.71  SM 111.4 1784 11.2 59.3 0.51  SM 113.6 1820 16.3 91.3 0.48  SM 95.2 1525 15.1 53.0 0.77  SM 90.3 1446 21.9 68.4 0.87  SM 111.8 1791 13.6 72.4 0.51  SM 105.3 1687 16.5 74.2 0.60  SM 98 104.1 1668 10.4 45.5 0.62	SM	107.1	1716	12.0	56.8	0.57							
SM 98.8 1583 14.6 56.0 0.71  SM 100.3 1607 6.6 26.2 0.68  CW-GM 102.7 1645 15.5 65.4 0.64  GW-GM 109.4 1752 2.9 14.5 0.54  SP 102.2 1637 3.5 14.7 0.65  SP 104.9 1680 4.3 19.0 0.61  SW 110.1 1764 15.5 78.9 0.53  SW 98.7 1581 6.2 23.7 0.71  ML 105.6 1692 6.9 31.2 0.60  SM 98.4 1576 5.1 19.4 0.71  SM 98.4 1576 5.1 19.4 0.71  SM 113.6 1820 16.3 91.3 0.48  SM 95.2 1525 15.1 53.0 0.77  SM 90.3 1446 21.9 68.4 0.87  SM 116.0 1858 7.4 44.2 0.45  SW-SM 111.8 1791 13.6 72.4 0.51  SM 102.1 1765 14.4 73.5 0.53  SM 110.2 1765 14.4 73.5 0.53  SM 110.2 1765 14.4 73.5 0.53  SM 104.1 1668 10.4 45.5 0.62	SW	111.3	1783	13.3	69.8	0.51							
SM 100.3 1607 6.6 26.2 0.68  CW-GM 102.7 1645 15.5 65.4 0.64  GW-GM 109.4 1752 2.9 14.5 0.54  SP 102.2 1637 3.5 14.7 0.65  SP 104.9 1680 4.3 19.0 0.61  SW 110.1 1764 15.5 78.9 0.53  SW 98.7 1581 6.2 23.7 0.71  ML 105.6 1692 6.9 31.2 0.60  SM 98.4 1576 5.1 19.4 0.71  SM 111.4 1784 11.2 59.3 0.51  SM 113.6 1820 16.3 91.3 0.48  SM 95.2 1525 15.1 53.0 0.77  SM 90.3 1446 21.9 68.4 0.87  SM 116.0 1858 7.4 44.2 0.45  SW-SM 110.2 1765 14.4 73.5 0.53  SM 100.1 1668 10.4 45.5 0.62	SP-SM	114.5	1834	10.7	61.5	0.47							
SM 100.3 1607 6.6 26.2 0.68  CW-GM 102.7 1645 15.5 65.4 0.64  GW-GM 109.4 1752 2.9 14.5 0.54  SP 102.2 1637 3.5 14.7 0.65  SP 104.9 1680 4.3 19.0 0.61  SW 110.1 1764 15.5 78.9 0.53  SW 98.7 1581 6.2 23.7 0.71  ML 105.6 1692 6.9 31.2 0.60  SM 98.4 1576 5.1 19.4 0.71  SM 111.4 1784 11.2 59.3 0.51  SM 113.6 1820 16.3 91.3 0.48  SM 95.2 1525 15.1 53.0 0.77  SM 90.3 1446 21.9 68.4 0.87  SM 116.0 1858 7.4 44.2 0.45  SW-SM 110.2 1765 14.4 73.5 0.53  SM 100.1 1668 10.4 45.5 0.62													
GW-GM 102.7 1645 15.5 65.4 0.64  GW-GM 109.4 1752 2.9 14.5 0.54  SP 102.2 1637 3.5 14.7 0.65  SP 104.9 1680 4.3 19.0 0.61  SW 110.1 1764 15.5 78.9 0.53  SW 98.7 1581 6.2 23.7 0.71  ML 105.6 1692 6.9 31.2 0.60  SM 98.4 1576 5.1 19.4 0.71  SM 111.4 1784 11.2 59.3 0.51  SM 113.6 1820 16.3 91.3 0.48  SM 95.2 1525 15.1 53.0 0.77  SM 90.3 1446 21.9 68.4 0.87  SM 116.0 1858 7.4 44.2 0.45  SW 105.3 1687 16.5 74.2 0.60  SM 105.3 1687 16.5 74.2 0.60  SM 106.1 1668 10.4 45.5 0.62	SM	98.8	1583	14.6	56.0	0.71							
GW-GM 109.4 1752 2.9 14.5 0.54  SP 102.2 1637 3.5 14.7 0.65  SP 104.9 1680 4.3 19.0 0.61  SW 110.1 1764 15.5 78.9 0.53  SW 98.7 1581 6.2 23.7 0.71  ML 105.6 1692 6.9 31.2 0.60  SM 98.4 1576 5.1 19.4 0.71  SM 111.4 1784 11.2 59.3 0.51  SM 113.6 1820 16.3 91.3 0.48  SM 95.2 1525 15.1 53.0 0.77  SM 90.3 1446 21.9 68.4 0.87  SM 105.3 1687 16.5 74.2 0.60  SM 105.3 1687 16.5 74.2 0.60  SM 100.1 1668 10.4 45.5 0.62	SM	100.3	1607		26.2	0.68							
SP       102.2       1637       3.5       14.7       0.65         SP       104.9       1680       4.3       19.0       0.61         SW       110.1       1764       15.5       78.9       0.53         SW       98.7       1581       6.2       23.7       0.71         ML       105.6       1692       6.9       31.2       0.60         SM       98.4       1576       5.1       19.4       0.71       •       •         SM       111.4       1794       11.2       59.3       0.51       •       •       •         SM       113.6       1820       16.3       91.3       0.48       •<	GW-GM	102.7	1645	15.5	65.4	0.64							
SP       104.9       1680       4.3       19.0       0.61         SW       110.1       1764       15.5       78.9       0.53         SW       98.7       1581       6.2       23.7       0.71         ML       105.6       1692       6.9       31.2       0.60         SM       98.4       1576       5.1       19.4       0.71       •       •         SM       111.4       1784       11.2       59.3       0.51       •       •       •         SM       113.6       1820       16.3       91.3       0.48       • </th <th>GW-GM</th> <th>109.4</th> <th>1752</th> <th>2.9</th> <th>14.5</th> <th>0.54</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>	GW-GM	109.4	1752	2.9	14.5	0.54							
SW       110.1       1764       15.5       78.9       0.53         SW       98.7       1581       6.2       23.7       0.71          ML       105.6       1692       6.9       31.2       0.60           SM       98.4       1576       5.1       19.4       0.71 </th <th>SP</th> <th>102.2</th> <th>1637</th> <th>3.5</th> <th>14.7</th> <th>0.65</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>	SP	102.2	1637	3.5	14.7	0.65							
SW       98.7       1581       6.2       23.7       0.71 <t< th=""><th>SP</th><th>104.9</th><th>1680</th><th>4.3</th><th>19.0</th><th>0.61</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></t<>	SP	104.9	1680	4.3	19.0	0.61							
ML 105.6 1692 6.9 31.2 0.60  SM 98.4 1576 5.1 19.4 0.71  SM 111.4 1784 11.2 59.3 0.51  SM 113.6 1820 16.3 91.3 0.48  SM 95.2 1525 15.1 53.0 0.77  SM 90.3 1446 21.9 68.4 0.87  SM 116.0 1858 7.4 44.2 0.45  SW-SM 111.8 1791 13.6 72.4 0.51  SM 105.3 1687 16.5 74.2 0.60  SM 110.2 1765 14.4 73.5 0.53  SM 104.1 1668 10.4 45.5 0.62	SW	110.1	1764	15.5	78.9	0.53							
SM 98.4 1576 5.1 19.4 0.71	SW	98.7	1581	6.2									
SM       111.4       1784       11.2       59.3       0.51       •         SM       113.6       1820       16.3       91.3       0.48          SM       95.2       1525       15.1       53.0       0.77           SM       90.3       1446       21.9       68.4       0.87           SM       116.0       1858       7.4       44.2       0.45            SW-SM       111.8       1791       13.6       72.4       0.51              SM       105.3       1687       16.5       74.2       0.60 <th>ML</th> <th>105.6</th> <th>1692</th> <th>6.9</th> <th>31,2</th> <th>0.60</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>	ML	105.6	1692	6.9	31,2	0.60							
SM       113.6       1820       16,3       91.3       0.48         SM       95.2       1525       15.1       53.0       0.77         SM       90.3       1446       21.9       68.4       0.87         SM       116.0       1858       7.4       44.2       0.45         SW-SM       111.8       1791       13.6       72.4       0.51         SM       105.3       1687       16.5       74.2       0.60         SM       110.2       1765       14.4       73.5       0.53         SM       104.1       1668       10.4       45.5       0.62	SM	98.4	1576		19.4	0.71			•			•	
SM       95.2       1525       15.1       53.0       0.77         SM       90.3       1446       21.9       68.4       0.87         SM       116.0       1858       7.4       44.2       0.45         SW-SM       111.8       1791       13.6       72.4       0.51         SM       105.3       1687       16.5       74.2       0.60         SM       110.2       1765       14.4       73.5       0.53         SM       104.1       1668       10.4       45.5       0.62	SM		1784						•				
SM     90.3     1446     21.9     68.4     0.87       SM     116.0     1858     7.4     44.2     0.45       SW-SM     111.8     1791     13.6     72.4     0.51       SM     105.3     1687     16.5     74.2     0.60       SM     110.2     1765     14.4     73.5     0.53       SM     104.1     1668     10.4     45.5     0.62	SM		1820				 	 		 			
SM     116.0     1858     7.4     44.2     0.45       SW-SM     111.8     1791     13.6     72.4     0.51       SM     105.3     1687     16.5     74.2     0.60       SM     110.2     1765     14.4     73.5     0.53       SM       SM     104.1     1668     10.4     45.5     0.62	SM		1525		53.0	0.77	 	 		 			
SW-SM     111.8     1791     13.6     72.4     0.51       SM     105.3     1687     16.5     74.2     0.60       SM     110.2     1765     14.4     73.5     0.53       SM     104.1     1668     10.4     45.5     0.62	SM	90.3	1446	21.9	68.4	0.87	 			 			
SM     105.3     1687     16.5     74.2     0.60       SM     110.2     1765     14.4     73.5     0.53       SM          SM     104.1     1668     10.4     45.5     0.62	SM	116.0	1858	7.4	44,2	0.45							
SM     110.2     1765     14.4     73.5     0.53       SM          SM     104.1     1668     10.4     45.5     0.62	SW-SM	111.8	1791	13.6	72,4	0.51							
SM 104.1 1668 10.4 45.5 0.62	SM	105.3	1687	16.5	74.2	0.60							
SM 104.1 1668 10.4 45.5 0.62	SM	110.2	1765	14.4	73.5	0.53							
	SM												
RM 101.3 1623 24.4 99.3 0.66	SM												
	SM	101.3	1623	24.4	99.3	0.66							

(a) Sample types

- (c) USCS Unified Soil Classification System
- 35 Standard split spoon
- P Pitcher
- (d) \* Indicates that test has been performed and results are included in this report
- 0 Fugro Drive
- B.b Bulk
- (b) MP Not Plastic

67	26	1 8	l 5		ı	I		1	SP-SM		i 1	Ī '	ı	I	ī	1	1	ī	
			1	1		<b></b>			SP-SM							1	<del></del>	$\vdash$	1
77	30	13	7			1	<b>†</b>		SW-SM	113.5	1818	6.1	34.3	0.48		<del> </del>		1	1
			1	1	1				SM	107.1	1716	4.0	19.1					1	1
100	81	57	33					NP	SM	85.5	1370	15.3				1	1		1
1						<u> </u>			SP-SM	117.0	1874	6.9							T
45	16	6	5						SP-SM	113.9	1825	14.0				1	1	1	T
									SP-SM							1		1	Ħ
				1					SM	107.9	1728	14,3	68.6	0.56				1	T
98	88	66	49						SM	98.8	1583	11.4				1	1	1	
									SP-SM	103.2	1653	8.5	36,3	0,63					
		<u> </u>						L,	SM				L				_1		
	ļ	<b>.</b>		L		<u> </u>		L	SM	108.6	1740	8.7	42.6					I	3
100	77	40	23		<b> </b>	<u> </u>	L	Ļ	SM	97.2	1557	14.0						<b>.</b>	$oldsymbol{\Box}$
1	L	<u> </u>		l	<u> </u>			L	SP	102.5	1642	19.2						l	$\mathbf{L}$
		L		<b></b>		<b>!</b>	ļ		SP	111.4	1784	13.0	68.6	0.51		<u> </u>		1	
100	94	8	2	l	<b>}</b>	ļ		L	SP							<del></del> -		<u> </u>	L
		ļ	ļ	ļ			<b></b>		SP	103.9		5.5	24.0					1	L
			<del> </del> _		<b></b>	ļ		<b></b>	SP	106.5		12.5				<del></del>		<b> </b>	L
75	40	13	6			<b>!</b>		<b>├</b> —-	SP-SM	108.4	1736	16.8	81.7	0.55				<b>↓</b>	L
4				<u> </u>	<b> </b>	<b> </b>	<u> </u>		SP				<b> </b>	<u> </u>		<b></b>		<b>↓</b>	L
		<b>!</b>	<b>!</b>	-		<b>.</b>	Ļ								<del> </del>	<del> </del>		↓	L
		<b> </b>	<b>!</b>	<del>   </del>	<b> </b>	<b>!</b>	<b>-</b>	<u> </u>	SP-SM	94.2	1509					→—		1	H
H	<u> </u>	<b>!</b>	-	l	<u> </u>	<del> </del>	├	<b> </b>	SM	114.3		5.1	28.8			<del>- </del>		<b> </b>	Ļ
		<b> </b>	<del>                                     </del>	<del> </del>	<b></b>	<b> </b>	├	<b></b>	SM	89.6	1435	15,7				<del>- </del>		<b></b>	H
-			<del> </del>		<u> </u>	<b>├</b> ──		<b>-</b>	SM	90.8	1454	9.1	28.7			┥—	<del></del>	<b>∔</b>	H
78	58	32	18	<del> </del>	<b> </b>				SM	110.5		11,9	61.3			<del></del>		<del> </del>	14
					<b>}</b>		ļ		SW-SM	116.8		11.6				<del>- </del>		<b> </b>	14
4		<del> </del>	<del>}</del>	<del> </del>	<b></b>	<del> </del>	}	-	SW-SM ML	112.7 78.2	1805 1253	11.1				<del> </del> -		<del> </del>	Н
	-		<del> </del>		<del> </del>			-	SP	105.6		21.7 14.5				<del> </del>		<b>├</b> ──	14
		<b></b>	<del>                                     </del>	<del>                                     </del>	<del>                                     </del>				SP	96.7	1549	17.7				┪	<del>- </del>	<del> </del>	H
1					<b></b>	<b>†</b>	1-	<b> </b>	SP	113.3		11.2				1	+	<del> </del>	H
		<b></b>	<del> </del>	<b>†</b>	<b></b>	<del>                                     </del>	1	_	SP	109.4		11.8				1	+	<del>                                     </del>	H
1	<b>-</b>		1	<b>†</b>		t			<del></del>		<del></del> -	<del></del>	† <del> • •</del>	<u> </u>		1	<del>                                     </del>	<del>                                     </del>	H
100	99	91	80	1	<b></b>	<b>†</b>	<u> </u>		MH	70.9	1136	21.1	41.4	1.30		1	+	2.62	H
<b>1</b>		<del>                                     </del>	99	t		58	38	20	MH	68.1	1091		72.0			1	+	† <del>* : ` * *</del>	H
			1				<u> </u>		SP	95.1	1523		66.2			1	<del></del>	t	Ħ
96	67	30	15			33	22	11	SC	100.9		13.3				1	1	1	Ħ
100	99	91	77			51	31	20	MH	77.5	1241	35.4				1	+	<del> </del>	H
		<u> </u>	<u> </u>	1		79	36	43	МН	87.8	1406	18.1				1	+	2.66	Ħ
									МН	81.8	1310	22.6	57.7	1,06				t <del></del>	Ħ
																			- 1

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				 <u> </u>
<u> </u>				 
<b></b>	<del></del>	<b></b>		 <b></b>
I	J			

	(3)								PERCE	NT FIN	ER BY	REIGHT	
[ 🖺 🚾 ]		SAMPLE 1	NTERVAL		2	TANDAR	B SIEV	E OPEN	ING		U S	STAI	NDA
ACTIVITY Number	SAMPLE Number			BLDRS	COBE	LES		GRA	VEL			SI	1110
2 2	Z ≡	FEET	METERS	24"	12"	6"	3"	1ኝ"	3/4"	3/8"	4	10	
RR-B-4	P-9	30.1-30.5	9.17-9.30										
	P-10	33.0-35.0	10.06-10.67										
	P-11	35.0-36.9	10.67-11.25										Γ
	P-12	40.0-40.7	12.19-12.41							I			
	P-13	50.0-51.7	15.24-15.76										
	P-14	60.0-62.8	18.29-19.14			L	L				I	L	L
	P-15	70.0-72.8	21.34-22.19			Ĺ							
	P-16	80.8-81.6	24.63-24.87										
	P-17	90.0-92.1	27.43-28.07							100	98	97	
	P-18	100.0-102.4	30.48-31.21										$\Gamma$
	P-19	110.0-112.8	33,53-34.38	L]							100	98	$\Box$
	P-20	120.0-121.1	36,58-36.91				ļ		<b> </b>				
	P-21	140.0-141.6	42.67-43.16	l			ļ		L	ļ	100	99	
<u> </u>	P-22	160.0-161.8	48.77-49.32	ļ					<b> </b>	<b></b>		ļ	_
RR-B-5	P-1	0.0-1.2	0.00-0.37				<del> </del>		<del> </del>	<del> </del>	<del> </del>	<del> </del>	╀
	D-3	3.6-4.3	1.10-1.31	<b>-</b>		<b></b>	<del> </del>	100	95	79	61	44	1 7
	D-4	7.2-7.9	2.19-2.41	·			<del> </del>	100	87	62	46	34	ti
	D-5	10.2-10.8	3.11-3.29	1 1			t	-	<del>                                     </del>	<u> </u>	1 33	<del> </del>	╅╸
	D-6	15.0-15.6	4.57-4.75				100	81	62	49	40	34	1
	D-7	20.0-20.5	6.10-6.25	1		<b></b>	<b>†</b>				1	<del></del>	オ╌
	D-9	30.0-30.6	9.14-9.33	1 1	,	·	† i	100	81	74	59	37	Ti
	D-10	35.0-35.5	10.67-10.82				1						✝₹
	D-11	40.0-40.4	12.19-12.31						100	88	78	67	17
	D-12	50.2-50.9	15.30-15.51								<u> </u>		М
	D-14	70.0-70.3	21.34-21.43				1	100	81	60	45	37	1
	D-16	90.0-90.7	27.43-27.65										
	D-17	100.0-100.6	30.48-30.66					100	96	83	56	32	П
	D-18	110.0-110.5	33.53-33.68				100	70	61	48	37	26	1
		120.0-120.2	36.58-36.64		· · · · · · · · · · · · · · · · · · ·	<b></b>	<del>Ĭ</del>	<del>ٺ</del>	<del>  ~</del>		<del>                                     </del>	<b>├</b> ▔	┪
	D-20	140.0-140.2	42.67-42.73					100	85	71	59	46	1
	D-21	160.0-160.2	48,77-48,83					100	96	77	65	48	T
RR-B-6	P-1	0.0-1.4	0.00-0.43			Ī					I		П
	D-3	3.7-4.4	1.13-1.34			I		100	96	86	69	49	T
	D-4	7.2-7.9	2.19-2.41			<u> </u>							П
	D-5	10.3-10.9	3.14-3.32								I		
	D-6	15.2-15.9	4.63-4.85				1		T				Т
	D-7	20.0-20.4	6.10-6.22					100	92	75	57	41	1
	D-8	25.0-25.6	7.62-7.80										П
	D-9	30.0-30.7	9.14-9.36							<u> </u>	<del>                                     </del>		1
	D-10	35.0-35.5	10.07-10.82				<b>—</b>		<u> </u>				
	D-11	40.2-40.9	12.25-12.47					100	82	72	60	41	П

(a) Sample types

- (c) USCS Unified Soil Classification System
- \$\$ Standard split spoon
- P Pitcher

B - Fugro Drive

- (d) \* Indicates that test has been performed and results are included in this report
- B,b Bulk
- (b) NP Not Plastic

EIGHT											110	-S 1 TU			C	OMPACTE			Г
STAR	IDARO S	IEVE N		PART SIZE T OR C	(mm)		TERBE IITS (		U <b>S</b> CS (c)	DRY (	JN I T GHT	MOISTURE CONTENT (\$)	SATURATION (\$)	VOID RATIO	MAX DRY DE		OPTIBUE BOISTURE (S)	SPECIFIC GRAVITY OF SOLIDS	
10	40	100	200	.005	.001	ĬĬ.	PL	PI		(pcf)	$(kg/n^3)$	<b>2</b> 8	S	무조	(pcf)	(kg/m²)	3 =	222	L
<u> </u>									ML										Γ
	<del>} }</del>		<u> </u>		<del>                                     </del>	41	29	12	ML	87.6	1403	8.3	24.3	0.92		1			Γ
				<b></b> -			<del></del>		ML	85.7	1373	31.0	86.6	0.97					Ĺ
				<b></b>		50	34	16	ML-MH	79.8	1278	34.5	83.7	1.11					L
	1				<b>-</b>	<b>                                     </b>	_		SM	97.7	1565	7.9	29.5				1		Ļ
	1							T	ML	80.9	1296	30,0	74.9	1.08		<u> </u>	L	L	L
<del> </del>	<b>†</b>		<b>1</b>	<b>†</b>		52	34	18	MH							L	<u> </u>		Ł
				1		44	32	12	ML	81.7	1309	36.6	93.2			<u> </u>	L		ļ
97	96	96	95	1		36	29	7	ML	89.4	1432	30.9		0.89		<b></b>	<u> </u>	<b></b>	1
<u> </u>								$\Box$	ML	88.4	1416	31.9		0,91	l	<b>]</b>	<b>↓</b>	<b></b> _	1
98	71	41	27		1	1			SM	105,5	1690	18.3		0.60	<u> </u>	L	L	<b></b>	ļ
			<u> </u>	Ì .					SM	105.6	1690	20.5	93,2	0,60	L	<b>↓</b>	<b></b>	<b> </b>	ł
99	88	68	48	I				<u> </u>	SM	94.4	1512	28.4		0.79		↓	<del> </del>	<b>↓</b>	ł
i								<u> </u>	SM	90.7	1453	29.6	93.2	0.86		<b>↓</b>	↓	<b>}</b>	ł
			I					<u> </u>	<u> </u>	<u> </u>	1	<b>!</b>	<b>!</b>	<b> </b>	<b></b>	<del>   </del>	<del> </del>	<b>}</b>	ł
1					$\Gamma_{}$	L	L	<u> </u>	SM	86.6	1387	10.1		0.95		↓	↓	<del>   </del>	ł
44	20	11	8				L		SW-SM	113.2	1813	3.8		0.49		<del> </del>	<b>↓</b> -	2.56	ł
34	19	12	10	Ι	$\Gamma$		<u> </u>	1_	GW-GM	112.6	1804	8.6		0.50		<b>}</b> -	<del> </del>	<b>∤</b> -	ł
				L	<u> </u>	<b>l</b> _	<u> </u>	<b></b>	GW-GM	113.6	1820	8.6		0.48		<b>├</b> -	<del> </del>	<del> </del>	ł
34	19	11	9_	<u> </u>		<u> </u>	<u> </u>	1	GW-GM	122.0	1954	8.4		0.38		<b>↓</b>	<del> </del>	<b>∤</b> -	ł
				l	l		<b>L</b>		GW-GM	110.2	1765	12.9	65.9			<del></del>	<del></del> -	<del> </del>	ł
37	18	12	9	L	L	1	<u> </u>	1	SP-SM	118.7	1901	11.9		0.42		<del> </del>	<del>}</del>	╂	ł
						<u> </u>	1	1	SP-SM	115.7	1853	11.6		0.46		<del> </del>	<del> </del>	<del>                                     </del>	ł
67	45	28	20			1	1	<del></del>	SM	113.8	1823	12.0		0.48		<del> </del>	<del> </del>	<del>\</del>	ł
						1	<b>_</b>	↓	SM	110.2	1785	12.8	65.7	0.53	<b></b>	<del> </del>	<del> </del>	<del></del>	+
37	25	16	11		1	1	1	<b>-</b>	GP-GM	<b> </b>	<del>                                     </del>	<del> </del>	<del> </del>	l	1	+	<del>                                     </del>	<b></b>	╁
					<u> </u>	1		<del></del>	GP-GM	117.2	1877	10.5		0.44		<del> </del>	<del> </del>	<del></del>	╂
32	11	7	6	<u> </u>	1	1	—	1	SW-SM	113.8	1823	15,2		0.48		<del> </del>	+	<del> </del>	┨
26	10	6	5	1	1				GW-GM	123.1	1972	9,9		0.37		<b>_</b>	<b>↓</b>	╂	+
					1	1_	<b>—</b>	↓	GW-GM	116.9				0.44		-∤	╅	<del> </del>	╁
46	23	14	11		↓		<del> </del>	↓_	SP-SM	119.4	1913			0.4		+	+	<b></b>	┪
48	21	12	10	<del> </del>	<del></del>	1		<del> </del>	SW-SM	119.2	1909	$\{11.7$	1/6.2	0.4	<del>'</del>	╅──	+	<del> </del>	1
1	<b>_</b>	L	<del> </del>		↓		<b></b>	-	·	<del> </del>	+ , , , , ,	1-22-	+ = = =	1, 7	<del></del>	-{	+	1	1
1	j		1	J		. <b>J</b>			SM	77.1	1235	1 24.7	56.2	: IT • T;	71	Í	1	•	1

		100	-SITU			C	OMPACTE			G	_ =				
<b>83C</b> 5 (c)	ORY U	NIT	MOISTURE CONTENT (\$)	SATURATION (\$)	VOID RATIO	MAXI DRY DE	MUM	OPTIBUM BOISTURE (\$)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (d)	UNCOMFINED COMPRESSION	DIRECT SHEAR	CONSOLIDATION	CHENICAL	CBR
ML															
ML	87.6	1403	8.3	24.3											
ML	85.7	1373	31.0		0.97										
ML-MH	79.8	1278	34.5	83.7	1.11										
SM	97.7	1565	7.9	29,5	0.72						<b>.</b>				
ML	80.9	1296	30,0	74.9	1.08						<b>.</b>				
MH										<u></u>	ļ				
ML	91.7	1309	36.6	93.2											
ML	89.4	1432	30.9	94.3							<b>.</b>	$\vdash$			
ML	88.4	1416	31.9	95,3	0,91			L			<u> </u>				
SM	105,5	1690	18.3	82,9 93,2	0.60			<b></b>			<b></b> -				
SM	105.6 94.4	1690	20.5	93,2	0.60		<u> </u>				<del>[</del> -			<b></b>	
SM	90.7	1512	28.4	97,6		·	<u> </u>				<b>}</b>				
SM	90.7	1453	29.6	93.2	0.80						<del> </del> — –	<b></b>			
SM	86.6	1387	10.1	28.9	000						<del> </del>				
SW-SM	113.2	1813	3.8	21.3	0.93		<del></del>		2.56		<del> </del>				
GW-GM	112.6	1804	8.6	47.0	0.50				2.30		<del> </del>	<del>  </del>			
GW-GM	113.6	1820	8.6	47.9	0.30						<del> </del>				
GW-GM	122.0	1954	8.4	59.9	0.38						<del>                                     </del>				
GW-GM	110.2	1765	12.9	65.9							<del> </del> -	1			
SP-SM	118.7	1901	11.9		0.42						†	1			
SP-SM	115.7	1853	11.6		0.46	· · · · · · · · · · · · · · · · · · ·	<del></del>				<del>                                     </del>				
SM	113.8	1823	12.0		0.48			1			<del>                                     </del>			Ť	
SM	110.2	1785	12.0	85.7	0.53						<b>†</b>				
GP-GM					1						t —				
GP-GM	117.2	1877	10.5	64.8	0.44						1				
SW-SM	113.8	1823	15,2	85.2							1				
GW-GM	123.1	1972	9.9	72.2	0.37										
GW-GM	116.9	1873	13.1	80.5	0.44										
SP-SM	119.4	1913	10.0	65.6	0.41										
SW-SM	119.2	1909	11.7	76.2	0.41										
			<u> </u>		<u> </u>		L				<u> </u>				
SM	77.1	1235	24.7								<b>!</b>				
SP-SM				15.0							<u> </u>				
SP-SM	119.8	1919	5.9	39.3	0.41		<u> </u>	L		L	<b></b>	lacksquare		ļ	
SP-SM			<b></b>	<u></u>						L	<u> </u>	L			
SW-SM	116.5	1866	6.2	37.6				<b></b>			<b> </b>				
SW-SM		1940					<b></b>	<b></b>		<u> </u>	<b> </b>	<b> </b>			
SP-SM	115.7	1853	9.7	57.7	0.46	<b></b>	<u> </u>	<b></b>	ļ		<b></b>	<b></b>			
SP-SM		<u> </u>		<b></b>	<b></b>		<u> </u>	<b> </b>		L	<u> </u>				
SP-SM		2103		100.0	0.28		<b></b>	<b></b>		ļ	<b>↓</b>	<b> </b>		ļ	igsqcut
SP-SM	117.5	1882	8,0	49.7	0.43		<u> </u>	L		L	<u> </u>				

SUMMARY OF LABORATORY TEST RESULTS

VERIFICATION SITE

REVEILE-RAILROAD COP. REVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAWSO

149LE 9-.1 3 07 0

**UBRO MATIONAL INC** 

					•				PERCE	NT FIN	R BY	MEIGHT
<b>   </b>	(E)	SAMPLE II	MTFRVAL		3	TANDARI	SIEV	E OPFN			U :	
ACTIVITY Number	SAMPLE Kunder	SAMPLE II	M15N v 45	BLDRS	COBE	BLES		GRA		SAI		
P P	S	FEET	METERS	24**	12"	6"	3"	15"	3/4"	3/8"	4	10
RR-B-6	D-12	50.5-50.9	15.39-15.51									
	D-13	60.0-60.7	18.29-18.50					100	83	56	41	30
	D-14	65.7-66.4	20.03-20.24			1						
	D-15	70.0-70.6	21.34-21.52									
	D-17	92.0-92.6	28.04-28.22									
	D-18	99.5-99.6	30.33-30.36									
	D-21	119.2-119.9	36.33-36.55					100	94	89	82	72
	D-22	140.1-140.6	42.70-42.85				100	85	74	61	49	38
	D-23	160.0-160.2	48.77-48.83					100	98	79	60	43
RR-T-1	B-1	0.5-2.0	0.15-0.61					100	95	87	79	71
<b></b>						<b>├</b>	ļ	ļ	<b> </b>			<b> </b>
RR-T-2	B-1	0.5-2.	0.15-0.61	ļ		<b></b>	<u> </u>	<u> </u>	100	97	87	71
			· <del></del>			<b>├</b>	<b> </b>					
RR-T-3	B-1	0.5-1.5	0.15-0.46			<b></b>	<u> </u>					l
<b></b>	b-4	7.0-8.0	2.13-2.44			ļ	<b></b>	<b>.</b>	ļ	100	99	95
	b-6	11.5-12.5	3.51-3.81	ļ		<b></b>		<b> </b>	<b></b>			<b>├</b>
<del></del>	b-7	13.0-14.0	3.96-4.27	<b>∤</b>		<b>}</b>		<b> </b>			<b></b>	<del>}                                    </del>
RR-T-4	-	0.35 1.5	0.08-0.46			<b> </b>	├	<del> </del>	<b></b> -			1 1
	9-1 b-3	0.25-1.5			<del></del>	}	<del> </del>	<u> </u>	100	-		100
	b-4	3.0-4.0	0.91-1.22			·	<b>}</b>		100	98	93	84
	<del></del>	7.0-8.0	2.13-2.44	<b>}</b> i		<b></b> -	<del> </del> -	ļ	100	87	68	45
RR-T-5	B-1	0.5-2.0	0 15-0 61		· :	<b>}</b>	100	01	59	49	41	1 34 1
	b-2	12.0-13.0	0.15-0.61 3 66-3.96				100	81 100	79	54	41	34
		22.0 23.0	3 66-3.96			<del></del>	<del>├</del> ─~	100	1/9	34	41	32
RR-T-6	B-1	0.5-2.0	0.15-0.61	<b></b>		<del></del>	<del> </del>	<del> </del>	100	99	96	90
				<del>\                                    </del>		<del>                                     </del>	$\vdash$	<del></del>	1-00	<del> </del>		┟╩┪
RR-T-7	B-1	0.5-2.0	0.15-0.61	1		<del>                                     </del>	100	99	98	96	89	78
				1		<del>                                     </del>	1 30	<del>  -</del>	<del> </del>	<del>  ~~</del>		<del>  '                                   </del>
RR-T-8	B-1	0.5-2.0	0.15-0.61			<del> </del>	t	100	97	85	72	50
	b-2	9.0-10.0	2.74-3.05					1				<u> </u>
RR-P-1	B-1	0.5-2.0	0.15-0.61			$\Gamma$	T	100	95	90	81	67
	b-2	2.5-3.5	0.76-1.07									
RR-P-4	B-1	1.0-1.5	0.30-0.40					100	88	74	56	46
RR-P-6	b-1	0.5-2.0	0.15-0.61						100	98	93	85
	b-2	2.5-3.5	0.76-1.07					100	89	68	52	40
RR-P-8	B-1	0.5-2.0	0.15-0.61						100	99	94	89
L												

(a) Sample types

- (c) USCS Unified Seil Classification System
- SS Standard split spoon
- P Pitcher
- (d) \* indicates that test has been performed and results are included in this report
- 0 Fugro Drive
- 8.b Bulk
- (b) NP Net Plastic

S. C.																						
											- 11	1-51TU			C	OMPACTE			(9)			
	DARD S	IEVE I		SIZE	( 📖 )		LIMITS (b)					ascs	DRY	UNIT	MOISTURE CONTENT (\$)	SATURATION (\$)		MAX DRY DE	1000 1 T Y	097:1888 80:5788E (5)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL
SA	MD 40	100	200	T OR C	.001	<del></del>		PI	(c)		B# 1			5 E		(NO 111	15 (S)	SEC.				
	40	100	200	.005	.001	LL	PL	<del>  ''</del>	GD GW	(pet)	(kg/m <sup>3</sup> )		<u>~</u>		(pel)	(hg/m³)						
0	11	5	3	<del>                                     </del>		<b> </b>	├		SP-SM GW	122.3	1959	8.4	78.6	0 30	<del></del>	<b> </b>	<u> </u>					
ř	**		,	<b> </b>		}	<del> </del>	<del> </del>	SM	115.9	1857	12.2		0.45		·						
		·			-	<b></b> -	<b> </b>	<del> </del>	SM	117.4	1881	12.0		0.44		f						
							<b></b>	<del>                                     </del>	GP-GC	117.2	1878	14.4	88.8				·					
									GP-GC													
21.0	53	40	33						SM	113.2	1813	10.5		0.49								
9	27	20	17			l			GM	124.4	1993	9.5		0.35								
3	22	11	7	<b> </b>		ļ		-	SW-SM	114.1	1828	11.4	64.7	0.48		<b></b>		ļ				
_	==			<b> </b>	ļ	<b> </b> -	ļ	1		<b>}</b>		<b> </b>	<b> </b>									
1	52	35	26	}	<b>{</b> -∤	<b>{</b> -	├	NP	SM	ł	<del> </del>	<del> </del>	<del> </del>		127.1	2036	8.9					
11	46	31	25	<b> </b>	<b></b>	<b>}</b>	<del> </del>	<del> </del>	SM	<del> </del>	<del> </del>	<del> </del>	<del> </del>	<del>  </del>		<del> </del>	<b></b>					
•				<b> </b>		<b> </b>	<b> </b>	<del>                                     </del>		<del> </del>	<del> </del> -	<del> </del>	<del> </del>	1		<del> </del>						
	100	99	97		<b>-</b>	44	30	14	ML	<b> </b>	1	1	1	1	84.6	1355	33.0					
5	33	2	1	1					SP	1	1	1	1		<del></del>		) . <del></del>					
			81			29	24	5	ML													
			95	l		50	34	16	MH													
		l	 	<b></b>		<b> </b>		l		<b>.</b>		<b>├</b>	ļ		100							
00 84 45	91	74	63	<b> </b>	<b></b> -	30	19	11	CL	<b> </b>	<del> </del>	<del>  </del>		<del> </del>	109.3	1751	17.5					
4	60 7	26 3	11 2	<b> </b>	ļ	ł	ł	ł	SP-SM SP	<b>}</b>	ł	<b> </b>		<del> </del>		<del> </del> -	·	·				
22	<del></del>	<del>  '</del> -	<del>  -</del> -	<del> </del>	<del> </del>	<del> </del>	├		SP_	ł	<del> </del>	<del> </del>	<del> </del>	<del>├</del> ──		<del> </del>						
24	28	24	19	<del> </del>	<del> </del>	<b> </b> -	<b> </b>	<del></del>	GM	<del> </del>	<del> </del>	<del> </del>	<del> </del> -	<del> </del>	<del></del>	<del> </del>		<b></b>	-			
32	23	16	9		<del>                                     </del>	1	_		GP-GM	<u> </u>	1	<del></del>	<del></del>		<del></del>	t						
						1				1	1	<del>                                     </del>	1			1						
0	71	49	37	17	6	22	17	5	SC-SM						127.0	2034	9.0					
78	50	31	25	9	5	42	24	18	SC	<b>.</b>	<b></b>	<b></b>	L	<b></b>	124.0	1986	11.5					
-	1.	<del>  10</del> -	-	<b> </b> -		<u> </u>	<b> </b>	<b>├</b> ──		<b>}</b>	<b>├</b> -	<del> </del>		<b> </b>		<b>}</b>	<b>}</b>	ļ				
50	17	10	8	<del> </del>	<del> </del>	<del> </del>		├	SW-SM GC	<del> </del>	<del> </del>	<del> </del>	<del> </del>	}	<del></del>	<del> </del>	<b>}</b>	<b></b>	-			
		<b></b> -	<b></b> -	<del> </del>	<del> </del>	<del> </del>	<b>-</b>	<del> </del>	<del>  ""</del>	t	<del>                                     </del>	<del> </del> -	<del> </del>	1			<b></b>					
67	47	30	16	<del> </del>	<b></b>	1-		1	SM	1	<del>                                     </del>	<del></del>	t			t	·	t				
				1				1	CL	1	1	<u> </u>	<b> </b>		<del></del>			<b>1</b>				
46	21	6	3					NP	SP													
85	64	42	31		L	L		<b> </b>	SM	<b></b>	ļ	ļ		<b></b>		<b></b>	L					
40	21	12	9			L	ļ	<u> </u>	SW-SM	<b> </b>	<b></b>	<b></b>		<b></b>			<b></b>					
25		<del></del> -			<b> </b>	<b></b>		<del> </del>	<del></del>	<b> </b>	<del> </del>	<b> </b>	}	<b> </b>	<b></b>	<b></b>	<b> </b>					
89	78	42	20		<del> </del>	<b>├</b> ─			SM	<del> </del>	<del> </del>	<del> </del>	<del> </del>		ļ. ——	<b> </b>	<del> </del>		-4			
		<u> </u>		<u> </u>		ــــــــــــــــــــــــــــــــــــــ	Щ_		<del></del>	<del></del>	ــــــــــــــــــــــــــــــــــــــ	<del></del>	Ь		<u> </u>	<u> </u>	<u> </u>	<b></b>				

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DEPART

			110	-SITU			C	OMPACTE	)					8		
	95C5 (c)	DRY U	IN I T SHT	MOISTURE CONTENT (\$)	SATURATION (S) VOID RATIO		MAXI DRY DE		OPTIMUM BOISTURE (\$)	SPECIFIC GRAVITY OF SOLIDS	TREAXIAL (4)	UNCONFINED COMPRESSION	DIRECT SHEAR	CONSOL I DAT I ON	CNEBICAL	=
1		(pcf)	$(kg/n^3)$	¥ 5	YS	22	(pcf)	(kg/m <sup>3</sup> )	3 <b>=</b>	2 50	11	33	9 12	3	15	<b>5</b>
	SP-SM			8.4												
	GW	122.3	1959	11.0		0.38						L				
	SM	115.9	1857	12.2	72.8	0.45						<u> </u>				
	SM	117.4	1881	12.0	74.8	0.44										
	GP-GC	117.2	1878	14.4	88.8	0.44										
-	GP-GC												<b></b>			<b></b>
-	SM	113.2	1813	10.5	58.3	0.49						<b> </b>			•	
-	GM	124.4	1993	9.5		0.35	<del></del>					<b> </b>				
	SW-SM	114.1	1828	11.4	64.7	0.48			<b> </b> -				<b> </b> -		<del>                                     </del>	<b></b>
P	SM				<b>}</b>		127.1	2036	-	} <u>-</u>						
	317				<del> </del>	<b></b> -	14/.1	2036	8.9			<del> </del>				
	SM		<b></b>			1			<b></b>			<del> </del>	-			
		<del></del>			<b></b>	<b> </b>		<del></del>				<del>                                     </del>				
4	ML						84.6	1355	33.0			<del> </del>				•
	SP											1	<b></b>			
5	ML						<u> </u>					1				1
16	MH											1				
rate)																
11	CT						109.3	1751	17.5							
	SP-SM											I				
	SP					<b>.</b>										
					L							<b></b>				
	GM				L							ļ				
	GP-GM		<b> </b>		ļ				<b> </b>		L		ļ	ļ		
			<b>}</b> -		<b> </b>	<b> </b>	122 6	2024	\ <u>-</u>			<b>├</b> ──	<b></b>			<b>├</b> ——
5	SC-SM				<b></b>	<b> </b>	127.0	2034	9.0			<b>├</b> ──	<b> </b>			-
18					<del></del>		124 0	1986	11.5		<u> </u>	<del> </del>				<del>                                     </del>
**	SC				<b></b>		124.0	1300	11.3			<del> </del> -				•
	SW-SM				<del> </del>		\- <del></del>	<del></del> -	<b> </b>			<del>                                     </del>				
	GC				<del>                                     </del>		<del></del>	<del></del> -	<u> </u>			<del>                                     </del>				$\vdash \dashv$
	SM				<u> </u>											
	CL															
MP	SP															
	SM															
	SW-SM															
	SM			ļ	ļ	<b></b>	ļ	<u> </u>				<b></b>	L			
	L	L	L	<u> </u>	<u> </u>	نـــــا				لـــــــــــــــــــــــــــــــــــــ	Ц				L	

SUMMARY OF LABORATORY TEST RESULTS VERIFICATION SITE REVEILLE-RAILROAD COP. NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

140LE 9-1 4-07-0

VORO NATIONAL INC

AFY-01

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PERCENT FINER BY WEIGHT

#### NOTES:

(a) Sample types

(c) USCS - Unified Soil Classification System

SS - Standard split spoon

P - Pitcher

- Fugro Drive

(d) \* Indicates that test has been performed and results are included in this report

B.b - Buik

(b) NP - Not Plastic

										11	I-SITU			C	OMPACTE	)		9	
<b>20</b> S	IEVE N		PARY SIZE T OR C	(MM)		TERBE HITS (		USCS (c)	DRY (		MOISTURE CONTENT (\$)	SATURATION (S)	_=	MAX! DRY DE		OPT I MUNI Moisture (\$)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (d)	UNCORF 18ED
40	100	200	.005	.001	LL	PL	PL	(5)	(pcf)	(kg/a <sup>3</sup> )	200 C	San )	WOID RATIO	(pef)	(kg/m <sup>3</sup> )	200	232	TRI	3
26	20	16			29	18	11	GC						128.6	2060	8.6			
,	45																		
38	41	33			22	15	7_	SC~SM		<del> </del> -									
10	28	21						SC											
30 37	14	10		ļ :		<b></b>		CM CM		ļ	<b></b>								
117	9	7			} ·			SW-SM SP-SM		<del> </del> -	<b>}</b> ——-	ļ	<b></b>						-
32	16	10		<b></b> -	}	<b> </b>		SW-SM		<b> </b>	ļ		<b> </b>					ļ	
40	23	16						SM											
	-					<b>.</b>					ļ		ļ						
73	56	41			}			SM		ļ ——									
<b>5</b> 5	37	29						SM											
27	12		<b></b>	ļ	<b> </b>	ļ		SP-SM		ļ	<b> </b>	ļ	<b>.</b>				·		-
-	44	7		<b> </b>	<b>!</b>	<del> </del>		SF-SM				<del> </del> -	<del> </del> -	l		<b></b>		<del></del>	1
50	29	23			30	19	11	sc						120,9	1937	11.4			
57	34	27			20	16	4	SC-SM		<del> </del>	<del> </del>	}	<del> </del>	131,1	2100	6.5	}		}
															_====				
58	28	19				ļ		SM											
66	42	30		<del> </del> -	}			SM		<del> </del>	<del> </del>	<del> </del>	<del> </del>			<b> </b>		<b></b> -	1-1
17	5	3						GP											
90	60		ļ	<b> </b>	24	19	-	CL-ML		<del> </del>	<b> </b>	<b>}</b>	<b> </b>	112 6	1010	15 0	2.55		H
80	69	62	<b></b>	<del> </del>	1-4	13.	5	CL-ML		<del> </del>	<del> </del>	<u> </u>	<del> </del>	113.5	1818	15.0	2.56	<u> </u>	H
45	30	22			20	17	3	SM						129.0	2066	9.0			口
52	29	18			<del> </del>		NP	SM		<del> </del>		<del> </del>	<del>  .</del>	112.2	1797	15.5		<b></b> -	H
																13.3			口
68	32	14	ļ					SM		<b></b> _									$\Box$
18	9	6	<b></b>	<del> </del>		<del> </del>		SW-SM	<del> </del> -	<del> </del>	<del> </del>	<b>├</b>		<u> </u>					H
					1_			J., 511											
70	46	26	<b></b>		1			SM		<b> </b>			1						$\Box$
88	65	50	ļ.——		25	20	5	SC-SM		<del> </del>	<del> </del>	<del> </del>		<del>}</del>	<b></b>	ļ			H
																			口
62	44	35			<u> </u>			SC		<u></u>									口

SUMMART REVE WX S11 DEPARTMENT

		11	1-SITU			C	OMPACTE			3	2 5		8		
USCS (c)	DRY (	INIT	II STURE INTENT (S)	SATURATION (S)	YOID RATIO	MAXI DRY DE	MUM MSITY	OPTIBUE Boisture (\$)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (6)	UNCONFINED CONPRESSION	DIRECT SHEAR	CONSOL I DATION	CHEBICAL	<b>183</b>
	(pcf)	(hg/m³)	<b>3</b> 3	S	N N	(pc1)	(kg/m <sup>3</sup> )		2 9 0	1	22	0 %	8	5	
GC	ļ	<b></b>	<b> </b>			128.6	2060	8.6							•
SC-SM	<del></del>	<del> </del>		-											
SC		<b></b>			<u> </u>				<b></b>		<b></b> -				
SW-SM SP-SM															
SW-SM															
SM															
SM															
SM			1												
SP-SM	1		1												
SC						120.9	1937	11.4							•
SC-SM						131.1	2100	6.5							•
SM				ļ									<b></b>		
SM	<b></b>	<del> </del> -	<del> </del>	<del> </del>	<del> </del>	<del></del>	<del></del>	<b></b>			<del> </del>				
GP					_										
CL-ML	ļ		ļ			113.5	1818	15.0	2.56						•
SM			1	ļ		129.0	2066	9.0							•
SM				-	·	112.2	1797	15.5							•
SM															
SW-SM															
SM	-				-										
SC-SM		1-	<del> </del>		-	<del> </del>									
8C															

SUMMARY OF LABORATORY TEST RESULTS VERIFICATION SITE REVEILLE-RAILROAD COP, NEVADA

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO

140LE 9-1 3 OF 8

VERO NATIONAL INC.

	b-2	2.2-2.5	0.67-0.76	1 1 1		I
RR-F-3	b-1	0.5-0.8	0.15-0.24			
	<b>B-</b> 2	0.5-1.6	0.15-0.49			I
RR-F-4	b-1	0.7-1.0	0.21-0.30			
	b-2	1.7-2.2	0.52-0.67			
					I	
RR-F-5	b-1	1.0-1.4	0.30-0.43			100
	b-2	2.0-2.3	0.61-0.70			100
			I			
RR-F-6	b-1	1.5-1.8	0.46-0.55			100
						I
RR-F-7	b-1	0.1-0.5	0.03-0.15			
	b-2	0.7-0.8	0.21-0.24		1	
	b-3	1.8-2.2	0.55-0.67			
RR-F-8	b-1	1.0-1.3	0.30-0.40			100
	b-2	2.0-2.3	0.61-0.70			100
RR-F-9	b-1	1.0-1.3	0.30-0.40			
	b-2	2.0-2.3	0.61-0.70			
			Ī			
RR-F-10	b-1	1.0-1.3	0.30-0.40			
	b-2	2.0-2.3	0.61-0.70			100
RR-F-11	b-1	1.0-1.3	0.30-0.40			1
	b-2	2.0-2.3	0.61-0.70			
			<del> </del>			<b>†</b>

BRT											11	-SITU			C	OMPACTE			3
		IEVE N			(88)		TERBE HITS (		USCS	DRY		BOISTURE CONTENT (\$)	SATURATION (S)		MAX	MUM	OPTIMUS BOISTURE (S)	SPECIFIC GRAVITY OF SOLIDS	TRIALIAL (d)
SAI	10			T OR C					(c)	WEI	BMT			51 51 51 51 51	DRY DE	MZITY	ERE		3
10	40	100	200	.005	.001	L	PL	=		(pef)	(kg/m <sup>3</sup> )	3 2	3	22	(pel)	(10/0 <sup>3</sup> )	2 <b>m</b>	222	=
83	51	25	18						SM										
86	53	26	20						SM						Ì	1			
97	85	68	63			53	32	21	MH			33.0							
91	75	58	53			46	29	15	MI,	ļ	<b>!</b>	ļ		<b> </b>	103.8	1663	21.0	ļ	
81		30					1	20			<b>}</b> -	ļ	ļ	<b>}</b>	ļ	<b>}</b>	ļ	ļ	_
80	54 52	38 32	30 25			38 37	18 21	20 16	SC SC	<del></del>	<b></b>		}	<del> </del> -	<del> </del>	<del> </del> -	<b></b> -	<b> </b>	<b> </b> -
80	- 32	32	25			3,	<del></del>	10	30		}	<b></b>			<b>}</b>	<del> </del>	<b></b>		-
52	38	24	19		<b> </b>		<del>                                     </del>	<b> </b>	GM		<del> </del>			<del> </del>	· · · · · · · · ·	<del>                                     </del>		<del>  </del>	<b>-</b>
18	4	2	1						GP		1		<b></b>	<b> </b>	<u> </u>	<del> </del>	l		<b>—</b>
37	12	2	1						GP										
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			85			27	22	5	CL-ML		ļ	ļ		<u> </u>	<b>}</b>	<b> </b>			
	45		72			25	19	6	CL-ML		<b> </b>	ļ	ļ	<b> </b>	<b></b>	<b></b>		<b> </b>	-
76	45	25	22			22	15	7	SC		<del></del>	<b></b>	<b> </b>		<del> </del>	<b></b>		ļ	<b> </b>
56	31	21	17				<del> </del>	<del> </del> -	SM		<del> </del>	<del> </del>	<del></del> -	├				<del> </del>	
59	45	35	29				<del> </del>	<del> </del> -	SM		<del>                                     </del>	<del> </del> -		<del>                                     </del>	<del> </del>	<del> </del>	<del> </del>		
~~											1			<b> </b>	1	1			H
87	71	50	39			37	21	16	SC					1	1	1			
67	46	24	14					NP	SM										
73	52	39	31				<b> </b>		SM		<b></b>			<b></b>	ļ	L			
42	19	11	7		<u> </u>	<b></b> -	<b>}</b>	_	SW-SM		<b> </b>	<b> </b>	<b>}</b>	<b> </b>	<u> </u>	<b>}</b> _		ļ	
94	68	50	35			ļ	<del> </del>		SM	<del></del>	<b></b>	ļ	<b> </b>	}		<del></del>	<del></del>	<b> </b>	
68	- 50	37	28				<del> </del>	-	SM			<del>}</del>	<b></b> -	<del> </del>		<del> </del>	<b></b>		H
-00	. 50	3/	20		<del> </del> -			<del> </del>	36	<del></del>	<del> </del>		<del> </del>	<del> </del>	<del> </del>	<del> </del>	<del>                                     </del>	<del></del>	1
100	97	83	79		<del>                                     </del>	28	22	6	ML		<b> </b>	<b> </b>	<b></b> -	<del>                                     </del>	<u> </u>	1			Н
100	95	89	82			45	30	15	ML										
]																			
				<b></b>	ļ	<b>.</b>	<b> </b>	<u> </u>			<b></b> _	<b></b>	<b> </b>	<b></b>	<u> </u>	<b>!</b>			
				<b>}</b> _	<b> </b> -	<b> </b>		<b> </b>	<b> </b>	<b> </b>	<b></b>	<b> </b> -	<b> </b>	<b>├</b> ─	<b> </b>	<b> </b>	<b> </b>	<b>  </b>	H
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USCS (c)	ORY WE !	unit Ght	ISTURE MTENT (S)	SATURATION (S)	VOIS RATIO	MAX! DRY DE	MUM MS I TY	OPTIMUM Boisture (\$)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (4)	UNCONFINED CORPRESSION	DIRECT SNEAR	CONSOLIBATION	CNEBICAL	<b>18</b> 5
	(psf)	(1g/n³)	3 3	2	25	(pef)	(kg/m³)	0 =	200		33	8	8	5	5
SM							Ĺ				L				
SM	<b>├</b>	<del> </del>			<b> </b>	ļ <del>-</del>	<b> </b>		·						
MH	<b> </b>	<del> </del>	33.0			<u> </u>	<b></b>				<b></b>				
MIL	<u> </u>	<del>                                     </del>	33.0		<b>-</b>	103.8	1663	21.0							
<b>S</b> C															
SC		L													
<b></b>	<b> </b>	<b>}</b> -	<b></b>		ļ	<b> </b>	<b> </b>								
GM GP	<del></del>	├	<b> </b>		<del> </del> -	ł	<b> </b> -		}{	<del></del>		}			
- GF	<b></b>	<del> </del>	<del>                                     </del>		<del>                                     </del>	<del> </del>	<del> </del> -	<b></b>	<b></b>	}	<del> </del>				
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sc	<b> </b>	╂		<b> </b>	<u> </u>	<b> </b>	<b> </b>		<b> </b>		<b></b>				
SM	<del> </del> -	<del> </del>	<del> </del>	<del>                                     </del>	├	<del> </del>	<del> </del>			<del></del>					
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SC															
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	<b>}</b>	<del> </del>	<b></b>	<b> </b>	<u> </u>	ļ	<b> </b>				ļ				
SM	<b></b>	<del> </del>	<b> </b>	<b>}</b>	├	<b> </b>	<b> </b>		<b> </b>		<b> </b>				
SW-SM	<del> </del>	<del> </del>	<del>                                     </del>	<del> </del>	}	<del></del>	<del> </del>		}	<del></del>	<del> </del>				
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SM	t	1			<u> </u>	<u> </u>	<b>!</b>								
ML															
ML	<b> </b>	<b></b> -	ļ	<b> </b>	<b> </b>	<b> </b>	<b></b>	ļ			<del> </del>				
	<b></b>	<del>├</del>	<del> </del>	<del> </del>	<del> </del>	<b>}</b> -	<u> </u>	ļ			<del> </del>				
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	<b>}</b>	<del> </del>	<b>.</b>		<del> </del>	<del>                                     </del>	<del> </del>	<b></b> -	<b> </b>						<u> </u>
J	I	<u> </u>	<u> </u>	L	<u></u>	<u> </u>	<u> </u>				<u> </u>				

								 		_		_	_		
PRESSURE	LH/e2	0	•	0	•	0	•								
25	111	0	-	-	•	0	0								
STRAIN	(\$/min)	900 .	.006	. 008	900	. 908	900 ·								
	2	848	1762	2700	723	1293	1958								
PAY I BUSH	ks (	18.0	38.0	58.4	15.1	27.0	40.9								
35 35 35	kN/n <sup>2</sup>	182	383	575	182	383	575								-
CONFINING PRESSURE (C3)	101	4.0	0.0	12.0	4.0	8.0	12.0								
	(\$)	5.1	8.2	11.2	11.4	19.7	12.6								
MSITY	14/83	1578	1602	1784	1583	1474	1527								
DAY DENSITY	pe 1	98.4	100.0	111.4	99.8	<b>9</b> 2.0	95.3								
3441	TEST	CO	93	93	23	63	03								
	TYPE	SIL	SH	SH	SH	SE	SH								_
INTERVAL	METERS	11.83-12.87	12.07-12.31	12.31-12.53	10.67-10.65	10.05-11.00	11.00-11.28								
SAMPLE	FEET	38.6-38.6	39.6-40.4	1-17-7-07	35.0-35.0	35.6-36.1	36.1-37.0								
SAHPLE		P-10	P-10	11-1	P-10	P-10	P-10								
•		18-8-2			R-1-3										

SUMMARY OF TRIAXIAL COMPRESSION TEST RESULTS
VERIFICATION SITE
REVEILLE—RAILROAD COP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

140LE 9-2

UGRO MATIONAL INC.

	_	_	_		_	_	 	_	 _	_	_	,	 _	 _	_	_	_	_	_	_	_	_	 _	_	_
	DIAMETER	2.1	2.4	2.0	1.1	1.2																			
DEGREE OF SATURATION	(\$)	42.8	91.4	53.0	83.7	93.2																			
CONTENT	(3)	15.3	35.4	11.1	34.5	30.00																			
DAY DENSITY	kg/83	1370	1521	1406	1270	1308																			
<b>D Y D</b>	2	65.5	77.5	87.8	79.1	81.7																			
UNCONFINED COMP. STRENGTH	kN /82	98	108	73	125	332																			
COMP. S	ks í	1.8	2.3	1.5	2.8	8.8																			
110\$	TVPE	SI	=	<b>=</b>	ML-MM	H.																			
NTERVAL	METERS	3.05-3.29	5.15-5.43	8.25-8.48	12.18-12.41	24.63-24.67																			
SAMPLE INTERVAL	FEET	10.0-10.6	18.9-17.8	20.5-21.2	40.0-40.7	86.1-11.6																			
1 7 E		P-5	P-6	1-1	P-12	P-18																			
9	HO.	RR-8-3	RR-8-4																						

SUMMARY OF UNCONFINED COMPRESSION TEST RESULTS VERIFICATION SITE REVEILLE-RAILROAD COP. NEVADA

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO TABLE 9-3

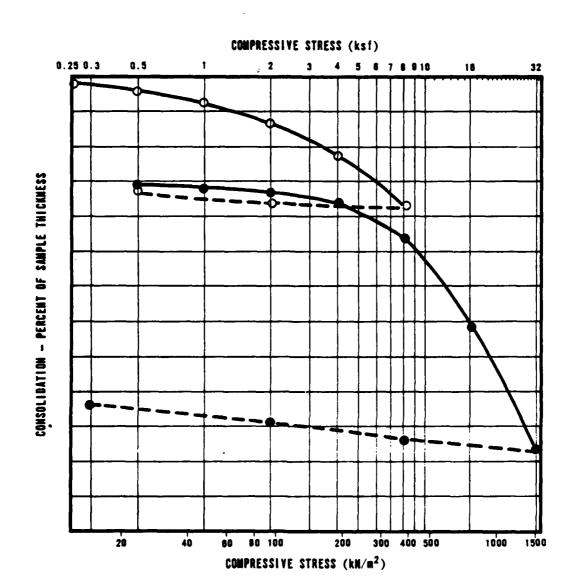
BORING	SAMPLE	SAMPLE	NTERVAL	SOIL	NORMAL	STRESS	MAX! SHEAR !	MUM TRENGTH
NO.	NO.	FEET	METERS	TYPE	ksf	kM/m <sup>2</sup>	kef	kM/m <sup>2</sup>
RR-B-1	D-10	40.1-40.6	12.22-12.37	SM-SM	4.0	192	5.4	259
				SW-SM	8.0	383	10.4	498
				SW-SM	12.0	575	11.4	546
RR-B-3	P-14	71.4-72.3	21.76-22.04	SM	7.0	335	4.9	235
L			<u> </u>	SM	11.0	527	7.1	340
				SM.	15.0	718	9.2	440
L						L		
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<u> </u>						} 	<u> </u>	<u> </u>
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SUMMARY OF DIRECT SHEAR TEST RESULTS
VERIFICATION SITÉ
REVEILLE-RAILROAD CDP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

TABLE 9-4

VORO NATIONAL INC



SYMBOL	BORING NO.	SAMPLE NG.	SAMPLE	INTERVAL	SOIL	INI Dry D	TIAL ENSITY	INITIAL MOISTURE CONTENT		INITIAL DEGREE OF SATURATION
			FEET	METERS		pe1	kg/m <sup>3</sup>	(\$)	KATIO	(%)
0	RR-B-4	P-7	20.5-21.2	8.25-8.46	MH	83.8	1342	20.4	0 98	55.4

O AT FIELD MOISTURE

AFTER ADDITION OF WATER

\_\_\_\_ COMPRESSION

\_ \_ REBOUNG

.CONSOLIDATION TEST RESULTS
VERIFICATION SITE
REVEILLE-RAILROAD CDP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

9-1

UGRO NATIONAL INC.

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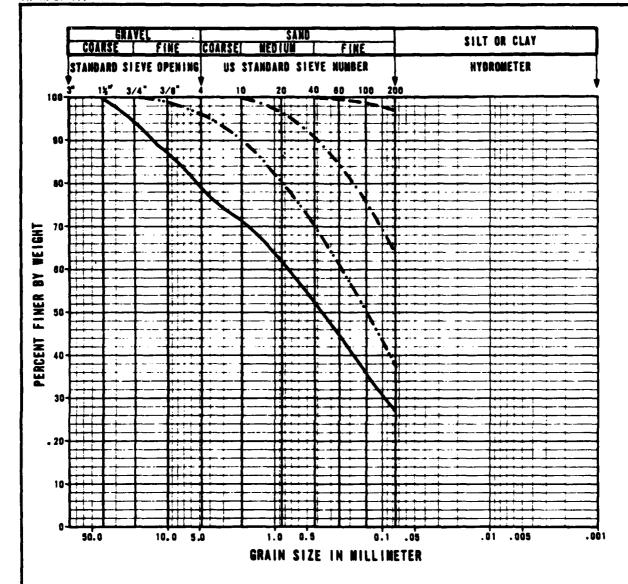
			4				7	WATER SOLUBLE	E	CALCIUM
ACTIVITY	SAMPLE		SAMPLE INTERFAL	SOIL	줊	300 I UM	CHLORIDE	SULPHATE	CALCIUM	CARBONATE
		FEET	METERS			ng/kg	ng/kg	ng/kg	mg/kg	mg/kg
RR-8-1	0-4	10.0-10.4	3.05-3.17	SM	7.8	348	180	153	07	178
	0-8	30.2-30.7	9.20-9.36	SW	7.5	113	43	37	38	198
RR-8-2	P-10	38.0-40.4	11.58-12.31	NS	7.0	28	99	34	89	264
RR-8-3	P-14	70.5-73.3	21.49-22.34	SM	7.1	22	97	88	35	202
RR-B-4	P-7	20.3-21.2	6.19-6.46	=	1.2	175	231	8540	2790	8180
	P-15	70.0-72.8	21.34-22.19	H	1.4	001	25	55	79	245
RR-8-5	0-10	35.0-35.5	10.87-10.82	SP-SM	7.3	18	54	48	14	121
	0-11	40.0-40.4	12.18-12.31	SH	7.3	23	38	1>	16	280
RR-B-6	0-21	119.2-119.9	36.33-36.55	SH	7.1	08	091	35	11	801
RR-T-5	8-1	0.5-2.0	0.15-0.61	<b>6M</b>	7.1	101	77	18	107	274
RR-T-8	p-2	9.0-10.0	2.74-3.05	ec	7.1	55	31	23	65	269
RR-P-1	p-2	2.5-3.5	0.76-1.07	เ	7.8	1200	576	531	47	187

SUMMARY OF CHEMICAL TEST RESULTS
VERIFICATION SITE
REVEILLE-RAILROAD CDP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

148LE 9-5

TUBRO NATIONAL INC.



SYMBOL	COMPOSITE SAMPLE	ACTIVITY	SAMPLE	INTERVAL	SOIL
41800	NUMBER	NUMBER	FEET	METERS	TYPE
	A	RR-T-1	0.5-2.0	0.15-0.61	SM
	В	RR-T-3	0.5-1.5	0.15-0.46	ML
	C	RR-T-4	0.25-1.5	0.08-0.46	CL
	D	RR-T-8	0.5-2.0	0.15-0.81	SC-SM

GRAIN SIZE CURVES, CBR TESTS
VERIFICATION SITE
REVEILLE-RAILROAD CDP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

9-2

**VERO NATIONAL INC** 

SYMBOL	COMPOSITE SAMPLE	ACTIVITY	SAMPLE	INTERVAL	SOIL
o: HDOL	NUMBER	NUMBER	FEET	METERS	TYPE
	E	RR-T-7	0.5-2.0	0.15-0.61	32
	F	RR-P-9	0.5-1.5	0.15-0.48	- 60
	8	RR-P-24	0.5-2.0	0.15-0.81	SC
	н	RR-P-29	0.5-2.0	0.15-0.61	SC-SN

GRAIN SIZE CURVES, CBR TESTS
VERIFICATION SITE
REVEILLE-RAILROAD CDP, NEVADA

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAWSO

9-2

<u>uoro national inc.</u>

SYMBOL	COMPOSITE SAMPLE	ACTIVITY	SAMPLE	INTERVAL	SOIL
	NUMBER	NUMBER	FEET	METERS	TYPE
	1	RR-CS-10	0.25-2.0	0.08-0.61	CL-ML
	1	RR-CS-11	0.5-2.0	0.15-0.61	M2
	ĸ	RR-CS-15	0.5-2.0	0.15-0.61	- SM
	ı	RR-F-3	0.5-1.5	0.15-0.48	ML

GRAIN SIZE CURVES, CBR TESTS
VERIFICATION SITE
REVEILLE-RAILROAD CDP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

9-2

**VORO NATIONAL INC** 

COMPOSITE Sample	SOIL	PERCENT PASS ING	ATTE	ATTERBERG LIMITS	SPECIFIC	KAXIN ORY DEN:	MAXIMUM ORY DENSITY	OPT I MUN MOISTURE		COMPACTED ORY DENSITY	COMPACTED	PERCENT OF MAXIMUM	CBR
NUMBER	4	<b>≠200</b>	11	Ξ	GRAVIIY	pc1	kg/a3	(\$)	pcf	16/83	(\$)	DRY DENSITY	(%)
									126.4	2025	9.7	98.4	43
									124.8	1999	9.4	88.2	11
~	3	28		<b>=</b>		127.1	2036	<b>8</b> .	117.2	1877	8.4	82.2	01
									83.0	1330	33.2	1 88	77
									78.2	1253	33.4	₽3.4	11
<b>a</b>	=	6	\$	=		8.8	1355	33.0					
									104.2	6991	6.81	95.4	9
									95.7	1533	0.71	9.78	2
u	ಶ	63	30	=		109.3	1751	17.5	87.8	1406	17.0	80.3	1
									124.2	1989	9.6	87.8	67
									117.5	1882	9.8	92.6	21
•	SC-SH	37	22	S		127.0	2034	9.0	106.6	1740		85.5	3
												•	

CALIFORNIA BEARING RATIO (CBR) TEST RESULTS
VERIFICATION SITE
REVEILLE-RAILROAD CDP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

TABLE 9-6

VERO NATIONAL INC

AFV-1

SITE SOIL	PERCENT PASS ING	ATTEI	ATTERBERG Limits	SPECIFIC	DRY B	MAXIMUM DRY BENSITY	OPT I MUM MOISTURE	COMPACTED DRY DENSITY	CTED Ensity	COMPACTED Moisture	PERCENT OF MAXINUM	CBR
וועב	#200	11	14	GKAV117	pef	kg/a3	(\$)	pcf	k 8/8 3	(\$)	DRY DENSITY	(\$)
									1685	10.3	8 ' 76	18
								116.9	1873	11.3	84.3	11
SC	22	42	=		124.8	1988	11.5	103.8	1663	10.8	83.7	2
								127.6	2044	1.1	89.2	86
						_		121.8	1848	1.4	94.5	28
<b>3</b>	9	29	=		128.6	2060	9.8	116.1	1960	6.7	80.3	7
								120.9	1937	6.7	100.0	58
								112.6	1804	7.8	93.1	*
2	23	30	=		120.9	1837	1.5.4	105.2	1665	8.0	0.78	7
					•							
								126.3	2023	7.6	Se. 3	78
								119.5	1814	7.8	2 . 18	33
SC-51	12	20	*		131.1	2100	6.5	110.7	1773	7.8	94.4	9
-												

CALIFORNIA BEARING RATIO (CBR) TEST RESULTS VERIFICATION SITE REVEILLE-RAILROAD CDP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

JORO NATIONAL INC

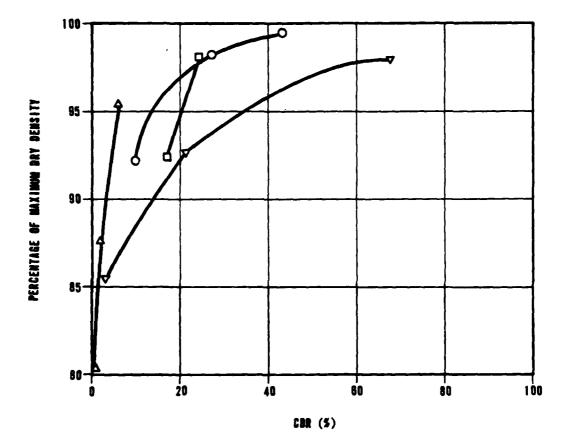
COMPOSITE SAMPLE	102	22	ATTEI	ATTERBERG Limits	SPECIFIC		MAXINUM ORY DENSITY	OPT INUM MOISTURE	1 1	COMPACTED DRY DENSITY	COMPACTED	PERCENT OF MAXIMUM	<b>85</b>
MARKE	7		11	H	BKAVIIT	pc f	kg/m3	(\$)	pcf	kg/83	(\$)	DRY DENSITY	(2)
									111.8	18/1	14.8	98.5	8
									105.6	7691	14.8	83.0	2
-	1 <b>II-1</b> 3	82	24	10	2.58	113.5	1818	15.0	97.6	1583	14.9	0.88	2
									128.2	2054	9.2	<b>7</b> 88	63
									123.2	1973	8.8	<b>3</b> · <b>38</b>	26
-	8	22	20	~		129.0	2086	9.0					
									105.0	7891	15.3	83.6	31
									100.7	1813	18.0	8.88	19
**	3	=		=		112.2	11797	15.5					
•													
						[ L_			104.8	1680	20.2	1.101	1
-									97.5	1562	20.2	83.8	•
	<b>=</b>	53	46	5		103.8	1663	21.0	90.6	1451	19.8	87.2	2

CALIFORNIA BEARING RATIO (CBR) TEST RESULTS
VERIFICATION SITE
REVEILLE-RAILROAD CDP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

9-6

<u>ubro national inc.</u>



SYMBOL	COMPOSITE SAMPLE NUMBER	SOIL TYPE
0	A	SM
U	8	ML
Δ	C	CL
₹	8	SC-SM

CALIFORNIA BEARING RATIO (CBR) CURVES
VERIFICATION SITE
REVEILLE-RAILROAD CDP, NEVADA

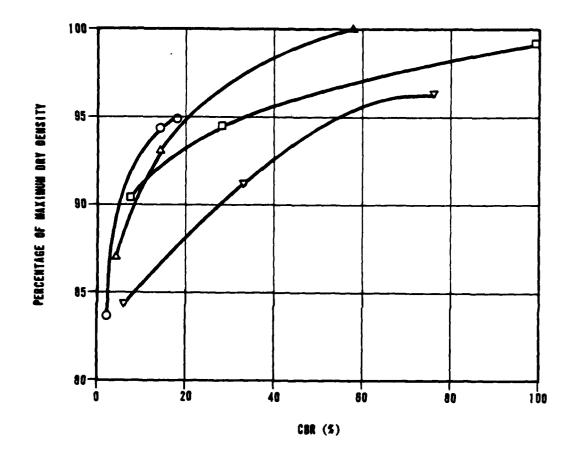
MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAWSO

9-3

UGRO NATIONAL INC.

AFV-1A

2 JUL 78



COMPOSITE SAMPLE NUMBER

E

F

H

SYMBOL

0

ā

Δ

A

SOIL

SC

GC

SC

SC-SM

CALIFORNIA BEARING RATIO (CBR) CURVES
VERIFICATION SITE
REVEILLE-RAILROAD CDP, NEVADA

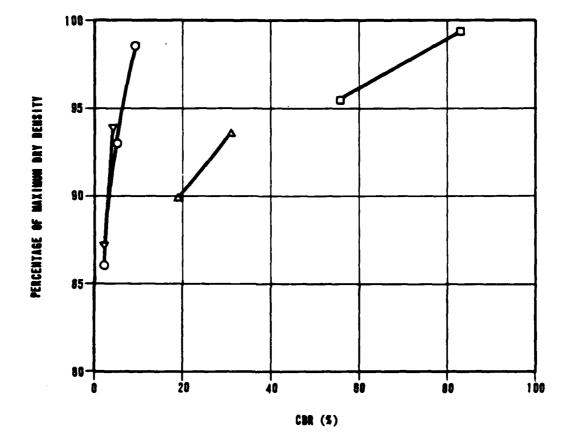
MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

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ugro national inc.

AFY-14

2 JUL 78



SYMBOL	COMPOSITE SAMPLE MUMBER	SOIL
0	1	CL-ML
0	J	SM
Δ	K	M2
♥	L	ML

CALIFORNIA BEARING RATIO (CBR) CURVES
VERIFICATION SITE
REVEILLE—RAILROAD COP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

9-3

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SECTION 10.0 FIELD COR TEST RESULTS

## EXPLANATIONS OF FIELD CBR TEST RESULTS

The results of field CBR tests and related field density, moisture content, and laboratory soil classification tests are presented on the summary table included in this section. The following explanations will aid in reviewing the data included in the table.

- A. Definition of California Bearing Ratio (CBR) California Bearing Ratio (CBR) is the ratio (in percent) of the resistance to penetration developed by a soil to that developed by a specimen of standard crushed-rock base material and is the basis for many empirical road design methods used in this country.
- B. Activity Number Field CBR tests are identified as follows: BS-F-1
  - BS abbreviation for the site (e.g., BS-Big Smoky)
  - F abbreviation for field CBR test
  - l number of activity
- C. Ground Surface Elevation Indicated elevations (in feet and meters) are estimated from topographic maps of the study area within an accuracy of half the contour interval.
- D. Surficial Geologic Units Indicates the surficial geologic unit in which the activity is located.
- E. USCS The symbols used are from the Unified Soil Classification System; see Table 6-1 of Section 6.0, "Boring Logs", for details of USCS.

- F. Grain-Size Distribution and Plasticity These are from results of laboratory tests. See Section 6.0, "Boring Logs", for explanations.
- G. In-Situ Dry Unit Weight Indicated dry unit weights are from field density tests conducted at each CBR test site in accordance with ASTM D 1556-64, "Test for Density of Soil in Place by the Sand-Cone Method".
- H. Moisture Content Moisture contents as determined in the field by the "Speedy Moisture Tester".
- I. Estimated Percent of Maximum Dry Density Indicates the ratio (as a percentage) of in-situ dry unit weight to the maximum dry density obtained in the laboratory from ASTM D 1557-70, "Moisture Density Relations of Soils Using 10-pound (4.5 kg) Hammer and 18-inch (457 mm) Drop".
- J. Average Field CBR Average of three field CBR tests performed at each level.
- K. Remarks These include comments about the in-situ soil conditions which may have had significant influence on the CBR test (cementation, cobbles, gravel, and/or unusual moisture content). See Section 6.0, "Boring Logs", for explanation of terms used to describe cementation and cobbles. Indurated indicates soil or rock hardened by heat, pressure and/or cementation. Disseminated caliche indicates a scattered distribution of calcium carbonate in the soil profile.

ACTIVITY		OUND FACE	SURFICIAL	DE	PTH		01	STI	I B	SIZ	ON	DRY	SITU	MOISTURE	ESTIMATED PERCENT OF	AVI
NUMBER	ELEV	ATION	GEOLOGIC Unit			uscs	ANE	P	LAS	TIC	ITY	WE	THAL	CONTENT (\$)	MAXIMUM Dry	FIE
RR-F-1	FEET 5480	METERS 1870		FEET 0.75	METERS 0.23	M2	GK	24	11	LL	PI	95.3	(kg/m <sup>3</sup> )	1.3	DENSITY	<del> `</del>
MK-Y-I	3400	10/0	A5y	2.2	0.23	SC-SM	-	77	23	20	4	114.3	1831	0.5	70 87	-
RR-F-2	5485	1672	A5y	1.0	0.30	SM2	5	77		1.0	-	108.6	1740	0.6	83	<b>-</b>
	0400	10.2		2.2	0.87	SM	_	75	_	<del>                                     </del>		115.0	1842	9.8	80	-
RR-F-3	5800	1707	A2	0.5	0.15	MH	ř		_	53	21	88.8	1387	33.0	83	<b> </b>
	1 3333	1707	7.6	1.5	0.48	ML	<u> </u>	42			15	80.2	1445	21.0	87	-
RR-F-4	5560	1695	A51	0.7	0.21	SC	_	81		<b>-</b>	20	94.7	1517	15. 2	75	
	t			1.7	0.52	SC				37		92.4	1480	15.0	73	<del>                                     </del>
RR-F-5	5000	1524	A5y	1.0	0.30	GM	42	39	18	1		114.3	1831	12.1	89	<u> </u>
	<b> </b>			2.0	0.81	GP.		48	1	1						
RR-F-8	4960	1512	A5y	1.7	0.52	SP (	52	47	1			108.7	1741	4.1	84	
				2.5	0.76	GP										
RR-F-7	49 30	1503	A40/A5y	0.1	0.03	CL-ML			85	27	5	84.0	1380	18.5	75	
				0.7	0.21	CL-ML			72	25	8	81.3	1302	9.5	72	
				1.8	0.55	\$C	14	84	22	22	7	98.8	1583	5.8	76	
RR-F-0	5050	1539	A5y	1.0	0.30	SM		54				99.2	1589	8.8	11	
L	<u> </u>			2.0	0.81	231		41				92.2	1477	12.3	12	
RR-F-9	5030	1533	A51	1.0	0.30	SC				37	16	79 0	1265	18.8	88	
L	ļ	<u> </u>		2.0	0.61	SM	22	84	14	L	NP	95.0	1522	9.0	74	
RR-F-10	4990	1521	A5y	1.0	0.30	SM	-	51		<u> </u>		102.8	1847	12.8	81	
		ļ		2.0	0.81	SM-SM	-	48	÷	_	L	105.0	1686	7.0	82	
RR-F-11	4960	1512	A5y	1.0	0.30	SM	2	-	35	<u> </u>		92.0	1474	11.1	12	
				2.0	0.81	SM	18	54		ļ		91.0	1458	11.3	12	
RR-F-12	4855	1480	A40	0.5	0.15	ML	0	21			8	78.5	1225	12.2	70	
l			l	1.5	0.48	ML	0	+	<del></del>	45	15	82.3	998	23.0	74	
RR-F-13	4930	1503	A40	2.5	0.78	SM	1	82	<u> 11</u>	$\vdash$	<u> </u>	100.3	1607	8.8	83	
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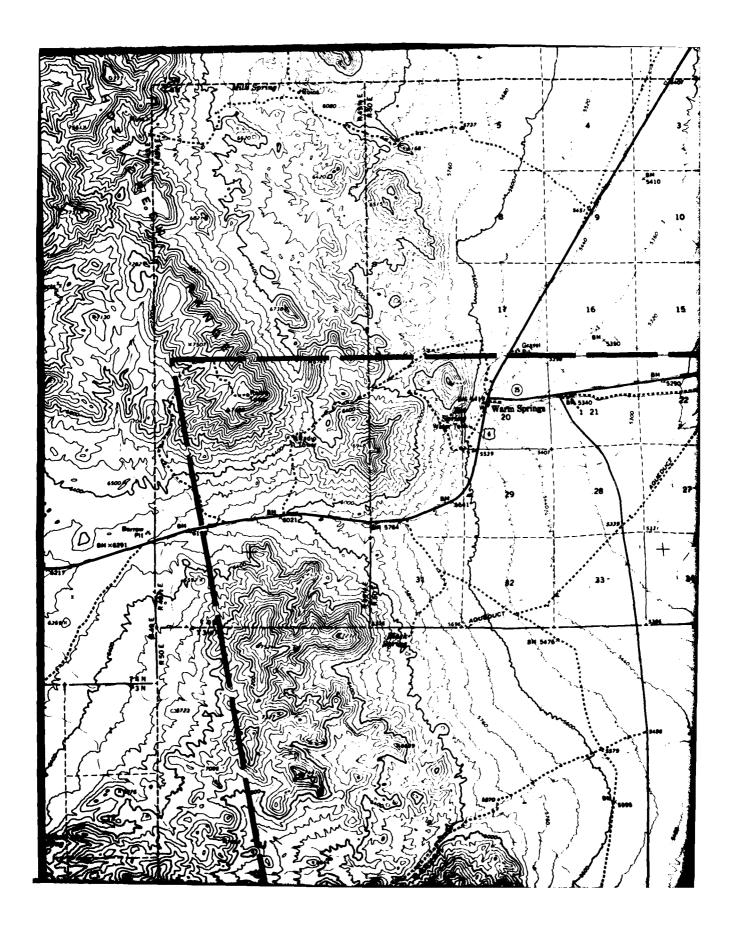
TED T OF	AVERAGE FIELD CBR (%)	REMARKS
	2	
	7	Stage I-II caliche, weak
	2	•
	4	
	2	
	1	Stage II caliche, soft to moderately hard, CBR soft ~ 4; CBR hard ~ 14
	2	
	2	
	5	
	11	Field density not obtained due to soil caving
	•	
		Field density not obtained due to soil caving
	14	Desicceted
	9	Desiccated
	22	Stage I caliche, slightly indurated
	1	
	1	
	3	Stage I caliche, variable cementation, weak
	2	Stage I Califolia, Valifable Comelication, weak
	4	
	3	
	5	
	9	
	7	Desiccated and fissured in situ
	21	Stage I-I caliche, slightly indurated

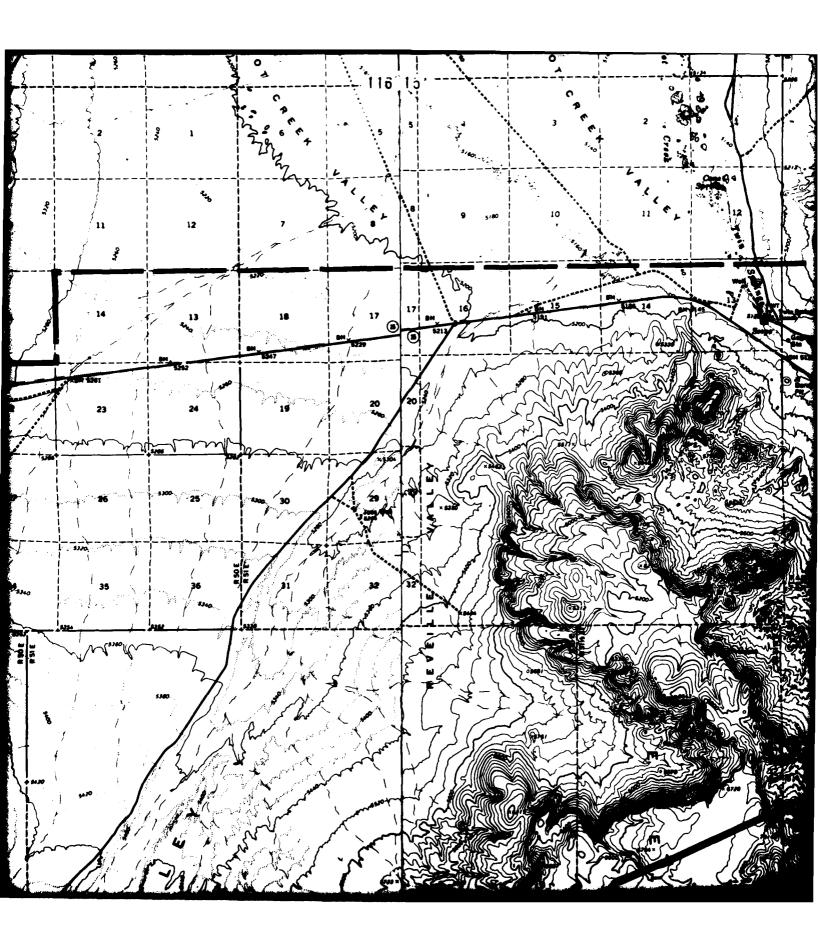
FIELD COR TEST RESULTS
YERIFICATION SITE
REVEILLE-RAILROAD COP, NEVADA

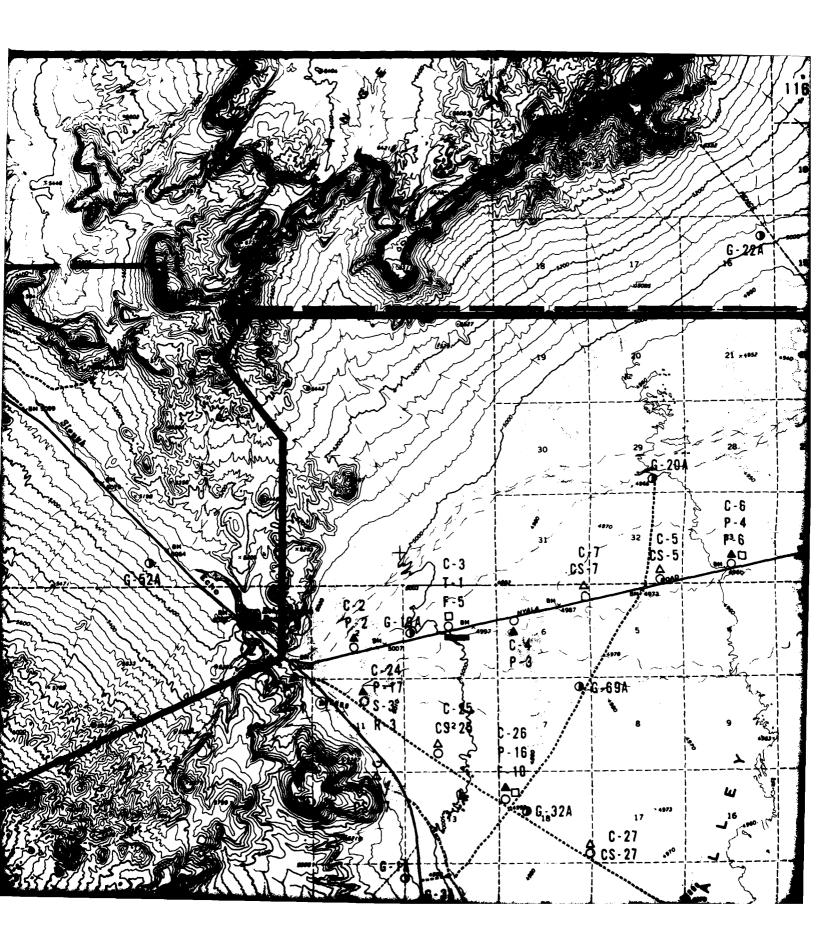
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DEPARTMENT OF THE AIR FORCE - SAUSO

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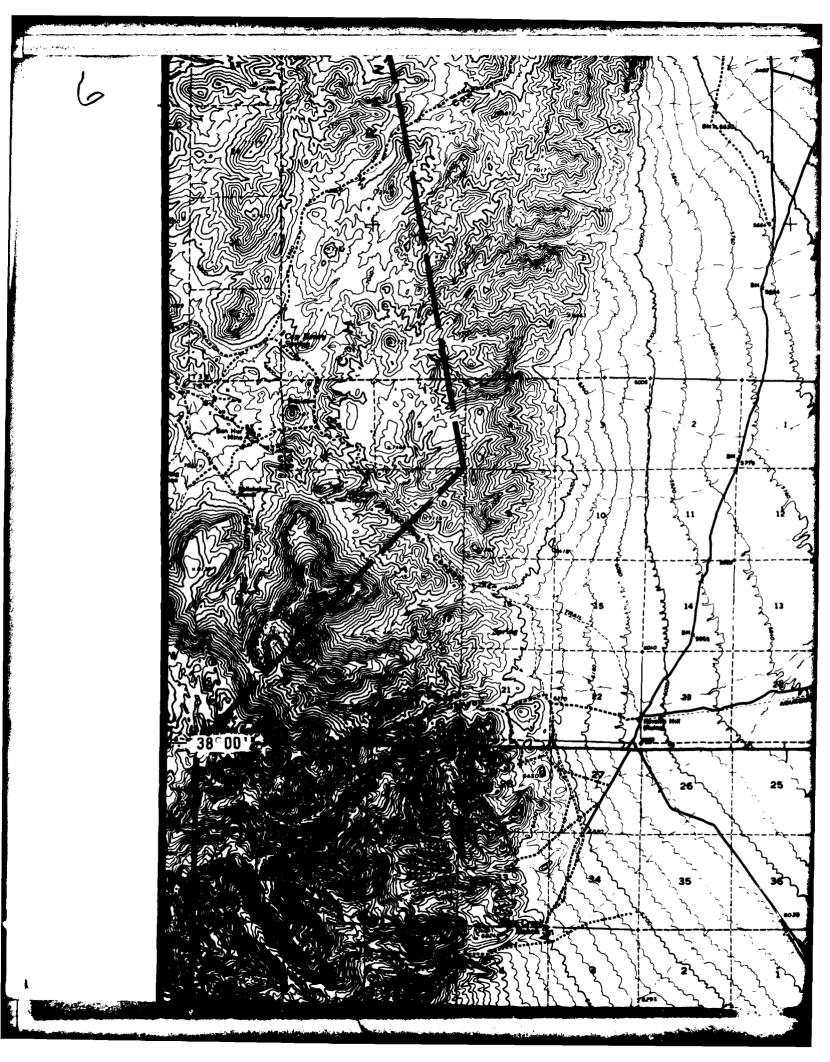


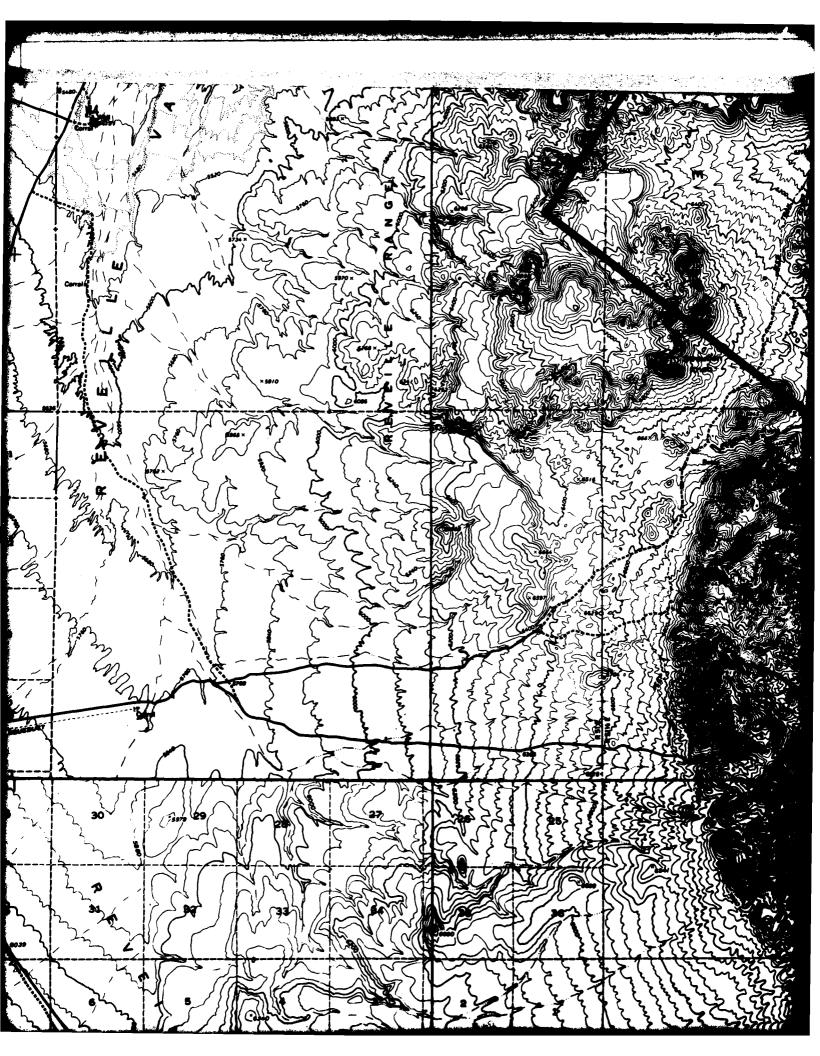


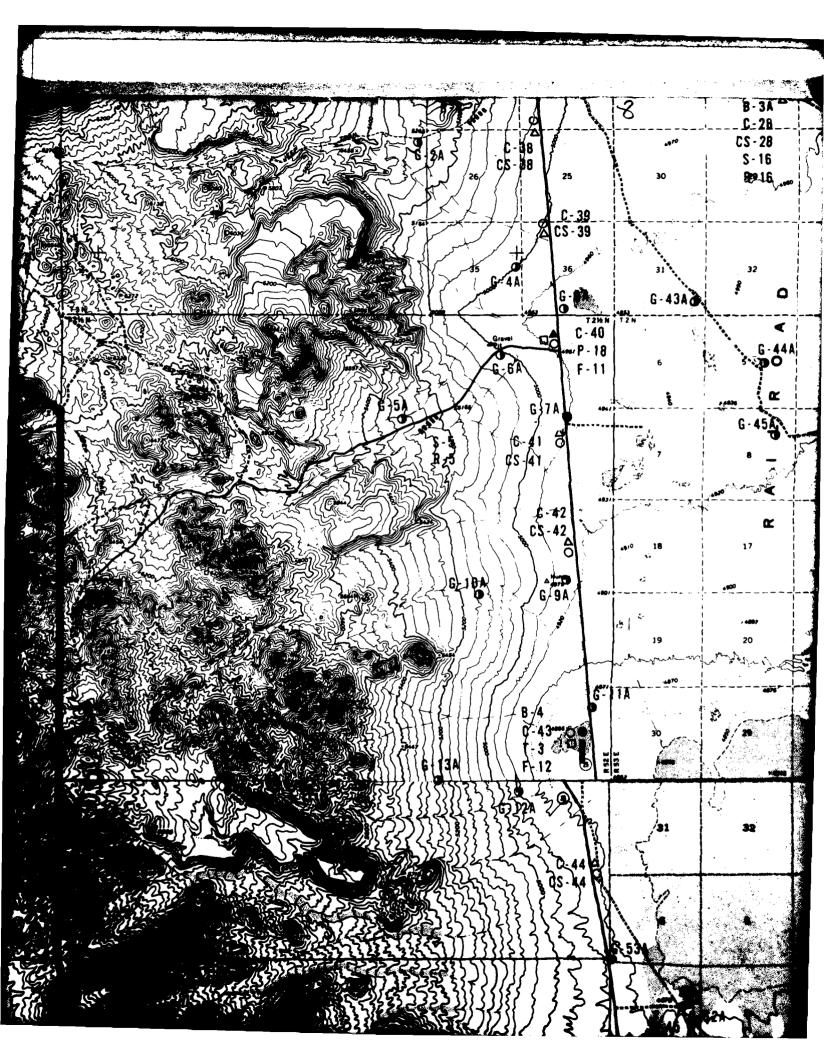


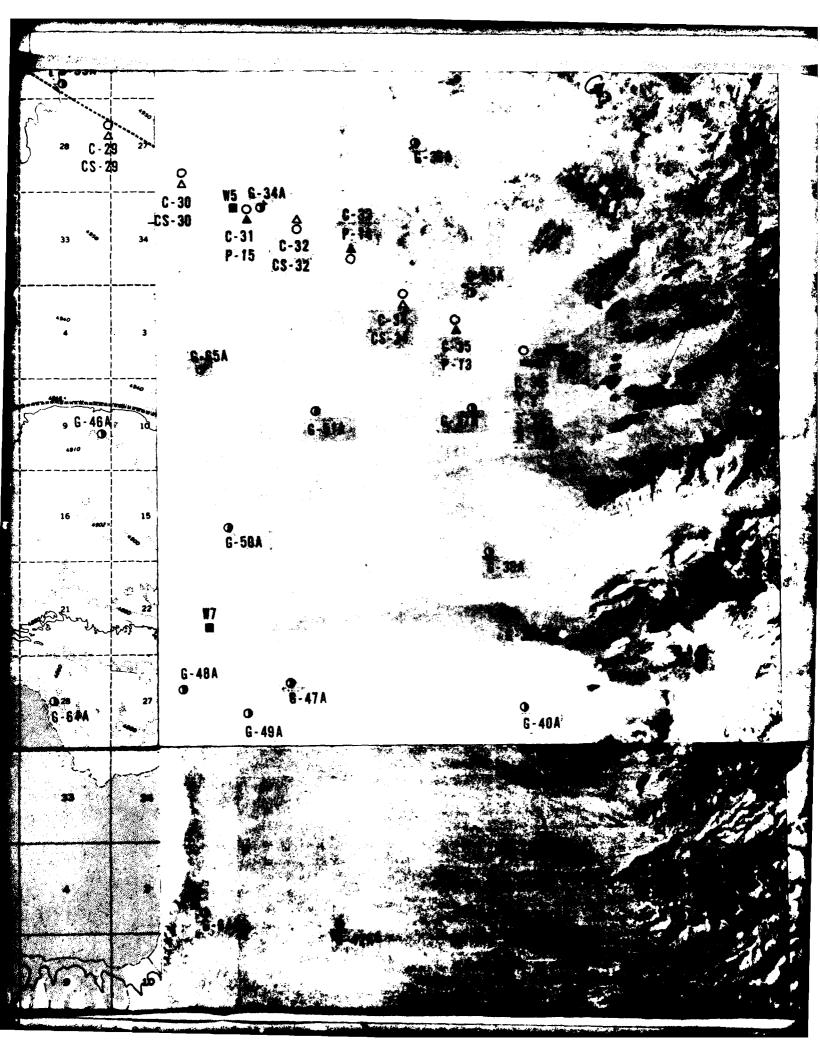




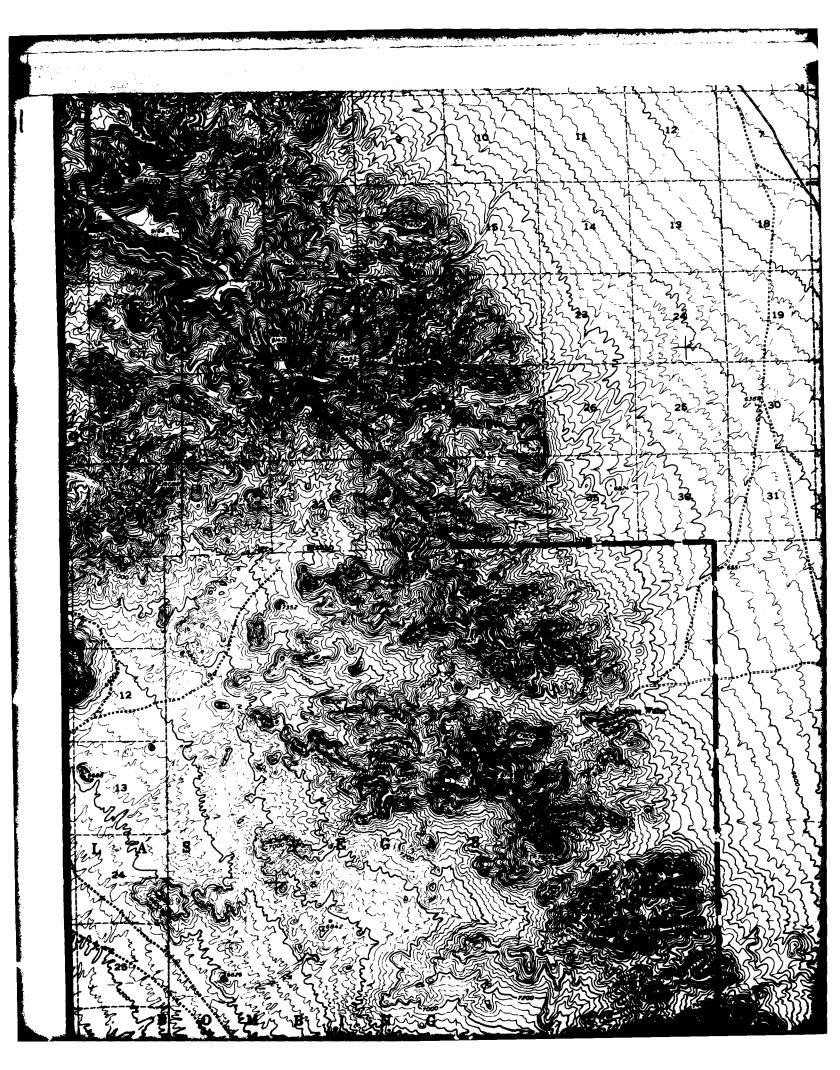


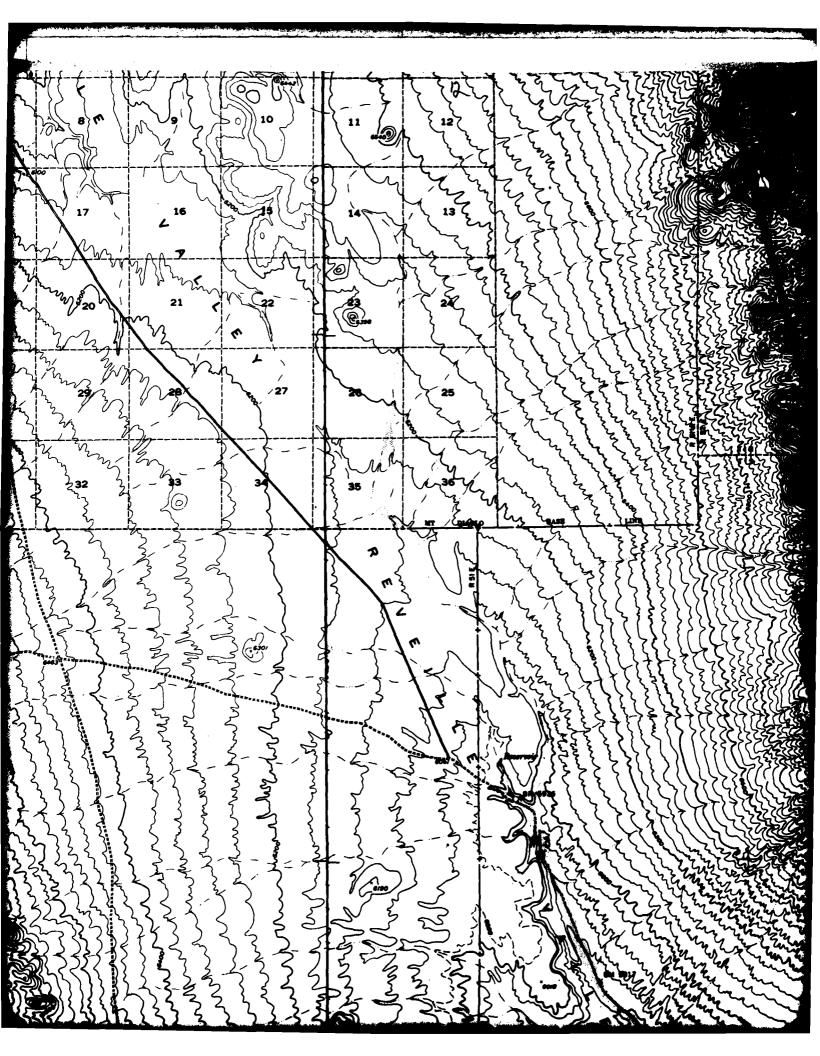


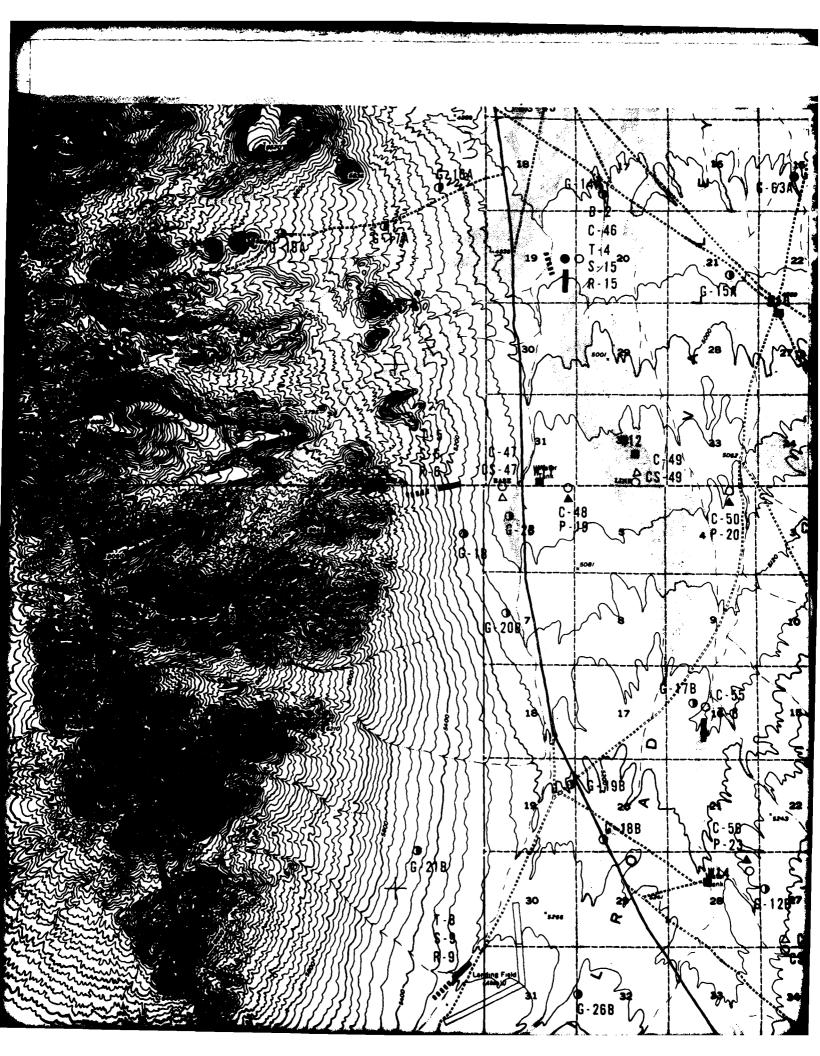


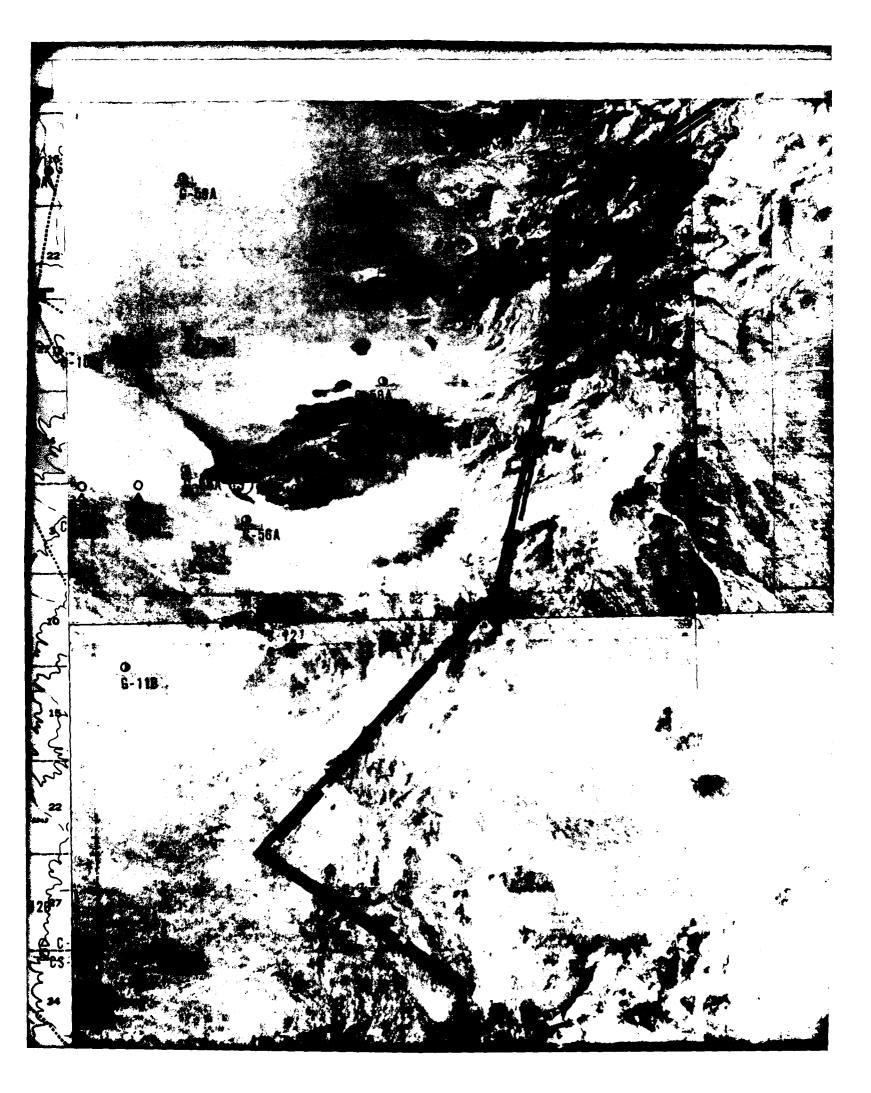


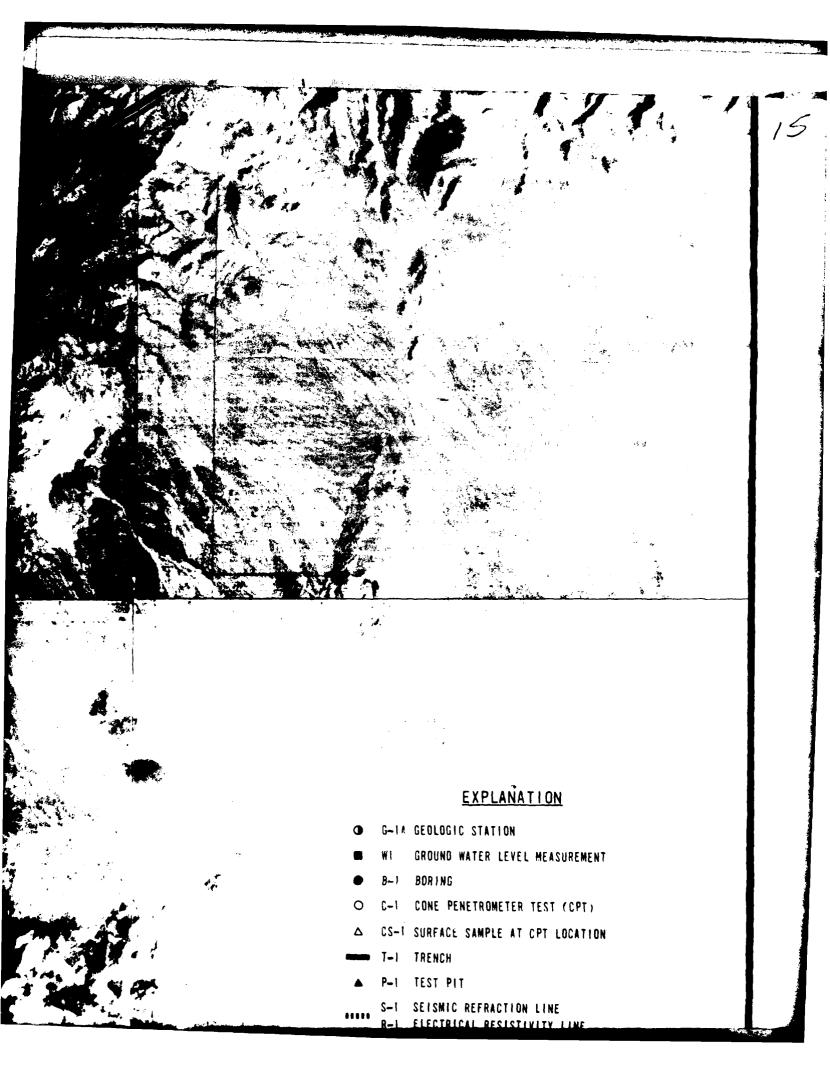


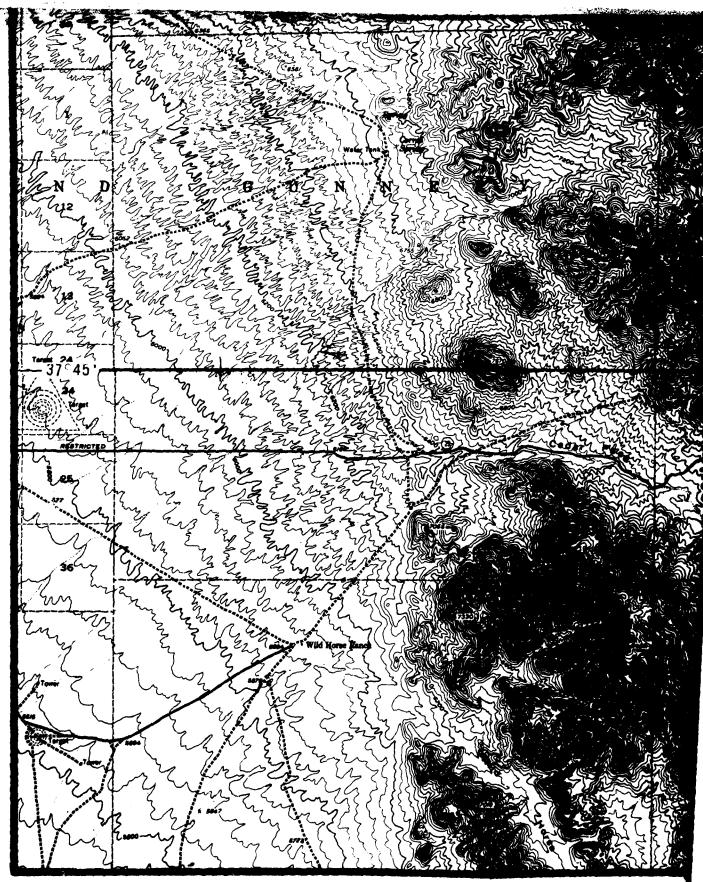






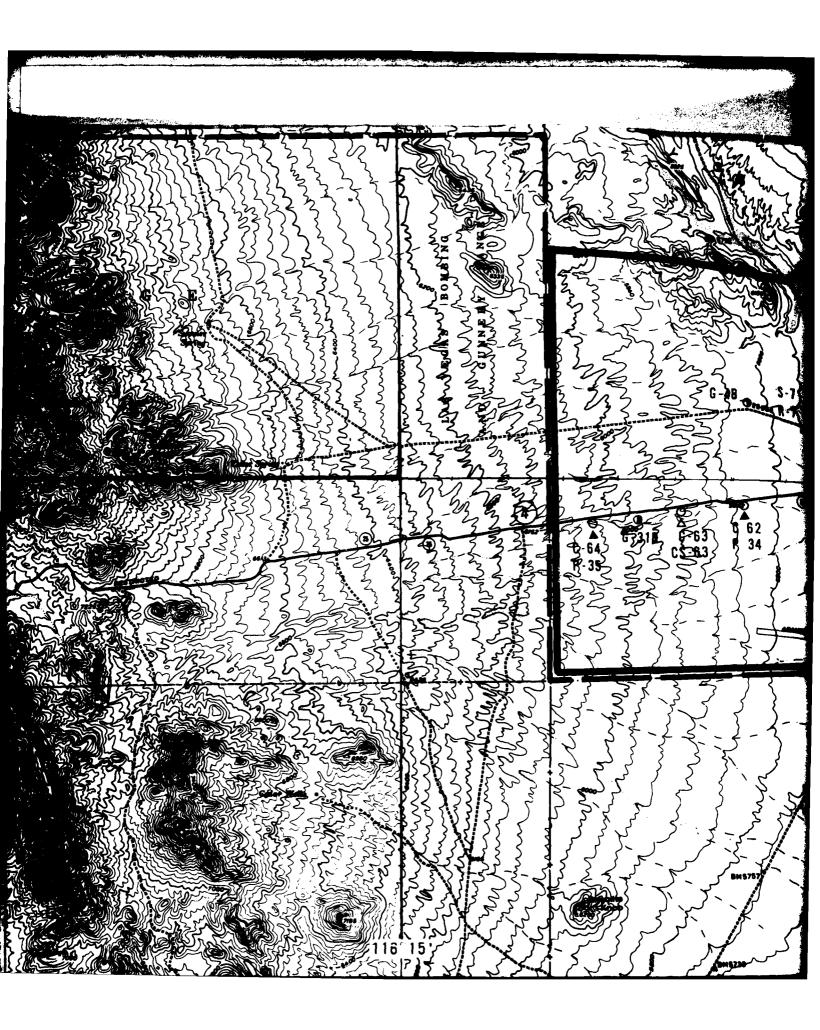


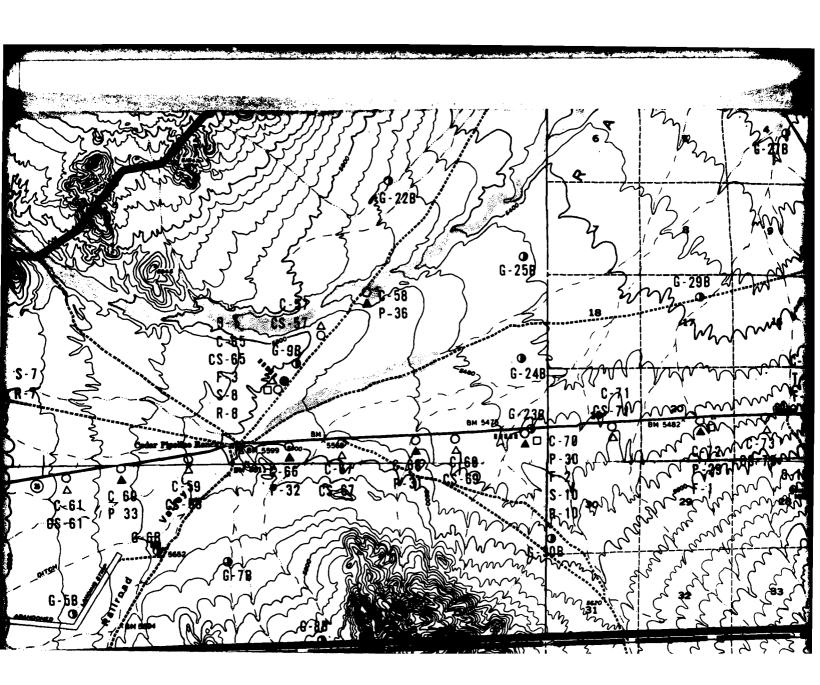


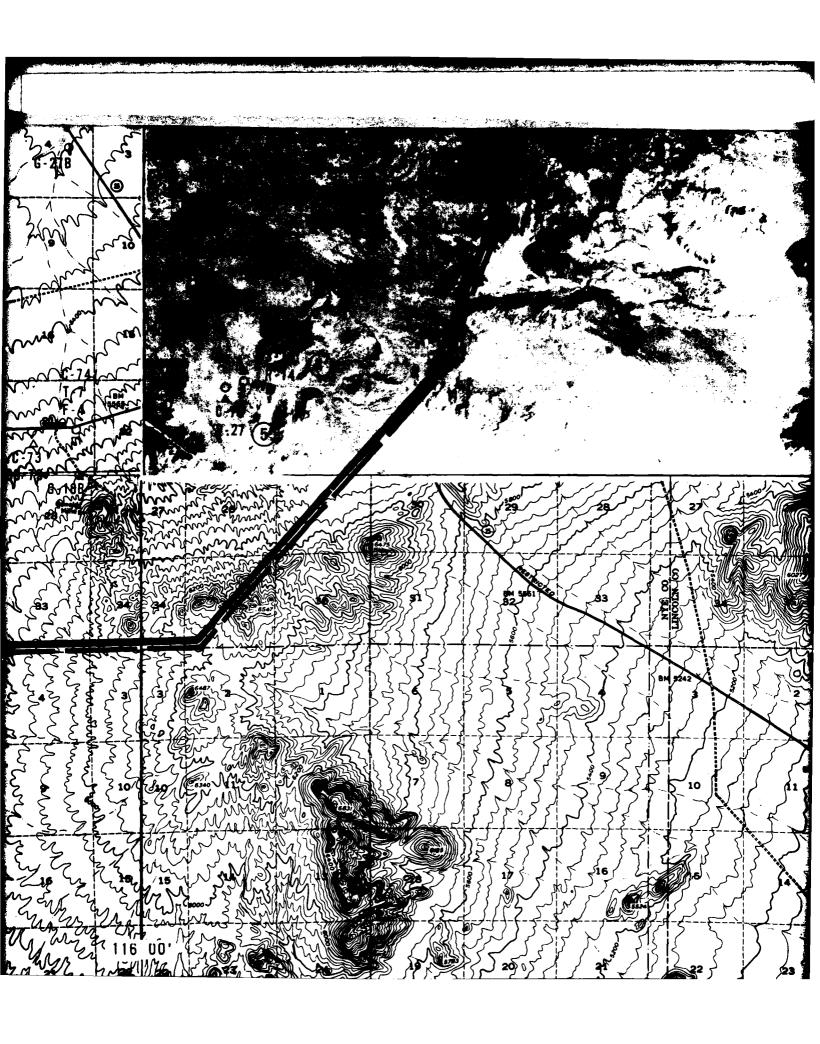


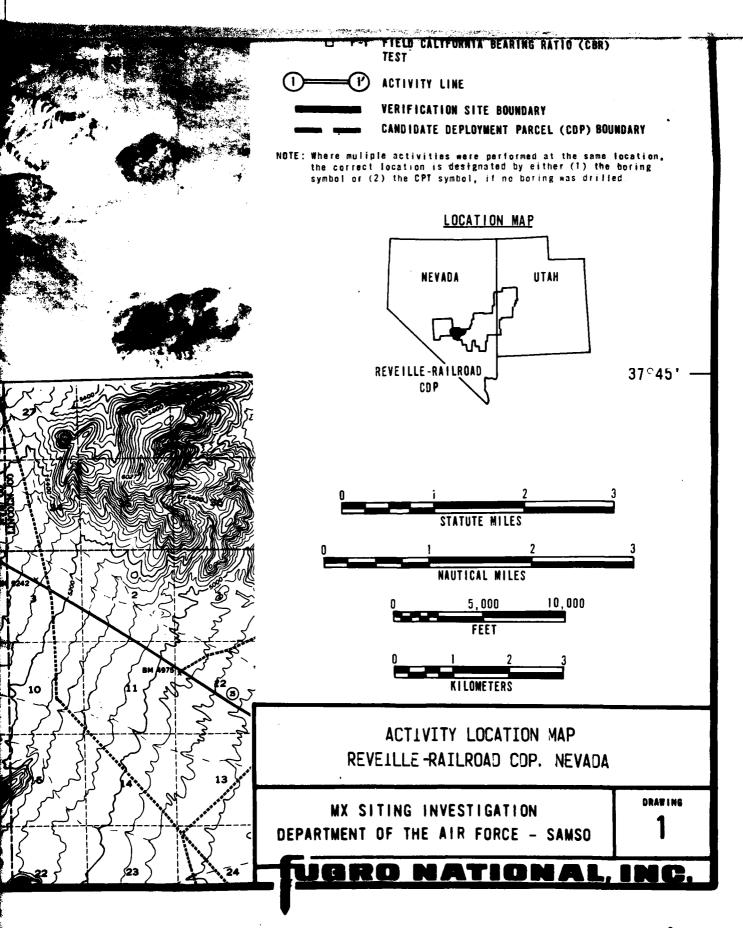
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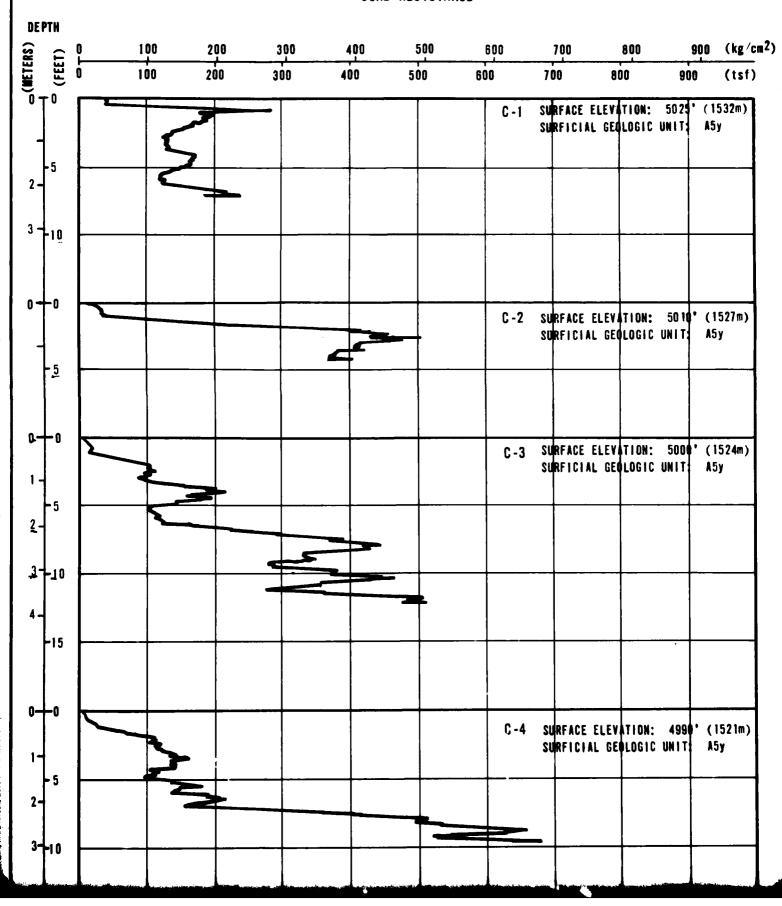




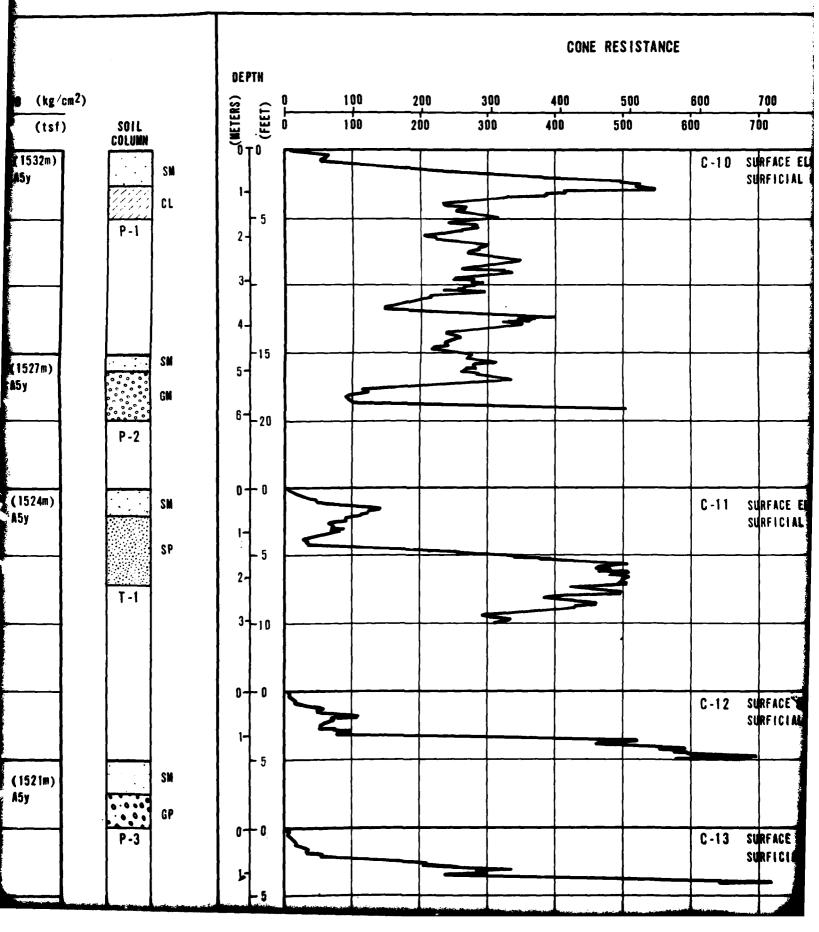


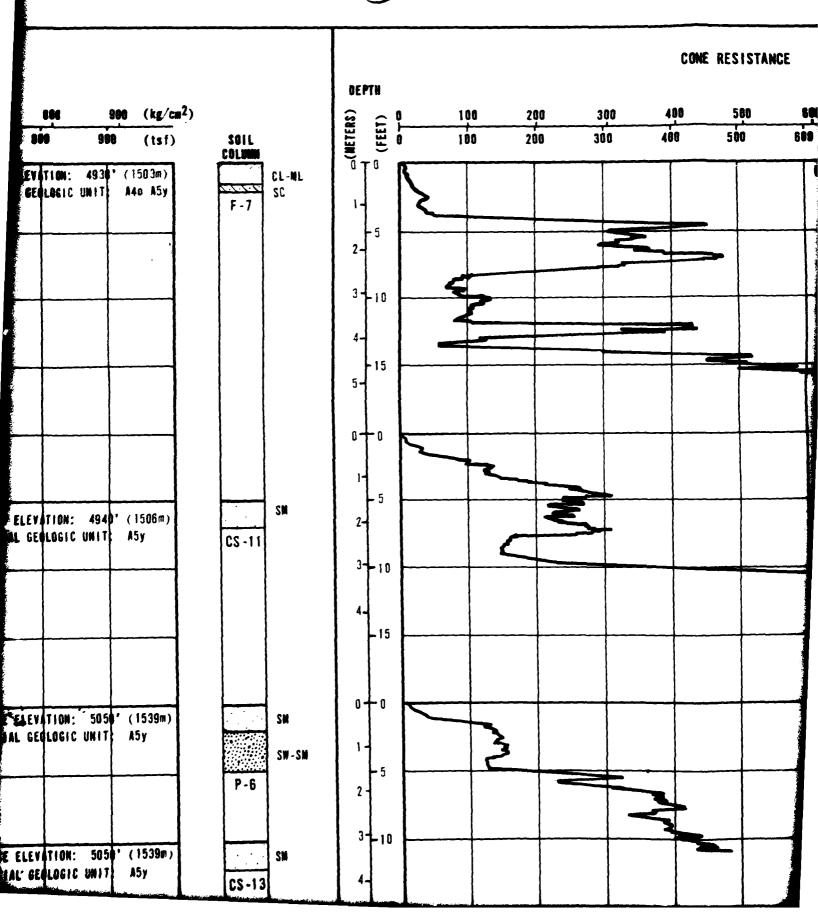


## CONE RESISTANCE



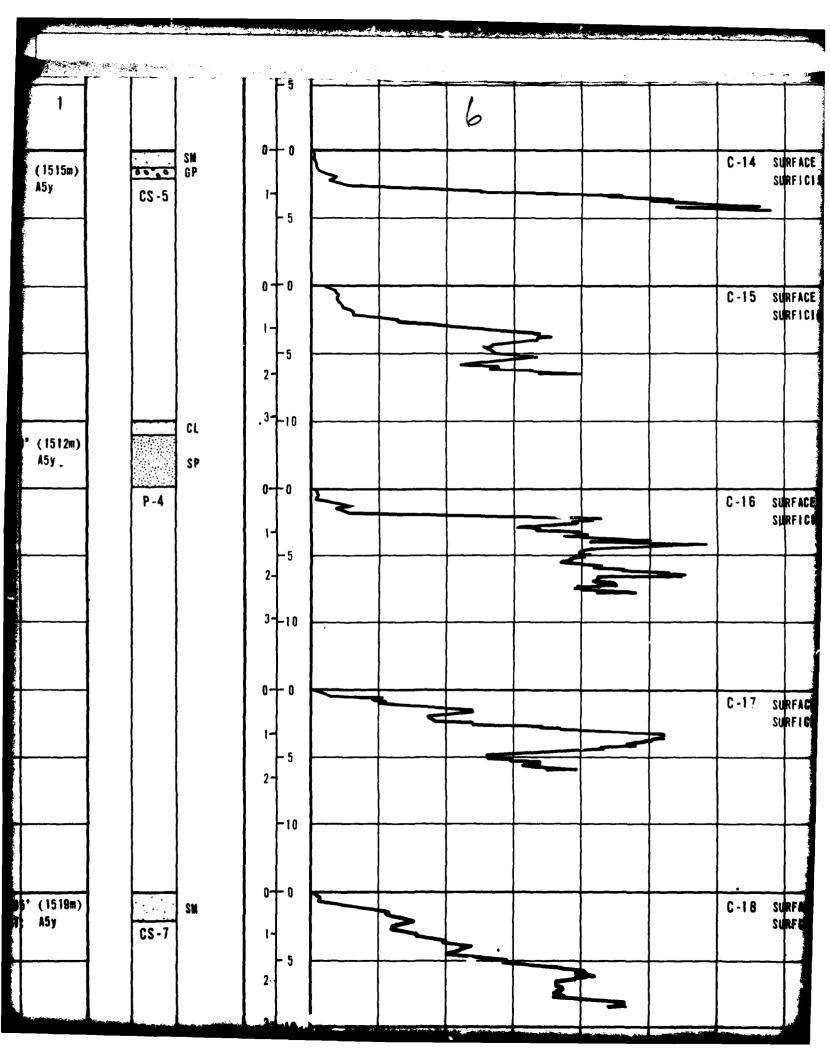
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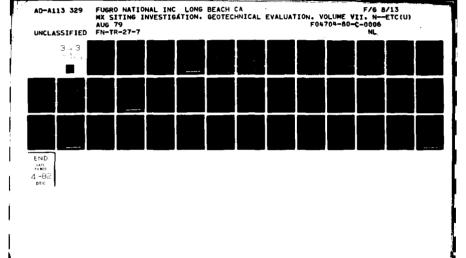
## CONE RESISTANCE

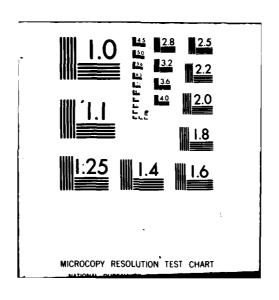
200 200	300	400	500	800	700	800	900 (kg/	cm <sup>2</sup> )
00	300	400	500	600	700	800	900 (tsf	) SOIL
				C-23	SURFACE SURFICIA	ELEVATION: L GEOLOGIC	515\$' (1571m) UNIT: A5i	
	-		-					P-8
				C-24	SURFACE SURFICIA	ELEVATION: L GEOLOGIC	5020° (1530m) UNIT: A5y	3,7-3
₹								P-17
				C-25	SURFACE SURFICIA	ELEVATION: L GEOLOGIC	5005° (1526m) UNIT A5y	CS - 25
		2						

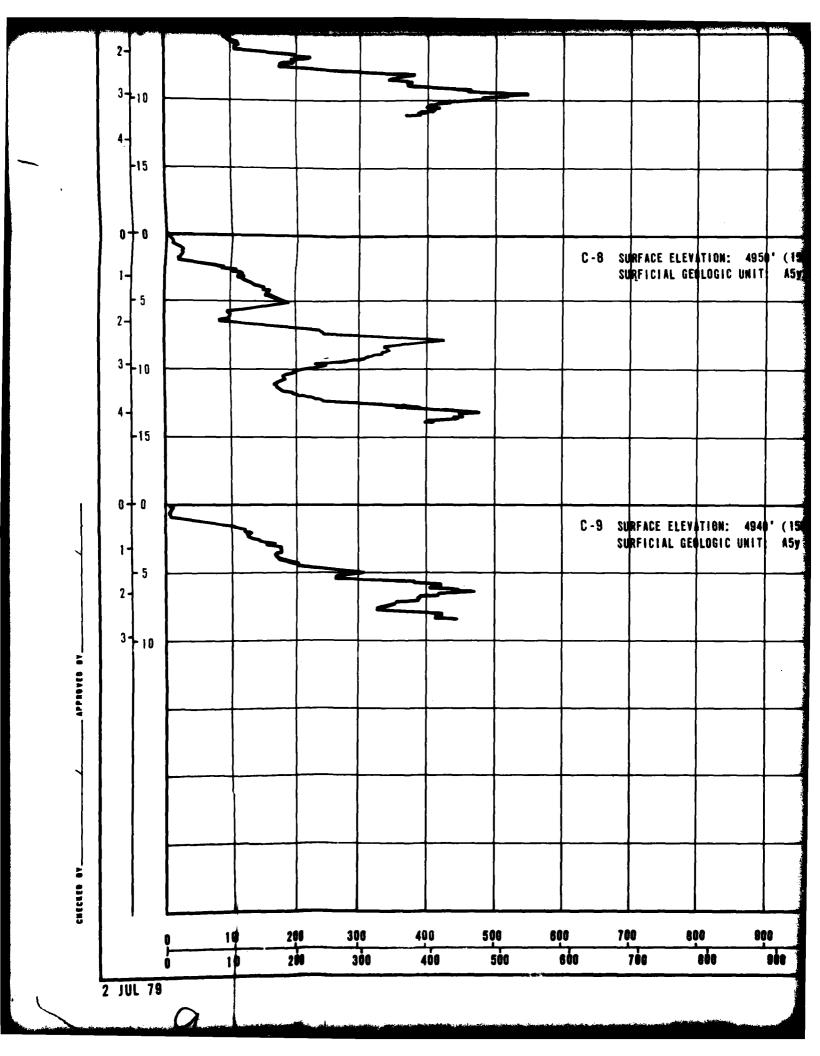


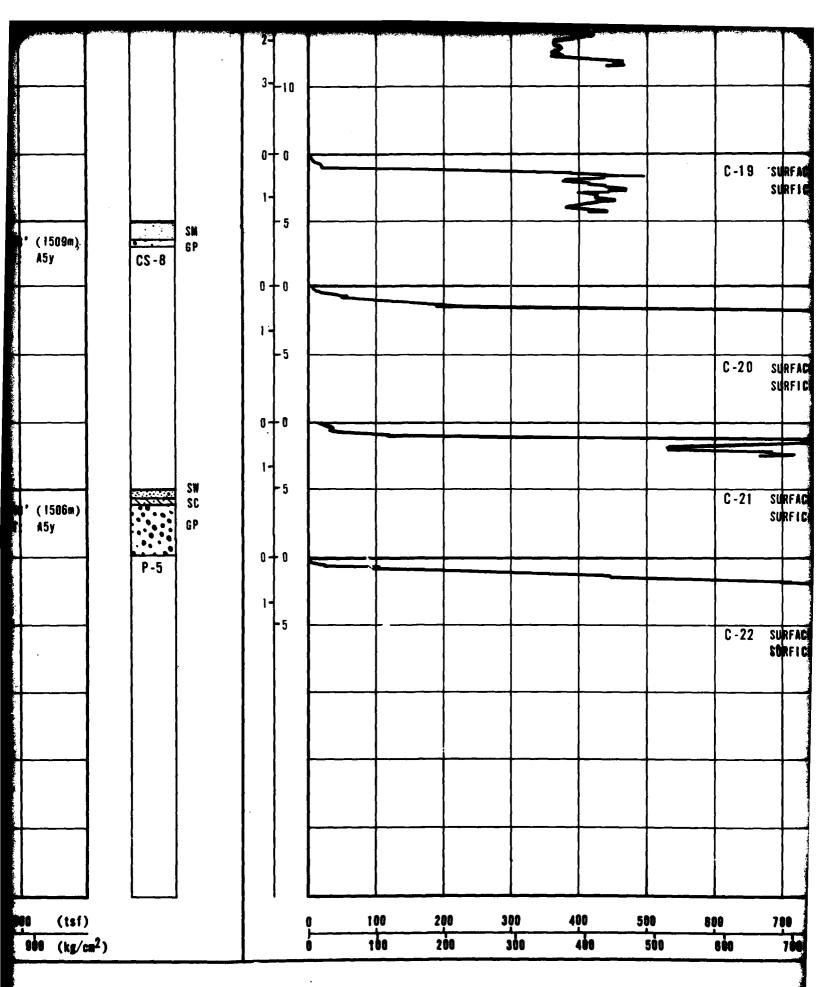
		7
ELEVATION; 5040' (1536m) AL GEOLOGIC UNIT ASY	SM SW SM	0 - 0 1 - 5 2 - 5
E ELEVATION: 5030' (1533m)	SC SM	3-10
		2-5
CE ELEVATION: 5300° (1615m) CIAL GEOLOGIC UNIT ASY	SC 6P	3-10
CE ELEVATION: 5500° (1678m) CIAL GEOLOGIC UNIT A51	SM SW SM	3-10
	B - 5	
CE ELEVATION: 5100' (1554m) GIAL GEOLOGIC UNIT A59	CS-18	3-10

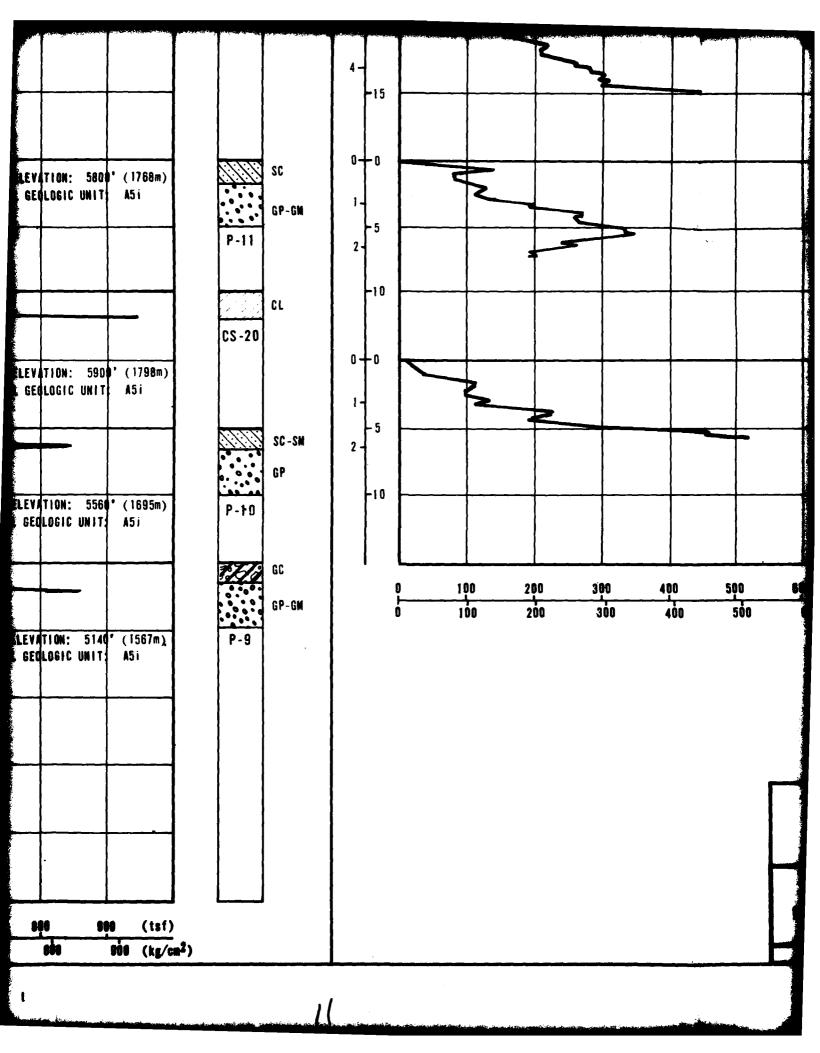
	1	
	C-26 SURFACE ELEVATION: 4990' (1521m) SURFICIAL GEOLOGIC UNIT A5y  GP	
3	P-16	
	C-27 SURFACE ELEVATION: 4975' (1516m) SURFICIAL GEOLOGIC UNIT: A5y	
	CS - 27	
	C-28 SURFACE ELEVATION: 4965' (1513m) SURFICIAL GEOLOGIC UNIT: A5y SP-S	u l
	SM	
	B - 3A	
	C-29 SURFACE ELEVATION: 4950' (1509m) SURFICIAL GEOLOGIC UNIT: A3 A5y  CS-29	

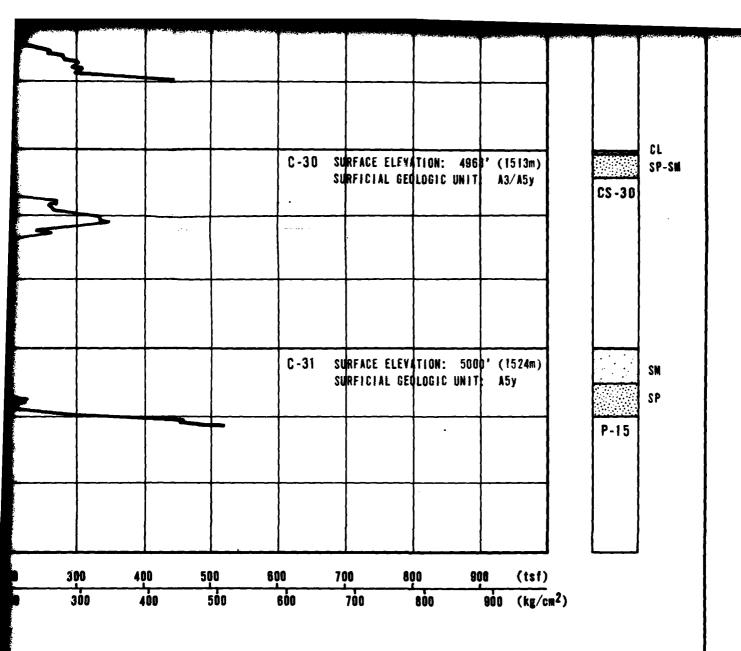










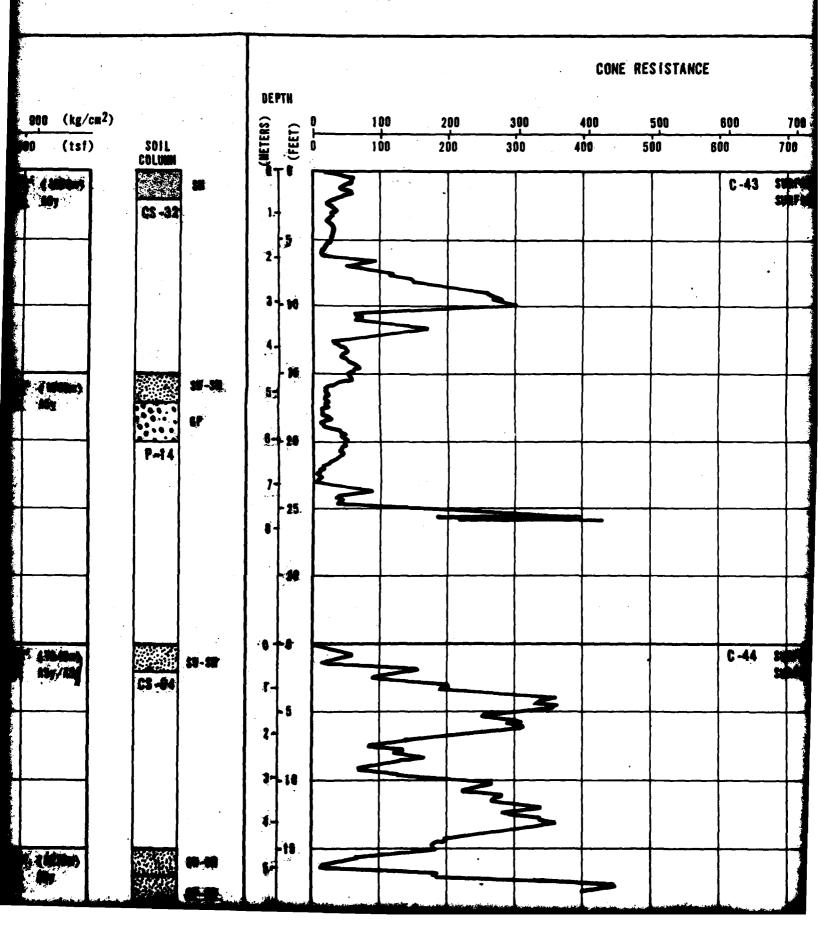


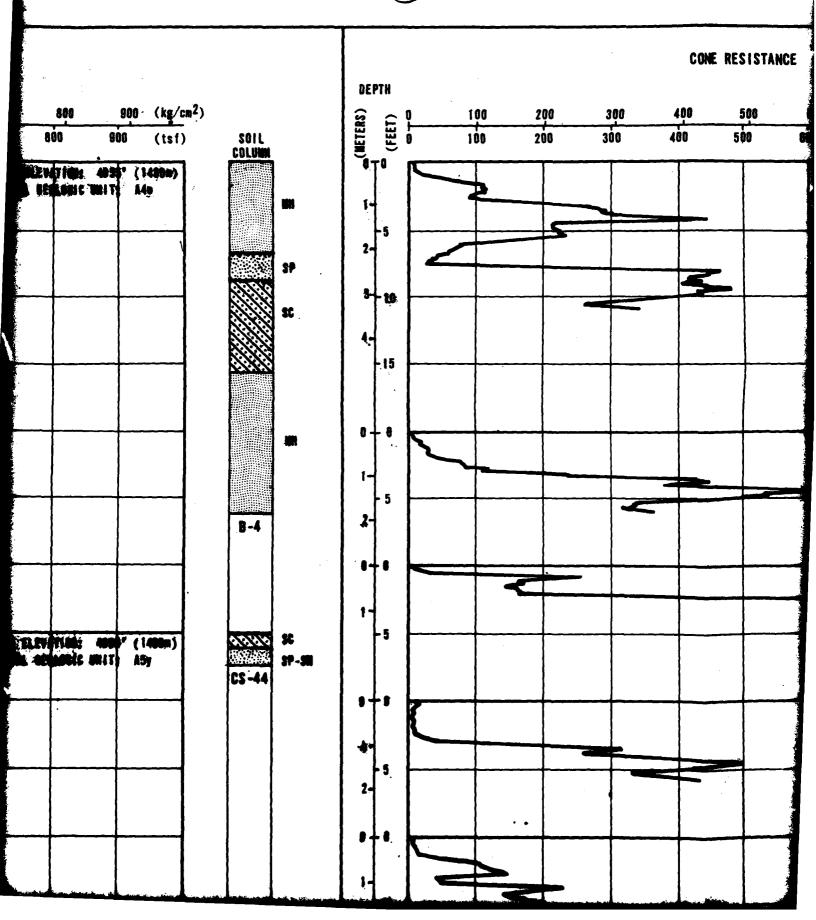
CONE PENETROMETER TEST RESULTS
VERIFICATION SITE
REVEILLE RAILROAD CDP, NEVADA

MX SITING INVESTIGATION

DEPARTMENT OF THE AIR FORCE - SAMSO

UGRO NATIONAL INC.





## CONE RESISTANCE

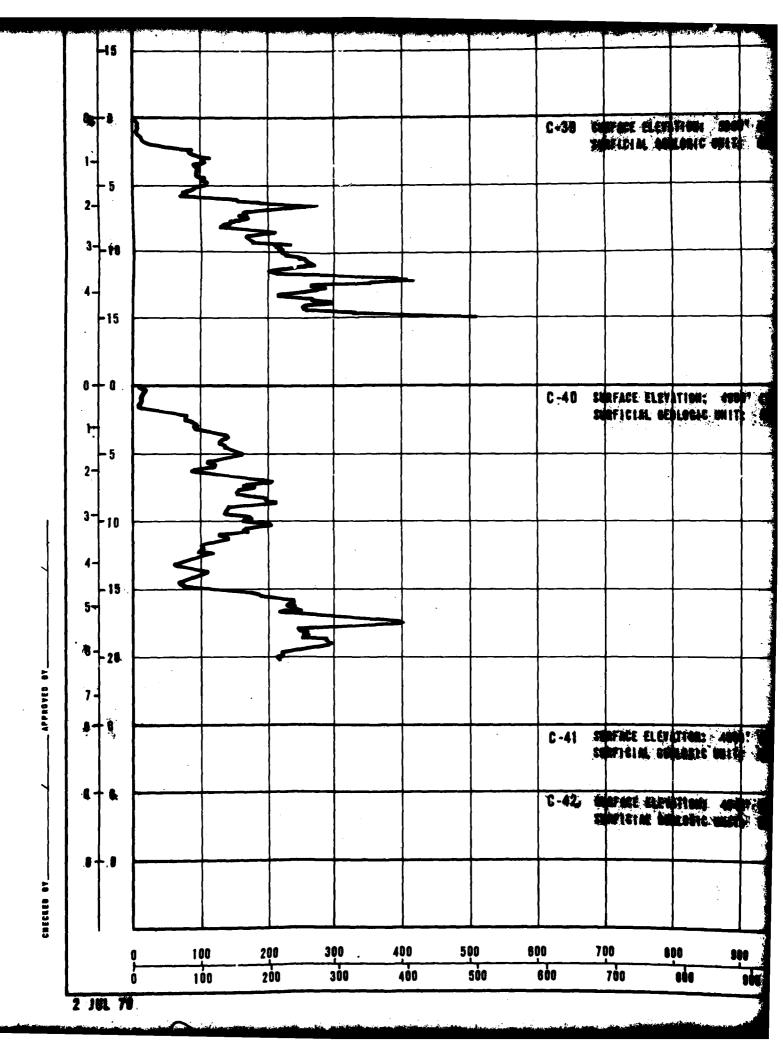
200	300	480	500	600	700	800	900	(tsf)	COLUMN 2011	
5				G-52	SURFACE EL SURFICIAL	EVATION:	5275° 1	(15 <b>90</b> m) ASy		\$ <b>P</b> -\$ <b>i</b>
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						-				
				C-53	SENFACE EL SURFIGHAL	ETATION: GEOLOGIC	5355°	( 1832m) A5 i	CS -53	sc
	~									
						+-				SP
				C-54	SUFFACE EL SUFFICIAL	OECLOSIC 1	gn e t	(1 <b>7070)</b> ASI	P-22	
				C -55	SURFACE EL SURFICIAL	ET TION: REPLOCIC	5189" SNIT	(1573m) R1		30-1 39-1
									1-4	
				C-56	MALIE E	SYSTIME:	1540°	(1987a)	SUNA	20 20

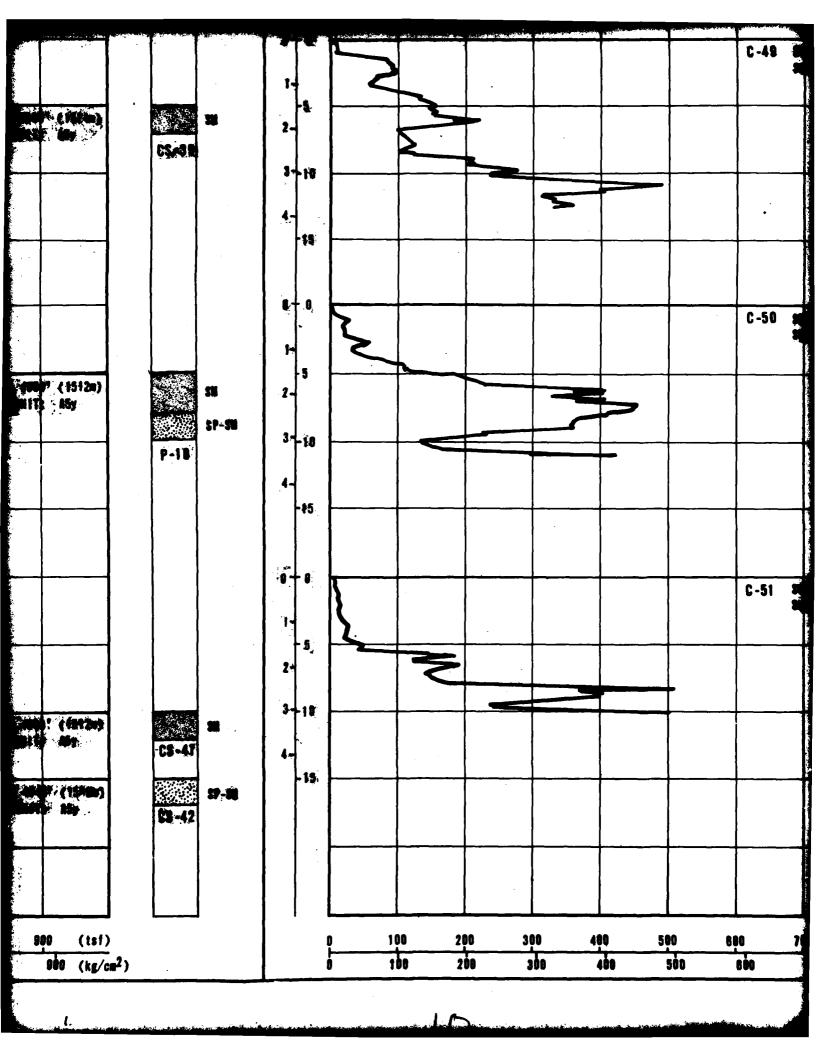
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		<b>69</b>	2-		<b>\</b>						
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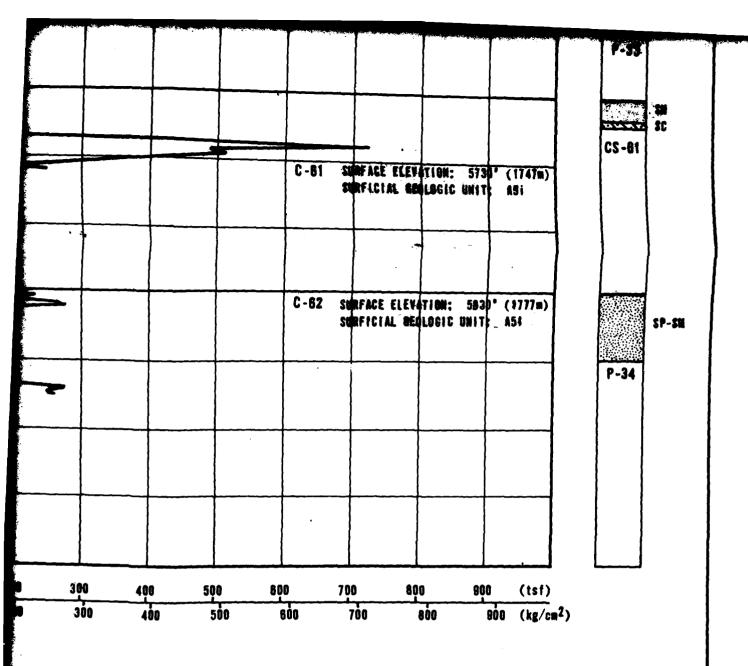
A company of the season									
		0+0			7			<u></u>	C-56
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7	C-56 SURFACE ELEVATION: 5240' (1597m) SURFICIAL GEOLOGIC UNIT: A5y	SM SC SP P-23
	C-57 SURFACE ELEVATION: 5580 (1701m) SURFICIAL GEOLOGIC UNIT: A2	SC GP CS-57
	C-58 SURFACE ELEVATION: 5500° (1676m) SURFICIAL GEOLOGIC UNIT: A1	SM SP P-36
	C-59 SUNFACE ELEVATION: 5840° (1740m) SUNFICIAL SECLOSIC UNIT: ASy	CS-59
	C-80 SURFACE ELEVATION: 5700° (1737m) SURFICIAL REGLOSIC UNIT: A5y	Sa 87-aa





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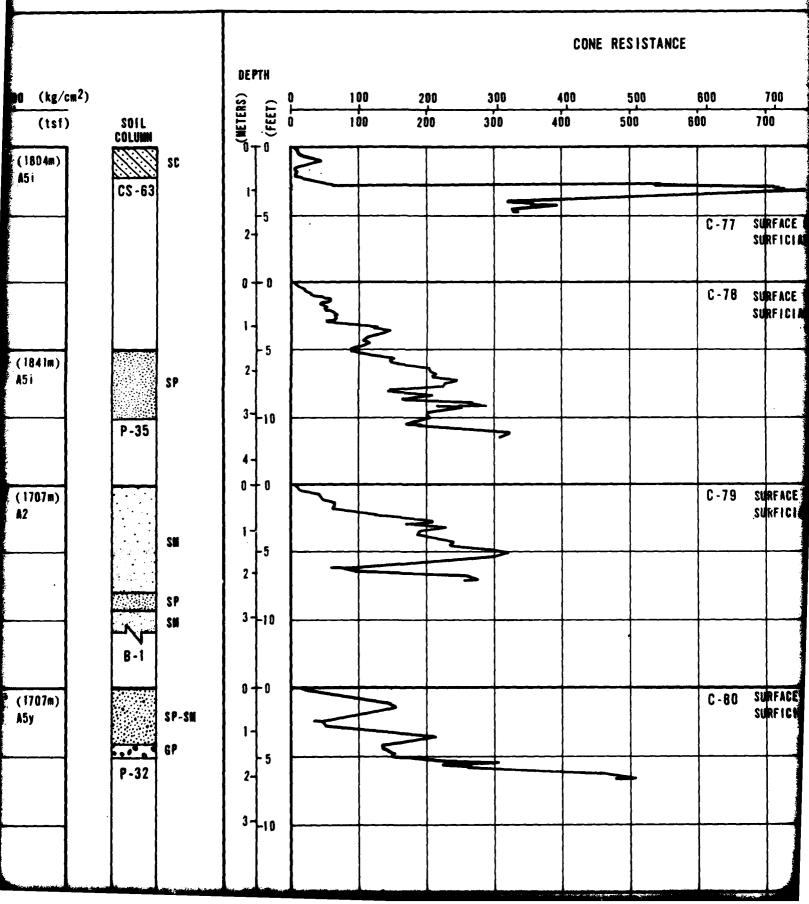
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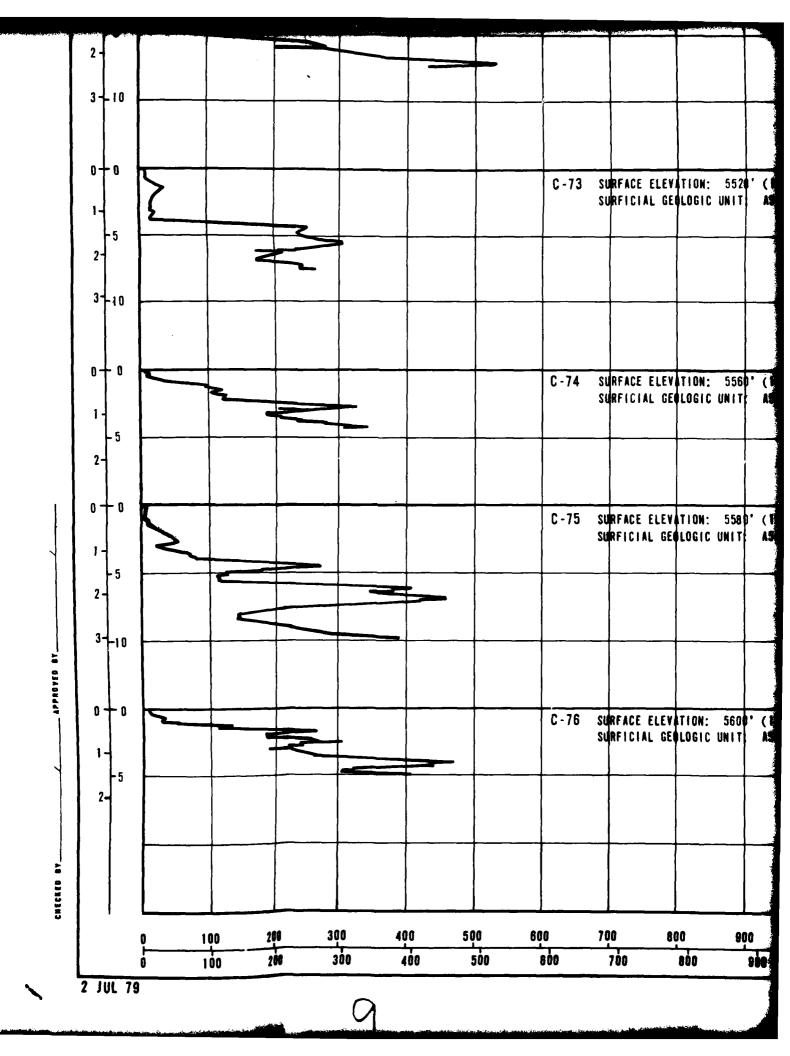
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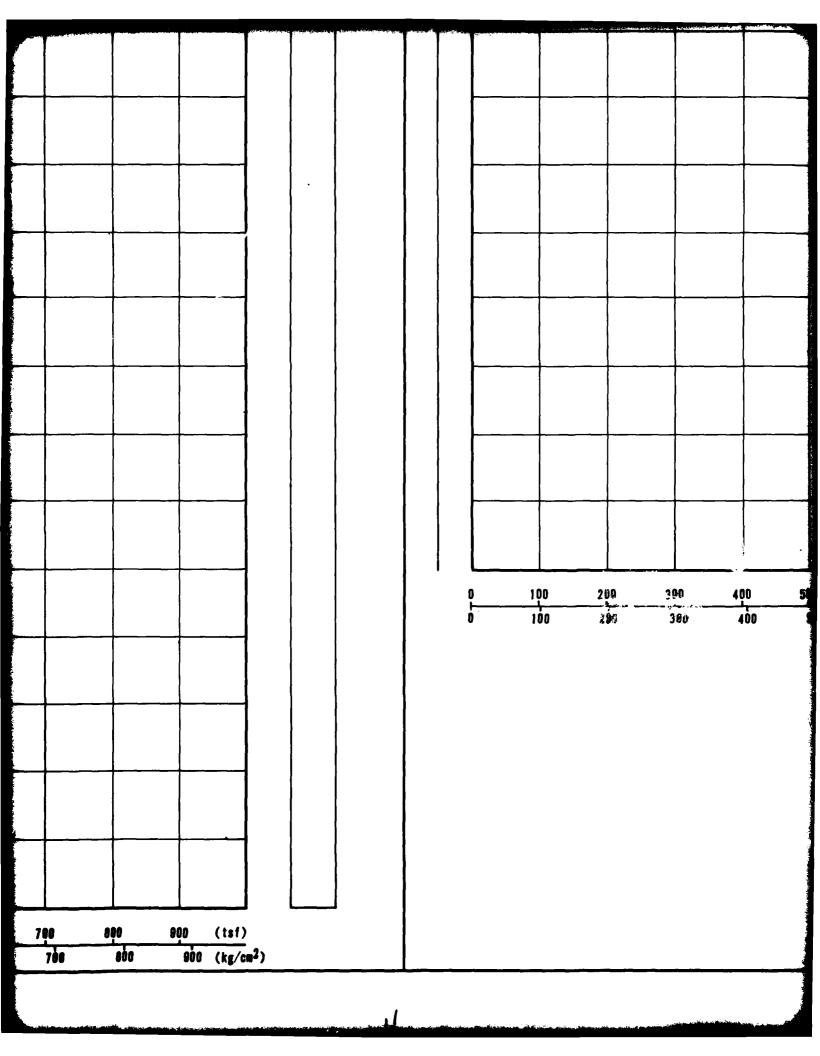
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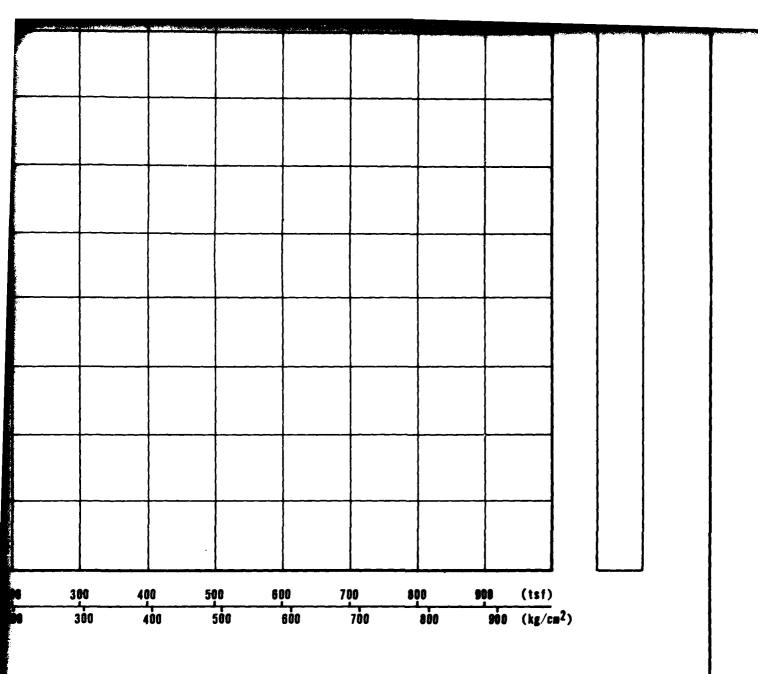
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(1682m) A5y	sc								
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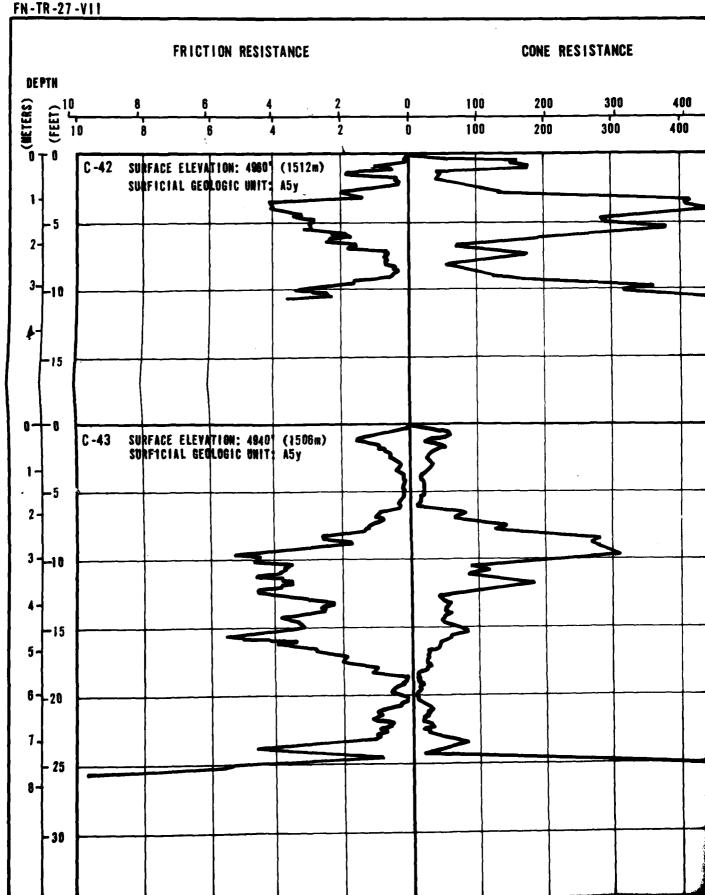


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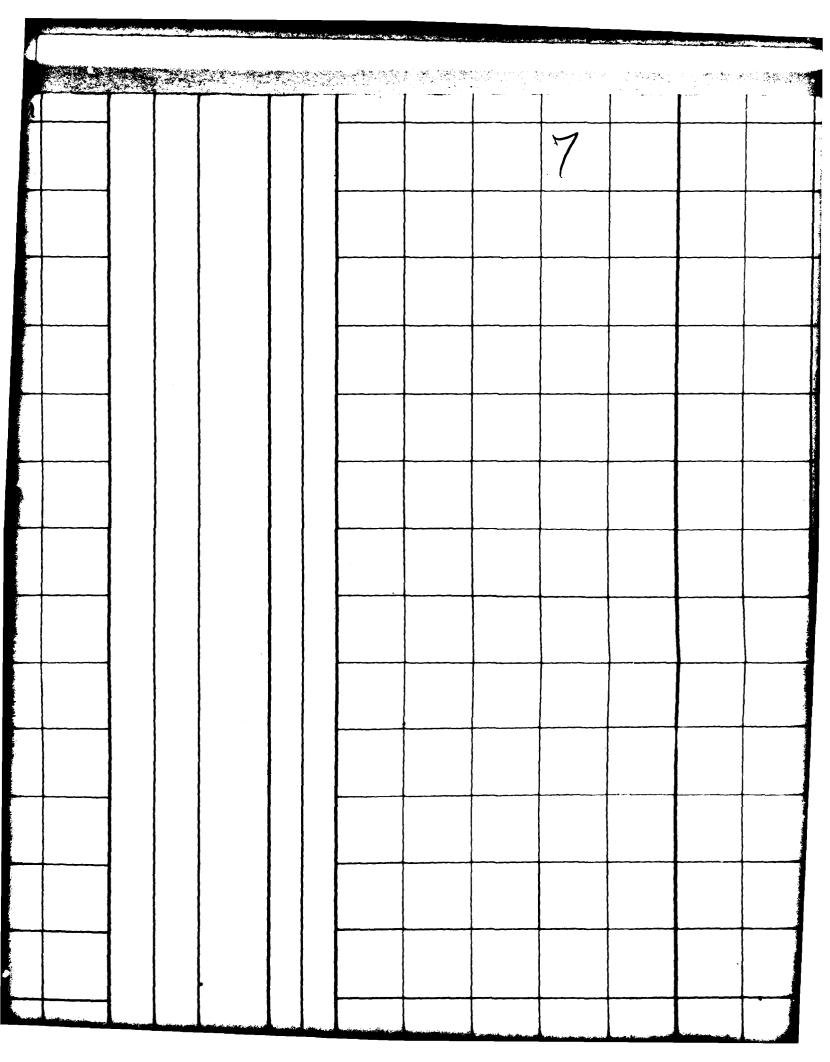


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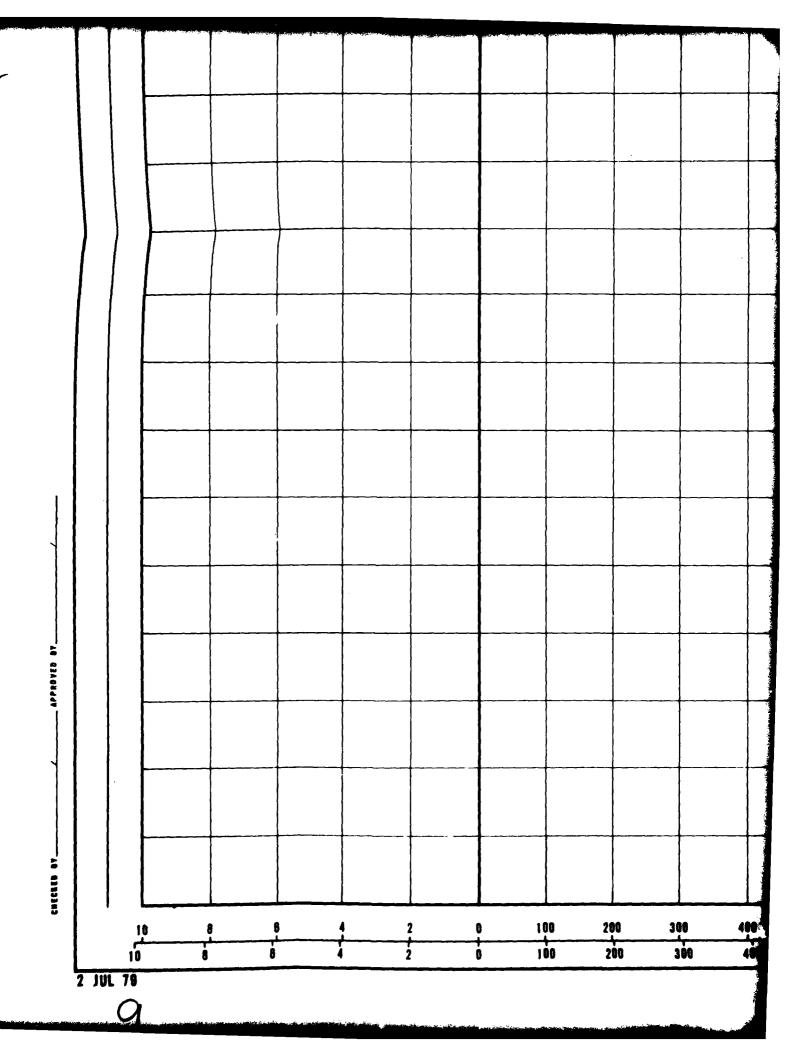
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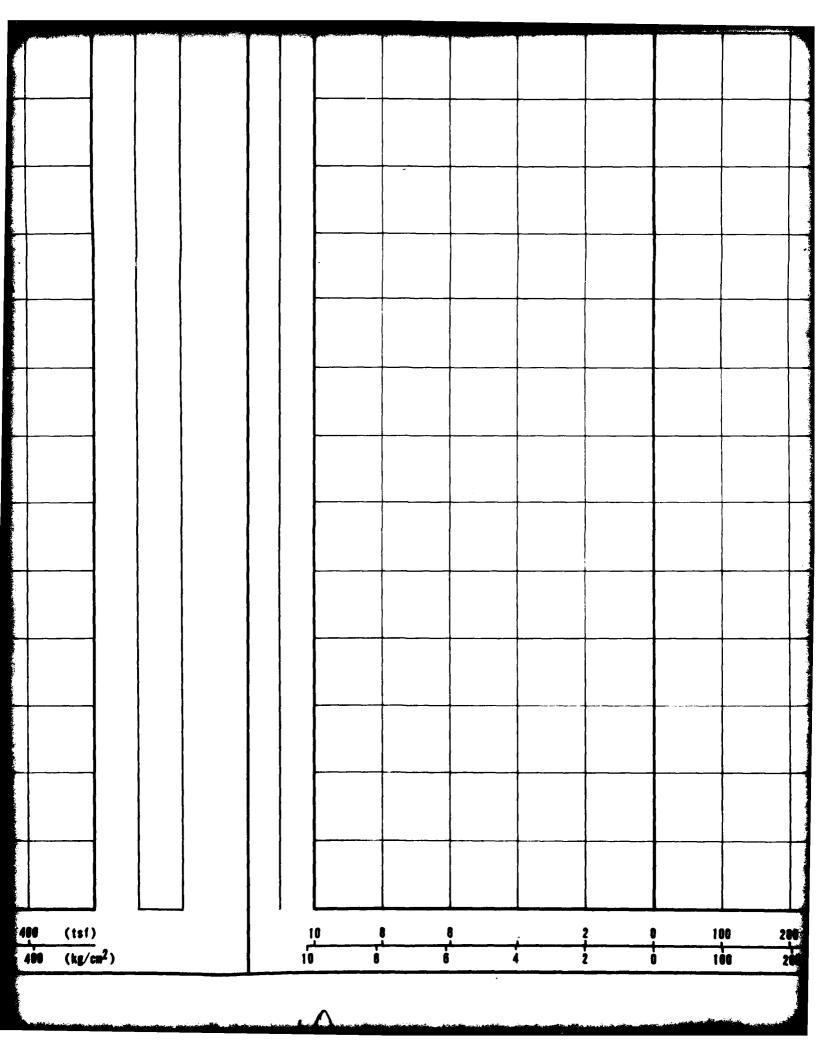
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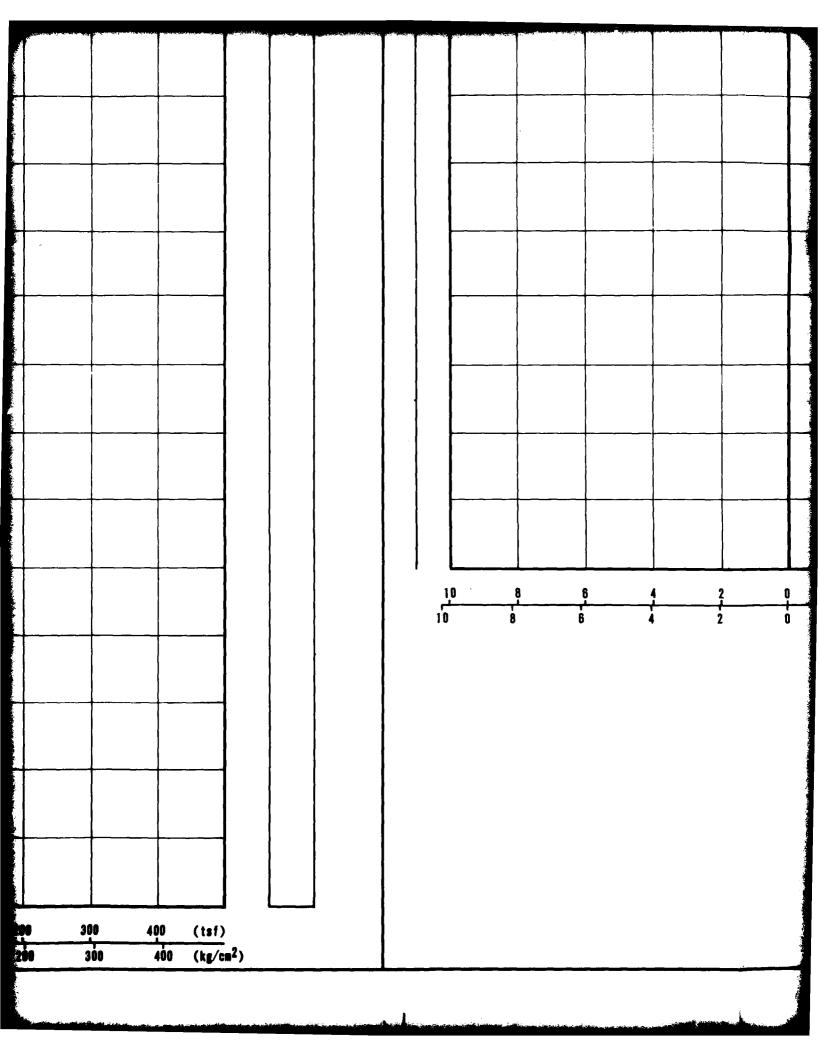
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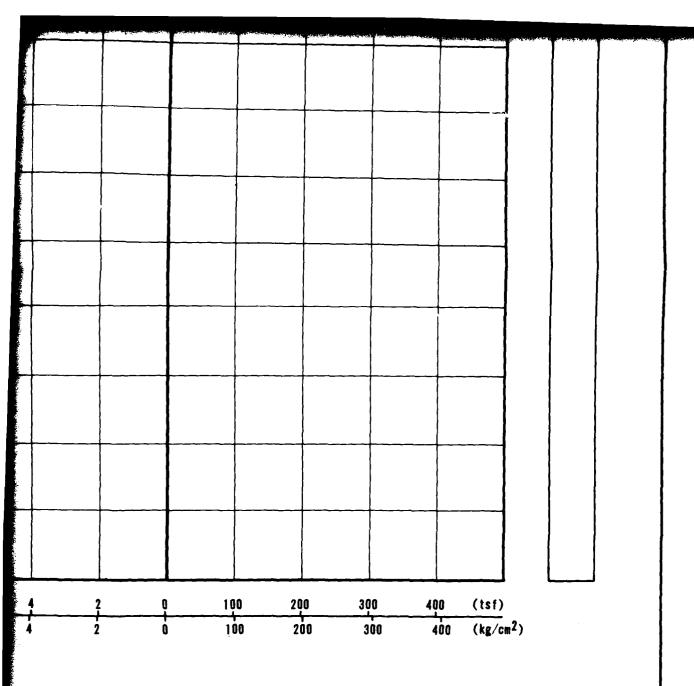


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FRICTION RESISTANCE TEST RESULTS
VERIFICATION SITE
REVEILLE-RAILROAD

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